



Development of Higher-Level Building Block Testing Standards

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NIAR



Development of Higher-Level Building Block Testing Standards

Research Team

NIAR

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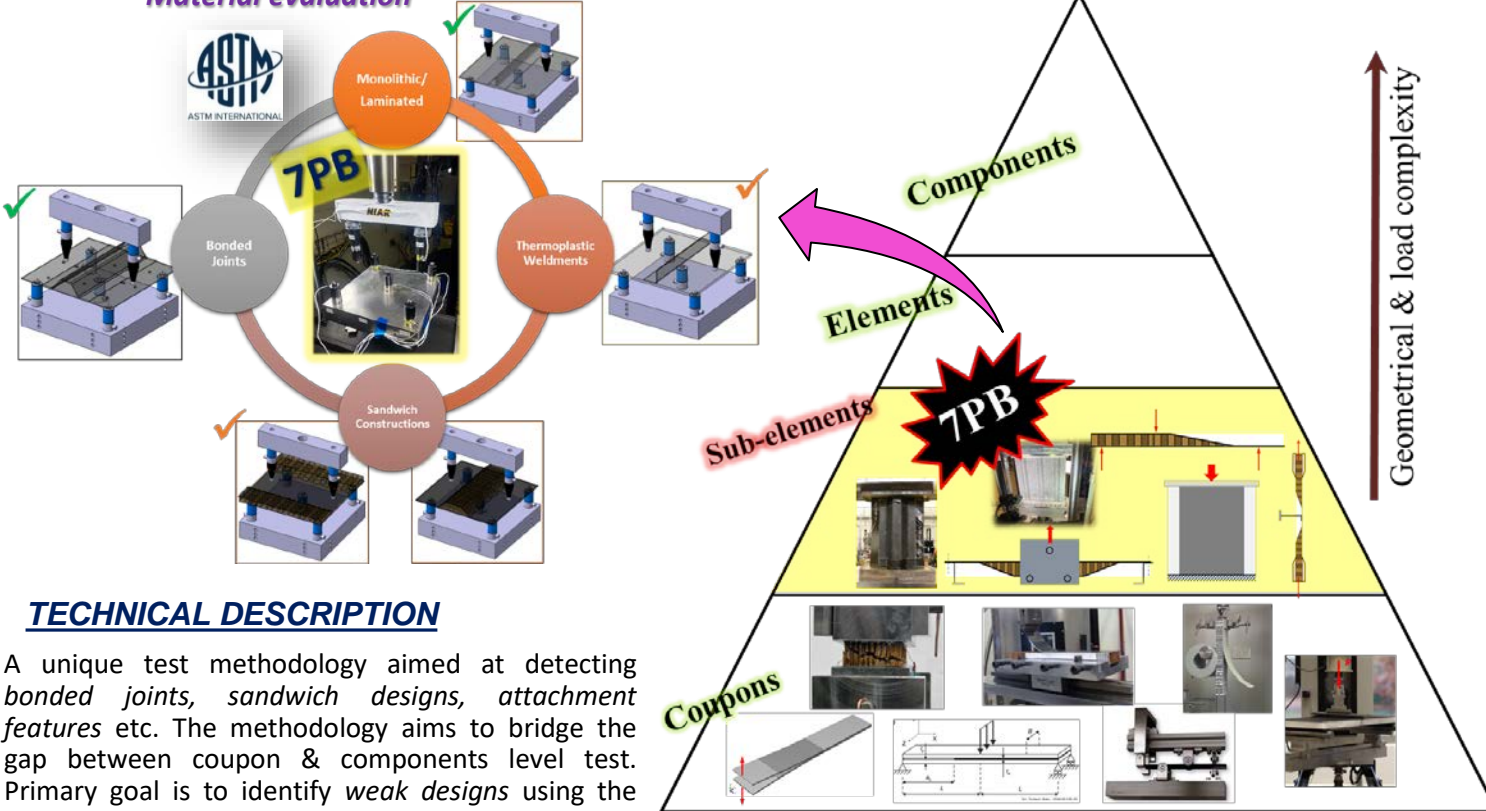
FAA

Ahmet Oztekin, PhD
Larry Ilcewicz, PhD
Cindy Ashforth



A Higher-Level Building Block Test Standard for Sub-Element level Features

Suited for Design, Geometry, Bondline & Material evaluation



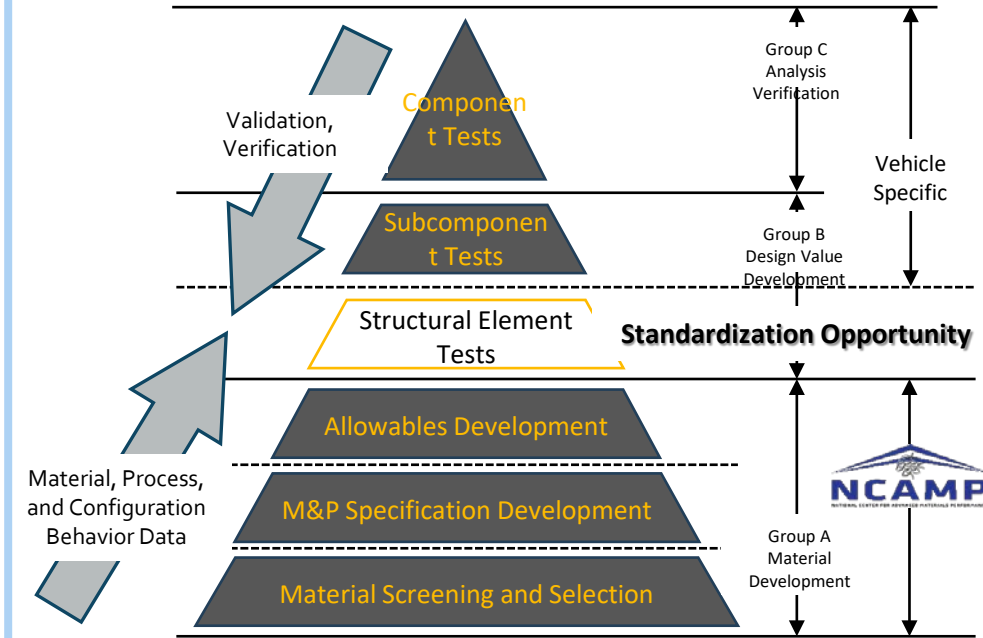
TECHNICAL DESCRIPTION

A unique test methodology aimed at detecting bonded joints, sandwich designs, attachment features etc. The methodology aims to bridge the gap between coupon & components level test. Primary goal is to identify weak designs using the selected methodology which also introduces complex loading scenario.

Project Goals

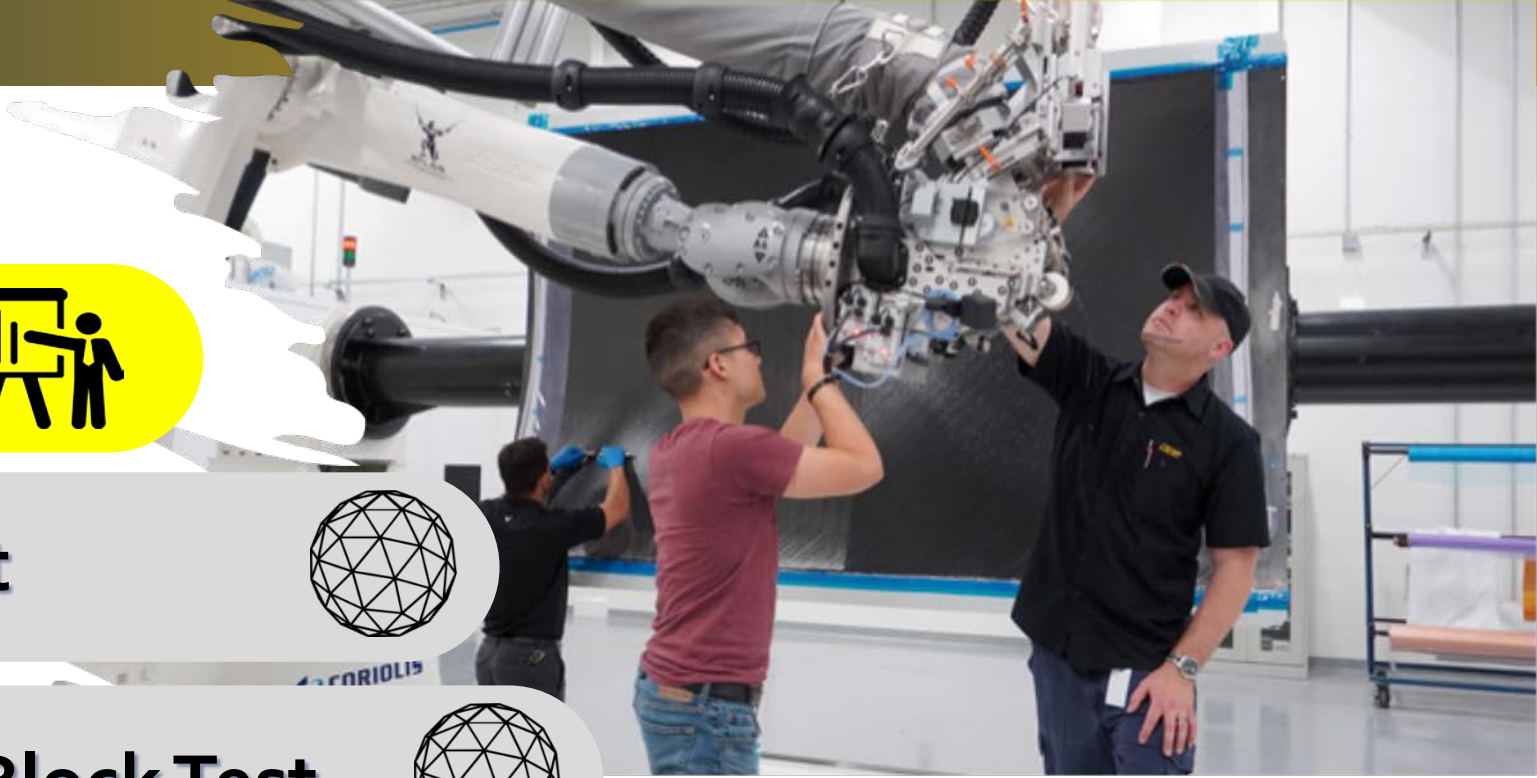
- Design & Development of sub-element based test methodology for *Monolithic & Bonded Structures*
- Evaluate design conservatism in lower-level compared to higher-level Building Block Testing

Approach



Test Findings & Analysis Takeaways

- Seven Point Bend (7PB) is clearly a **mixed-mode** test
- Easy to install & operate; yet **robust enough to introduce complex loading** (long. & transv. bending components)
- Developed **Cohesive Zone based model** is able to capture general specimen kinematics & damage growth.
- **Self-similar crack progression** at skin-stringer interface w/ Zero thickness cohesive layer is **robust**.



Program Overview



Mid-Level Building Block Test



"Smart" Mid-Level Building Block Test



Test Performance Evaluation



Process & Scaling Effects



Background – M&P Variability

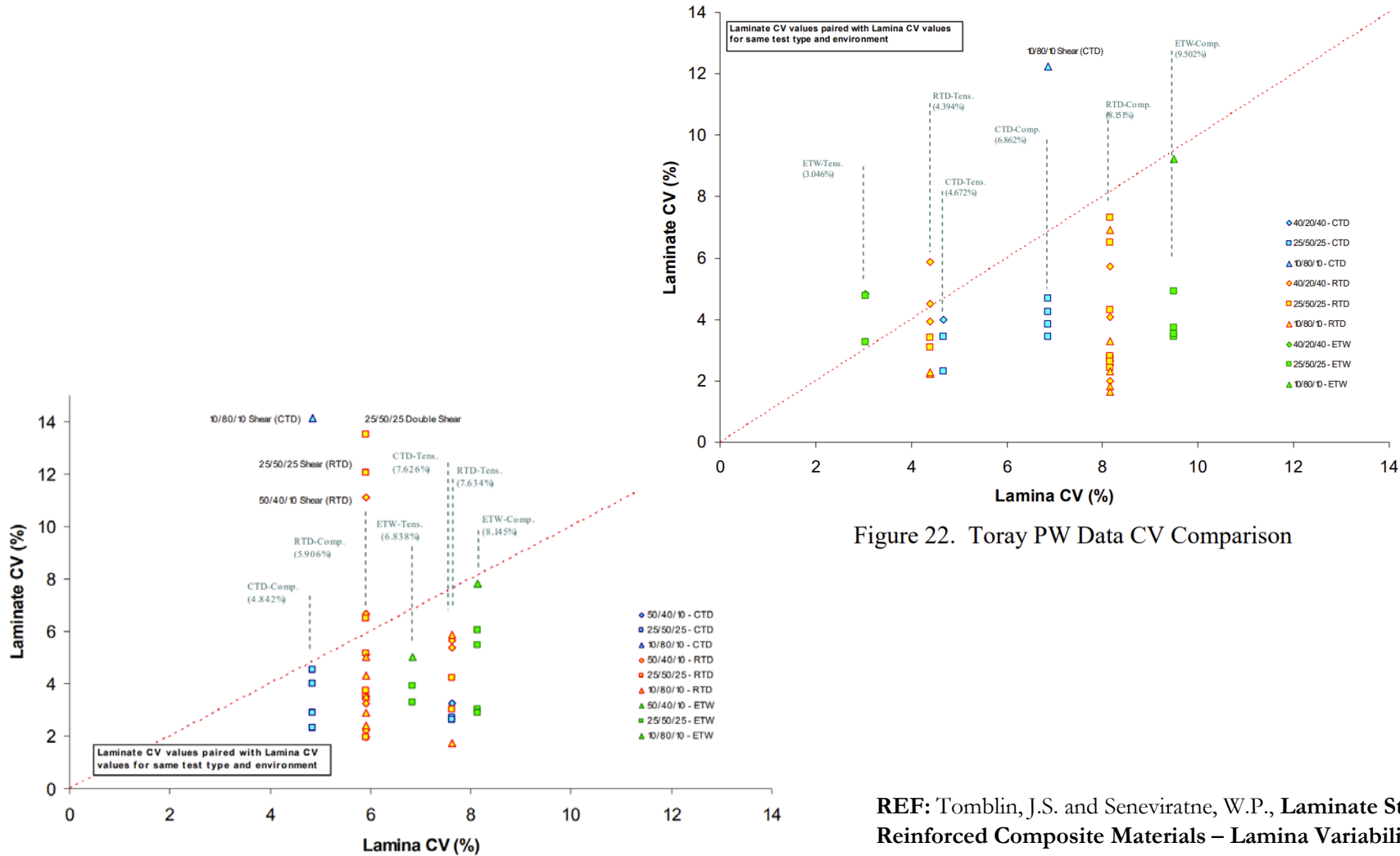


Figure 21. Toray Tape Data CV Comparison

Figure 22. Toray PW Data CV Comparison

DOT/FAA/AR-06/53

Air Traffic Organization
Operations Planning
Office of Aviation Research and
Development
Washington, DC 20591

Laminata Statistical Allowable Generation for Fiber-Reinforced Composite Materials: Lamina Variability Method

January 2009

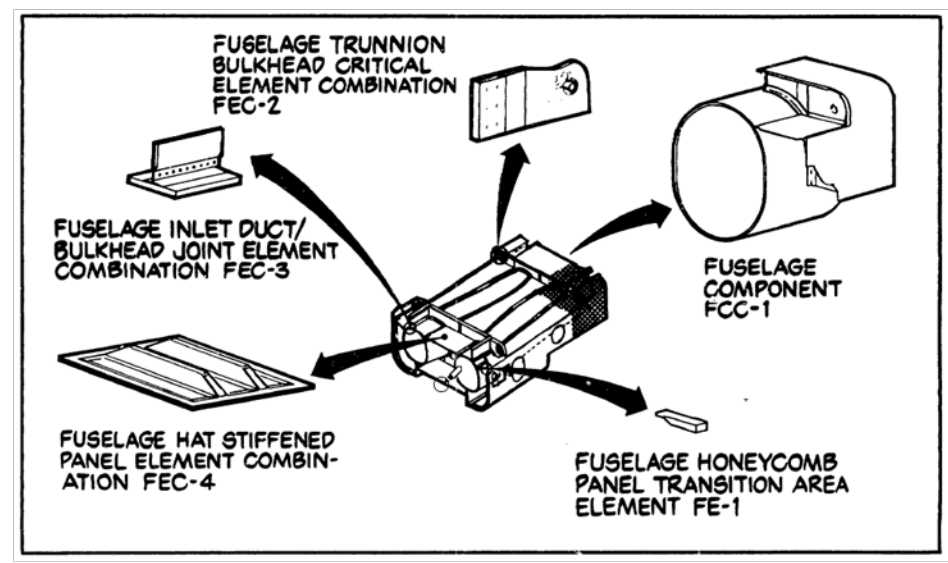
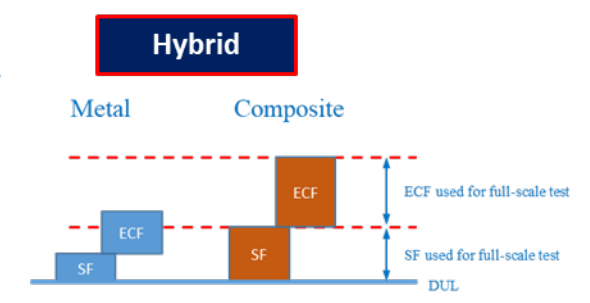
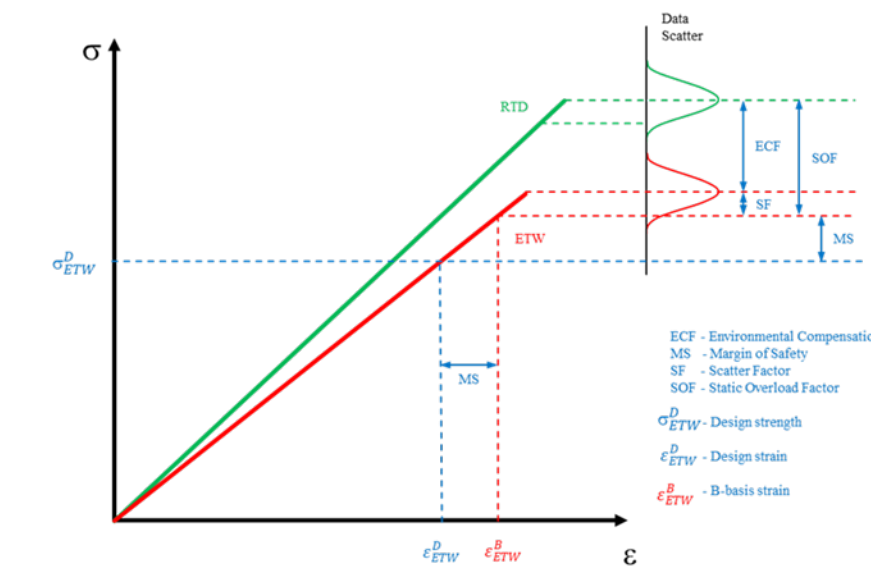
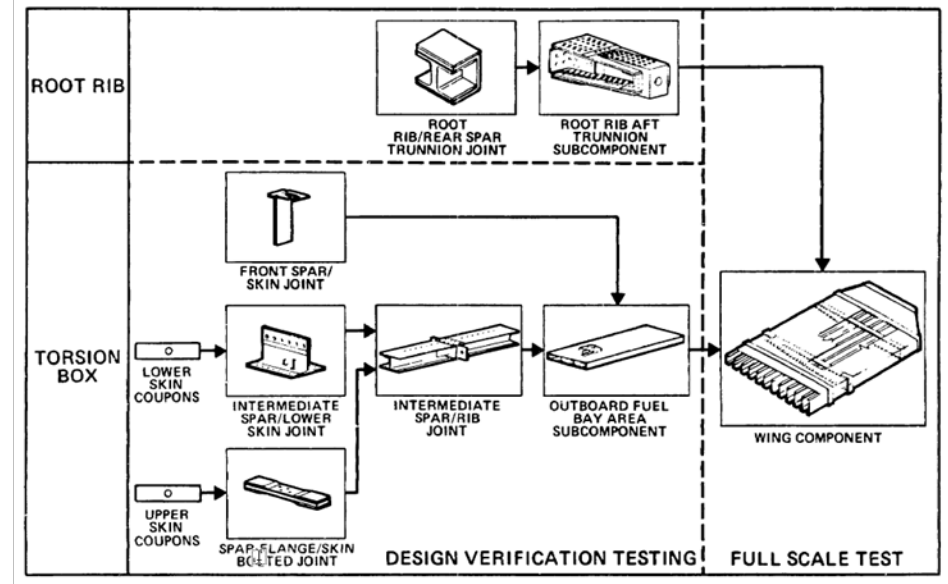
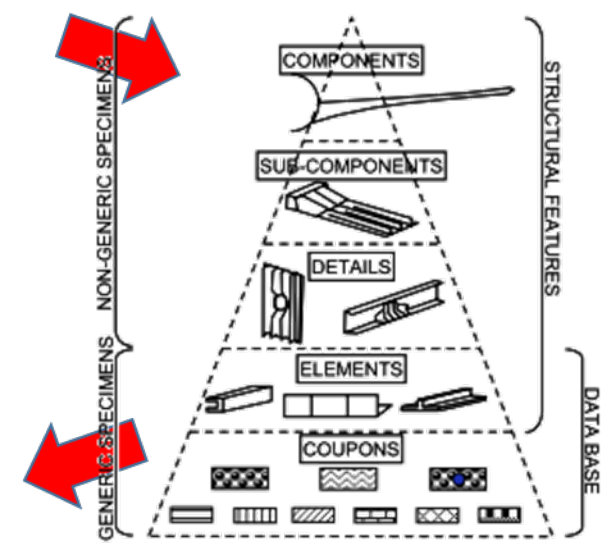
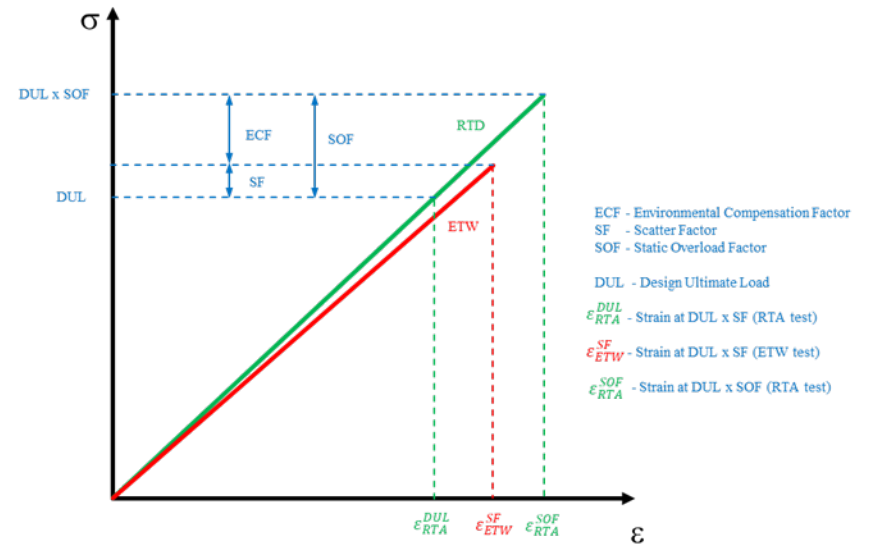
Final Report

This document is available to the U.S. public
through the National Technical Information
Service (NTIS), Springfield, Virginia 22161.

U.S. Department of Transportation
Federal Aviation Administration

REF: Tomblin, J.S. and Seneviratne, W.P., **Laminata Statistical Allowable Generation for Fiber Reinforced Composite Materials – Lamina Variability Method (LVM)**, DOT/FAA/AR-06/53.

Background - Static Overload Factor (ECF+SF)





Program Overview



Mid-Level Building Block Test



"Smart" Mid-Level Building Block Test



Test Performance Evaluation

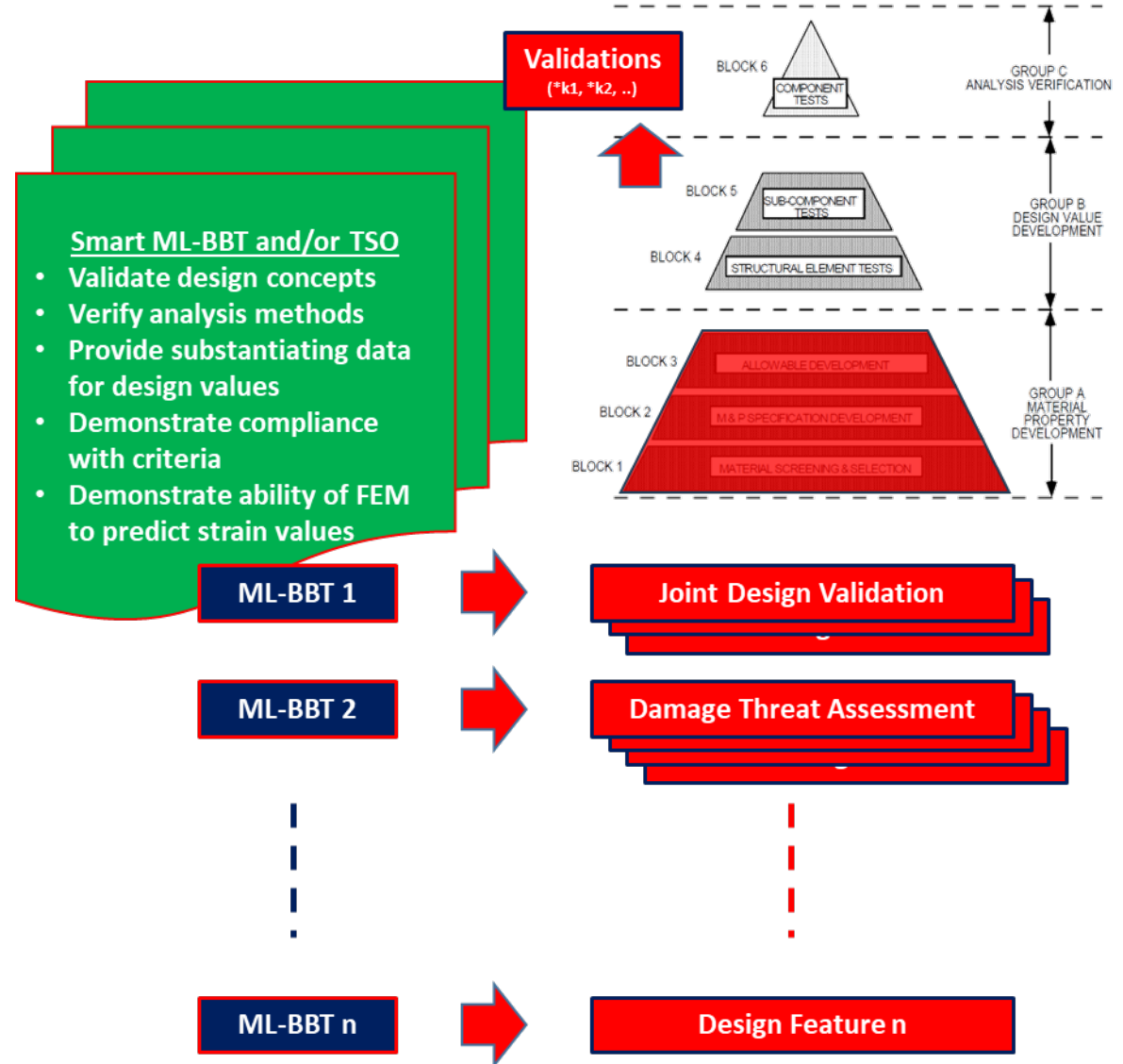


Process & Scaling Effects



Develop a Set of Mid-Level Building Block Tests

- M&P variability
 - Sensitivity to defects
 - Evaluate process spec limits
- Environmental effects
- Thermoset vs. thermoplastics
- Effectiveness of joints
- Manufacturing defects/features and in-service damages
 - Damage threat assessment
 - Scaling
 - Repair
 - Durability and damage tolerance
 - LEF substantiation (*statistical modal values*)

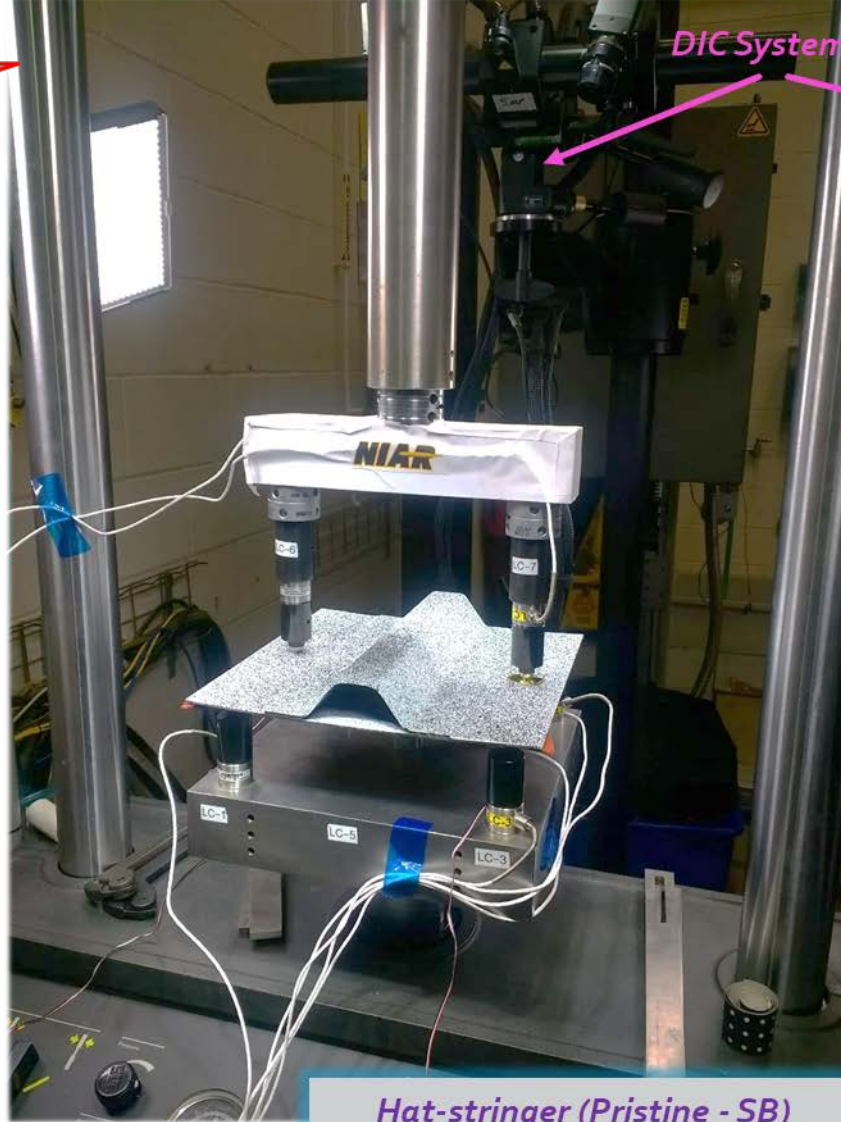


NIAR 7PB Test Setup: T & Hat – Stringers



**Fixture rated
> 6000 lbf**

Load cells



DIC System

Hat-stringer (Pristine - SB)

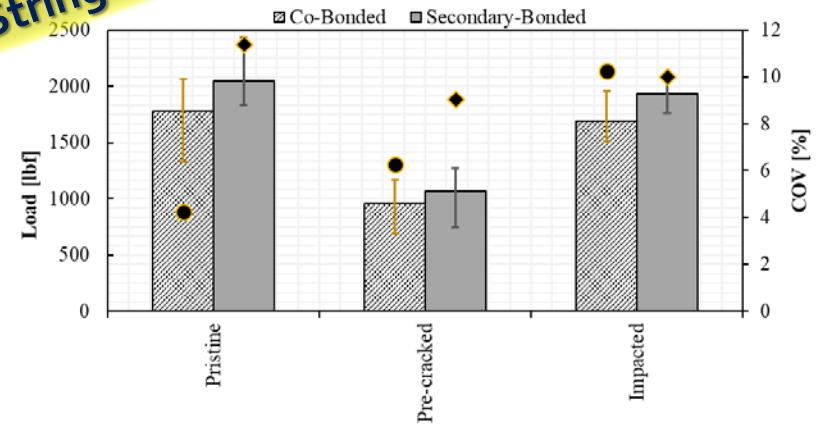


T-stringer (Pristine - SB)

- DIC Systems – 2 employed (front & back)
- Images are stitched post-test
- Each load cell capacity **2050 lbf**
- Test frame rating **11 kip**

7PB Quasi-Static Tests: Brief Summary

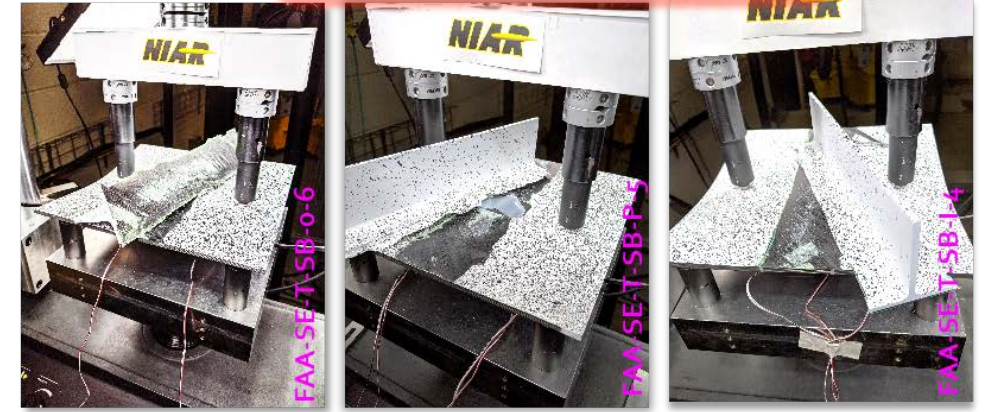
Hat-Stringer



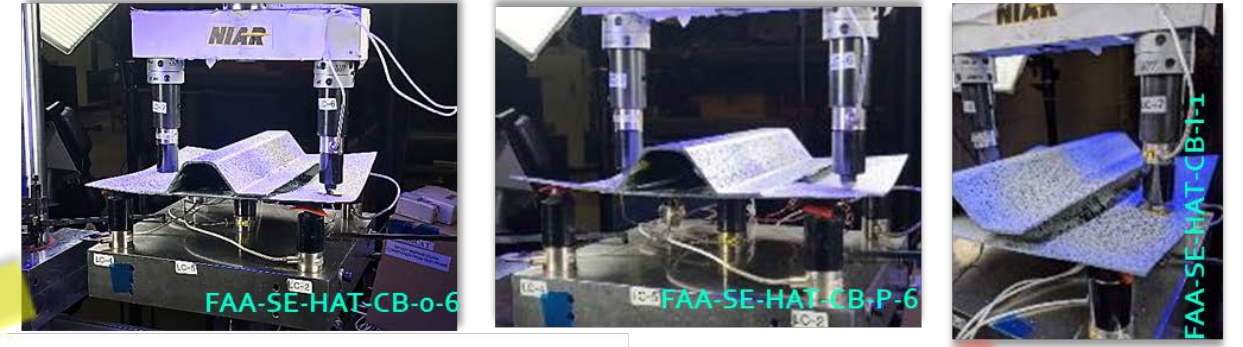
Skin/flange separation (cohesive failure w/ damage progression into first ply)



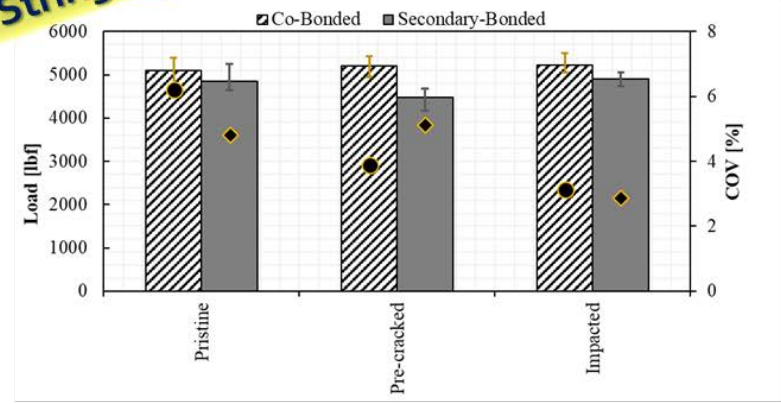
Cohesive failure w/ damage progression into first ply



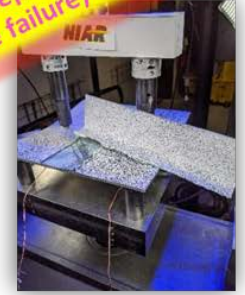
- Fairly Low COV: Highest 11% & lowest of 4%
- Predominantly Cohesive failure observed
- Inter-ply failure by crack migration into first ply and beyond



T-Stringer



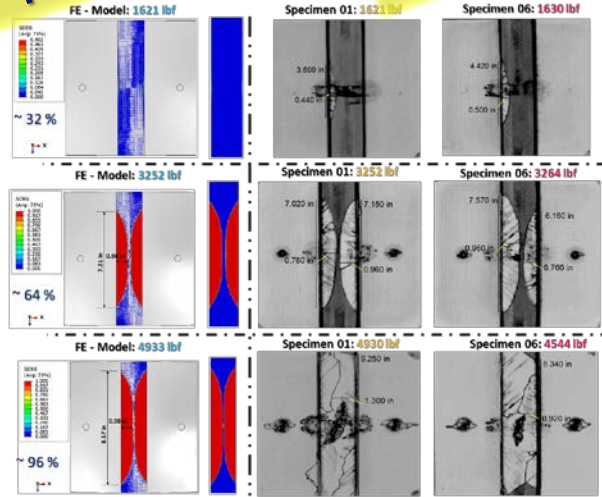
Skin/flange separation (cohesive failure)



Specimen Type	Fab. Process	Specimen Config.	Avg. Failure Load [lbf]	COV [%]
 T-Stringer	Co-bonded	Pristine (Baseline)	5096.4	6.2
		Pre-cracked	5211.1	3.9
		Impacted	5231.2	3.1
	Secondary bonded	Pristine (Baseline)	4856.2	4.8
		Pre-cracked	4478.7	5.1
		Impacted	4910.1	2.9
 Hat-Stringer	Co-bonded	Pristine (Baseline)	1777.1	4.2
		Pre-cracked	957.4	6.3
		Impacted	1691.2	10.3
	Secondary bonded	Pristine (Baseline)	2046.3	11.4
		Pre-cracked	1067.7	9
		Impacted	1934.1	10

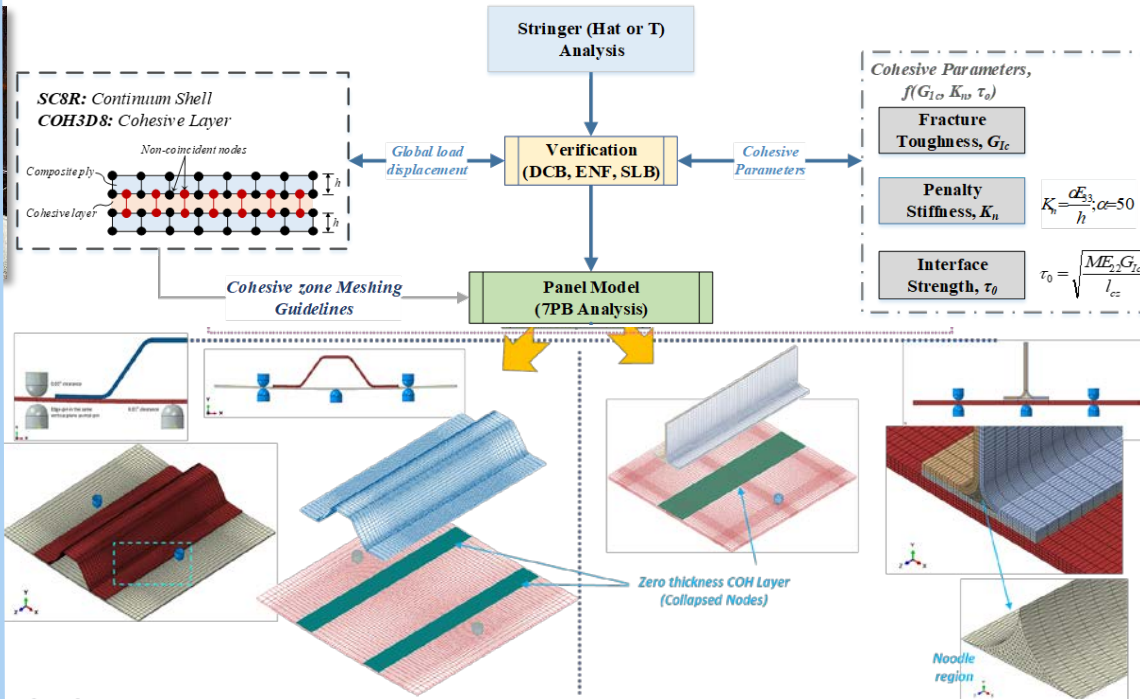
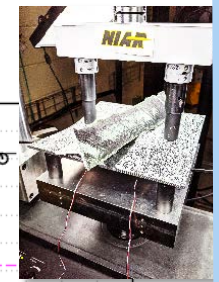
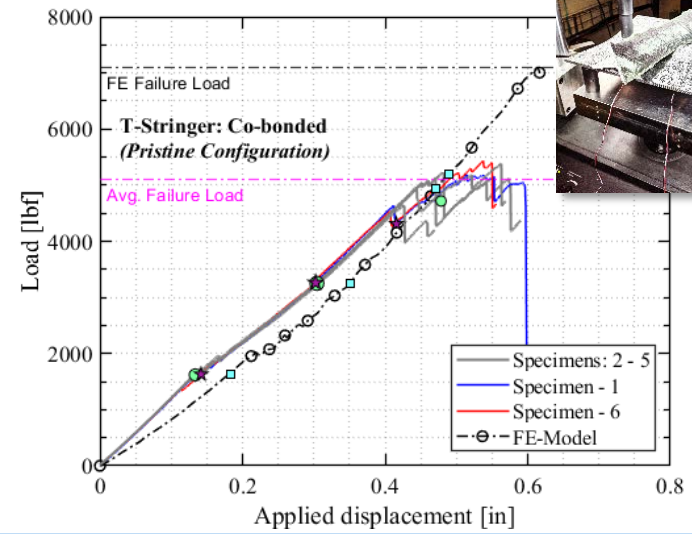
Prediction of Damage Initiation & Evolution in Co-bonded T & Hat-Stringers

FEA

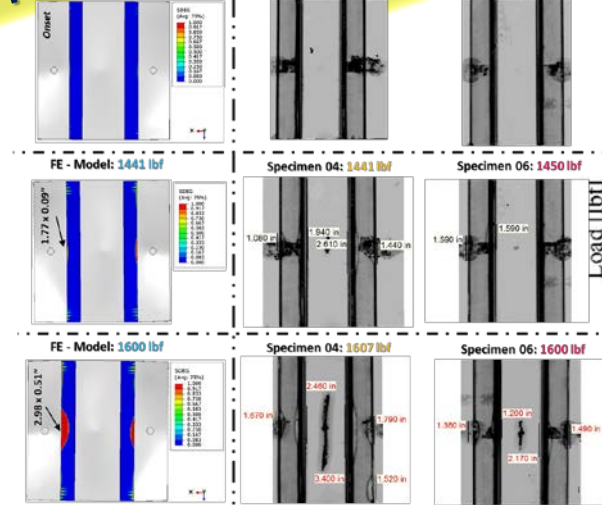


NDI

Co-Bonded T-Stringer (Pristine)

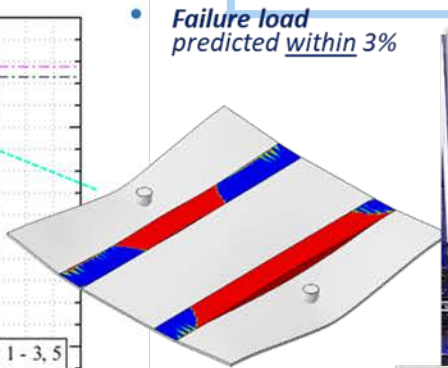
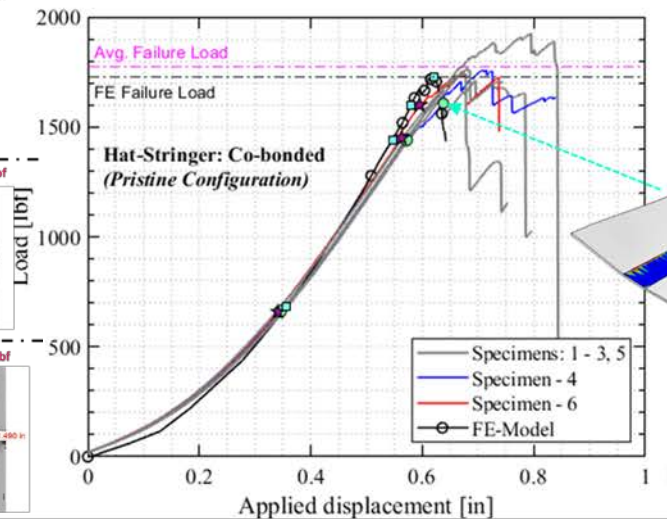


FEA

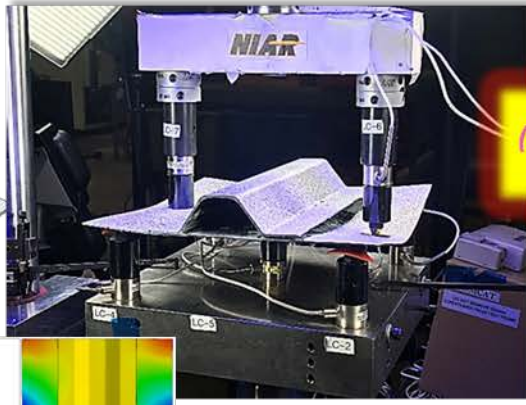
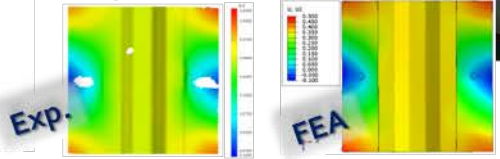


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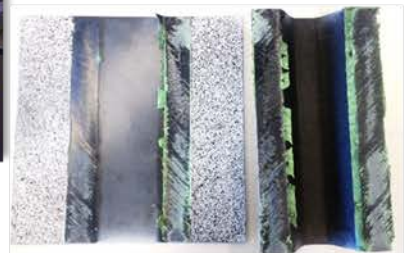
Co-Bonded HAT-Stringer (Pristine)



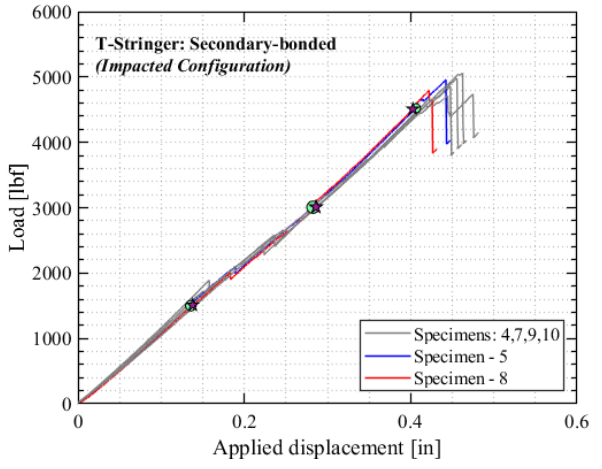
Failure load predicted within 3%



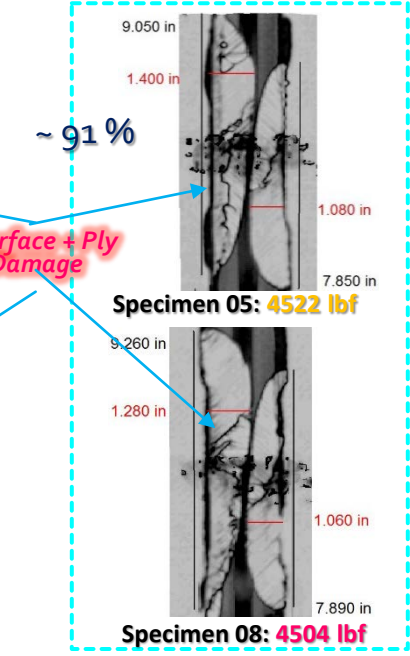
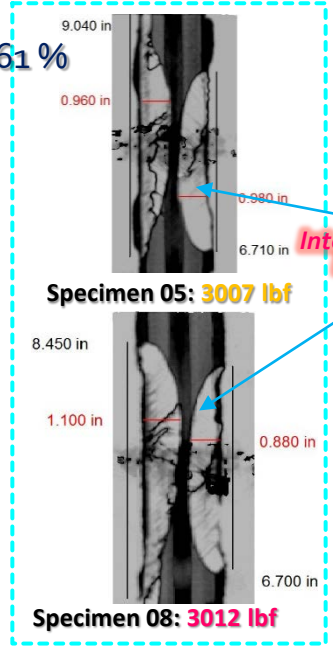
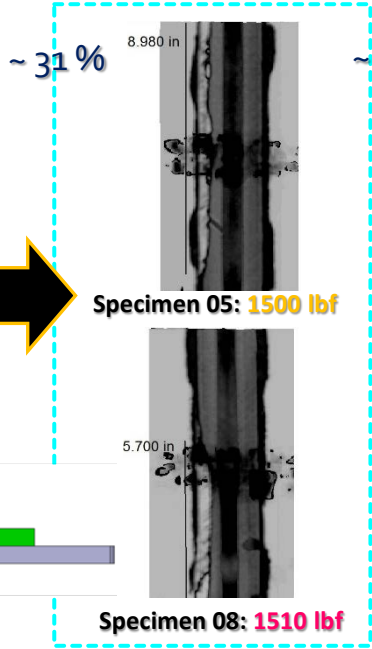
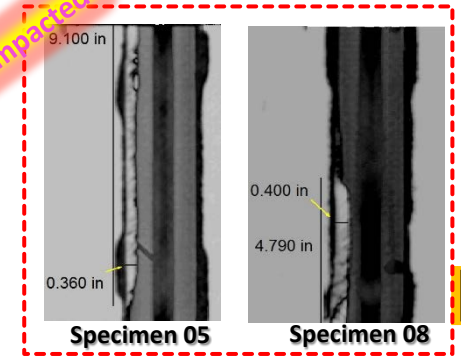
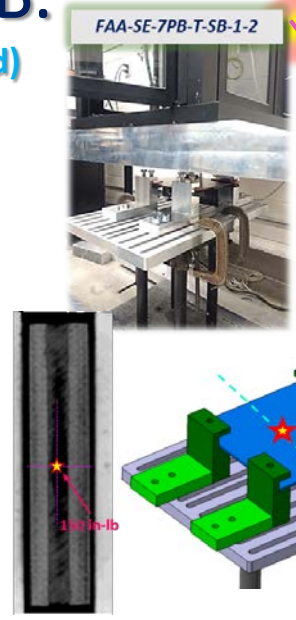
Skin/flange separation (cohesive failure w/ damage progression into first ply)



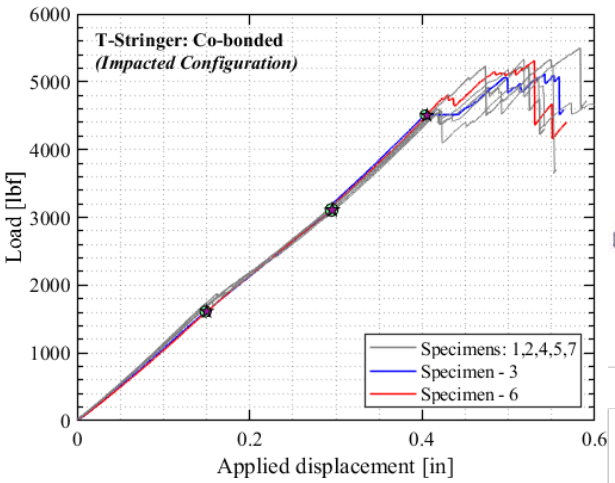
Impact Study w/ 7PB: Secondary-Bonded T-Stringer (Impacted)



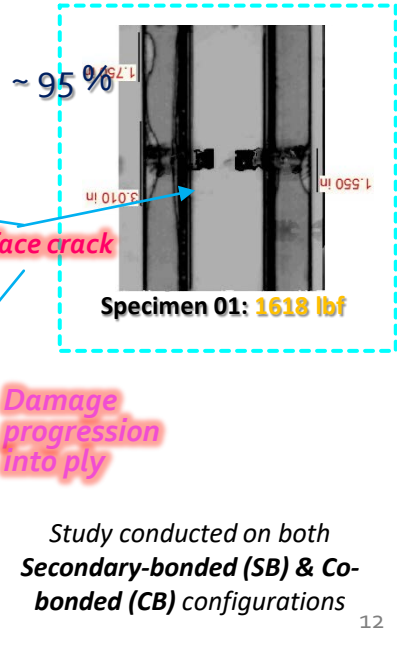
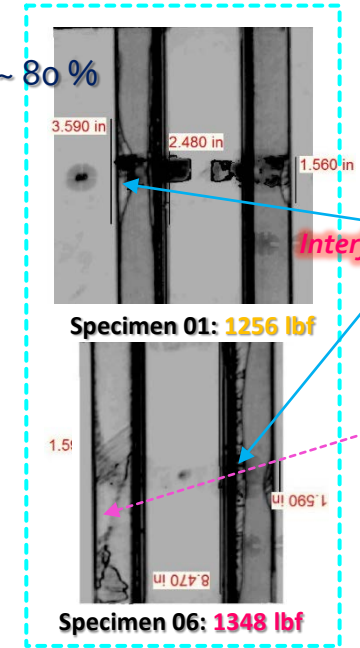
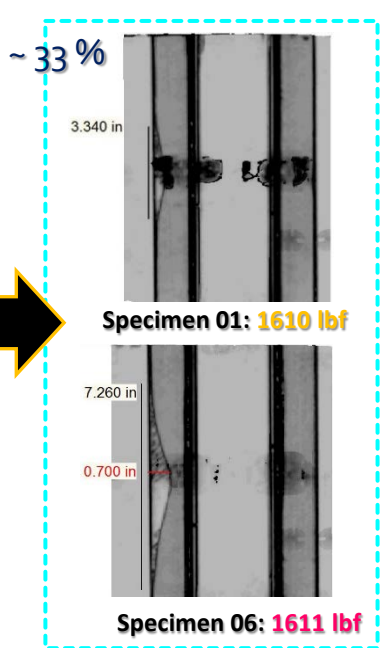
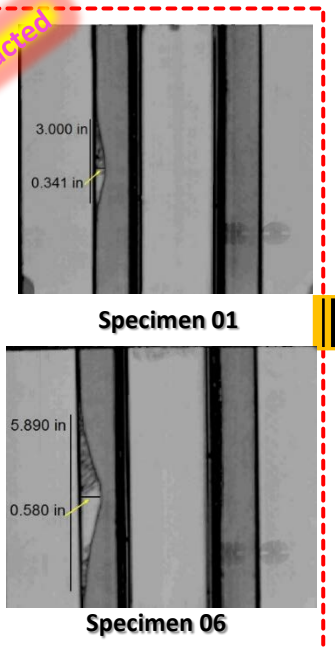
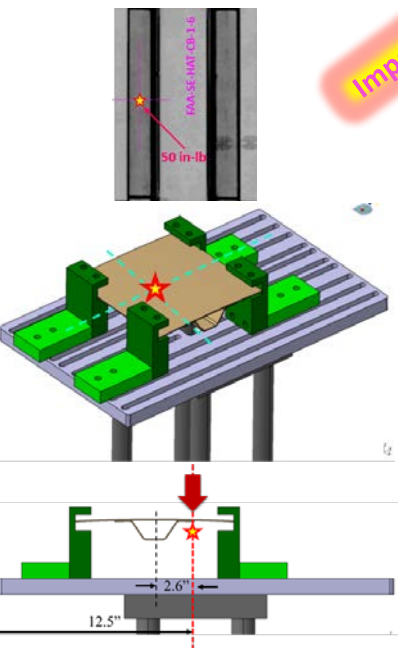
Avg. failure load = 4910.1 lbf



Co-Bonded HAT-Stringer (Impacted)



Avg. failure load = 1691.2 lbf



Study conducted on both Secondary-bonded (SB) & Co-bonded (CB) configurations



Program Overview



Mid-Level Building Block Test



“Smart” Mid-Level Building Block Test



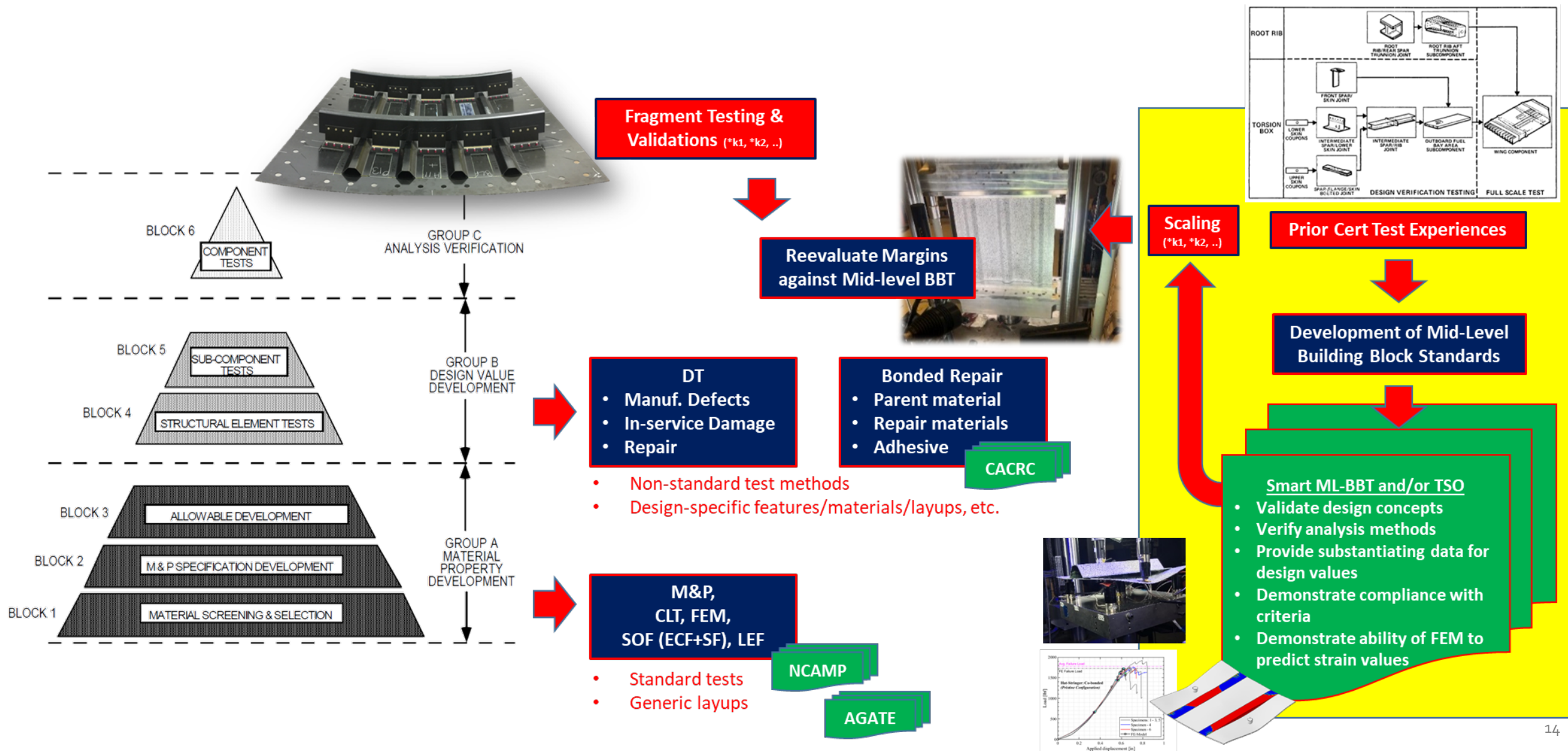
Test Performance Evaluation



Process & Scaling Effects

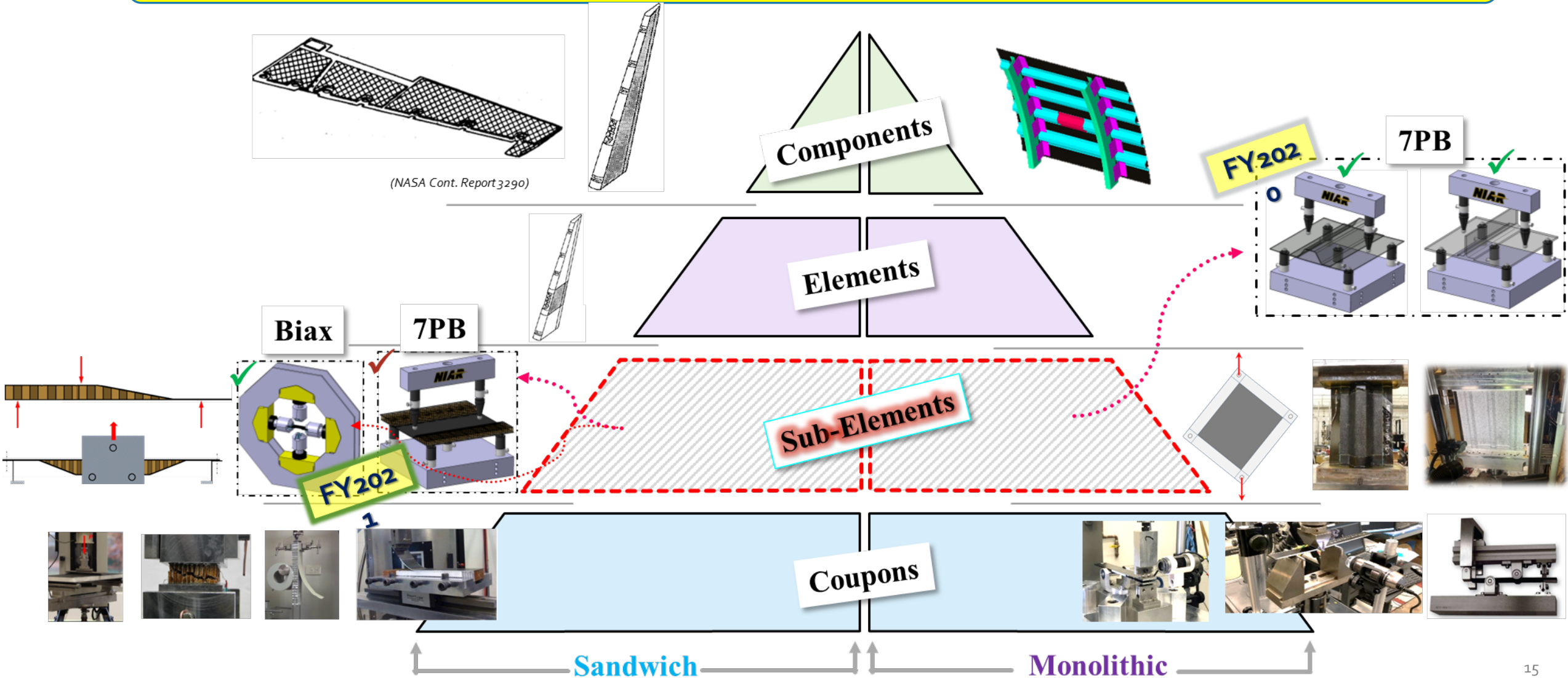


“Smart” Mid-Level Building Block Tests



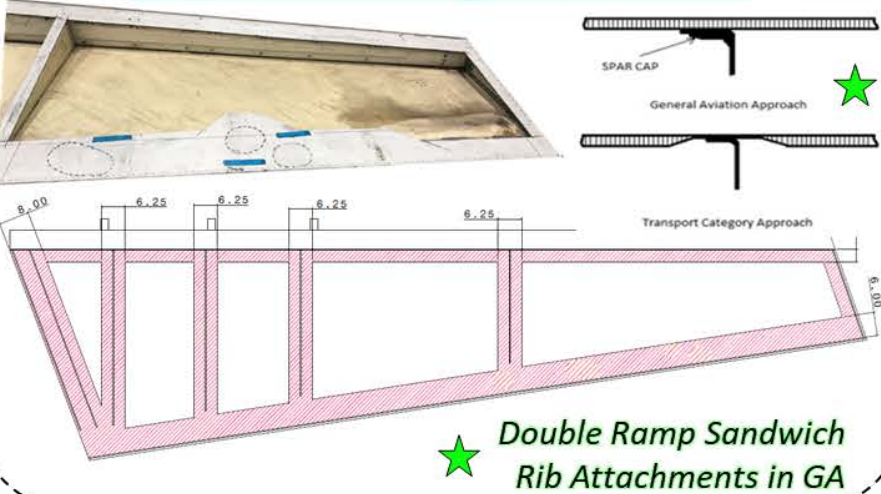
Overview of Current Test Methods: Scope for a Mid-Tier Test Methodology

GOAL: Identify *Weak Design* w/t Aid of selected Test Methodology which introduces *Complex Loading Scenario* (representative of an actual control surface).

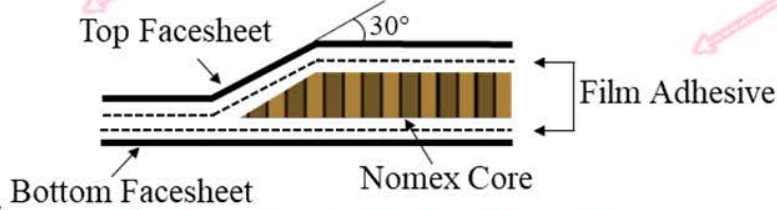
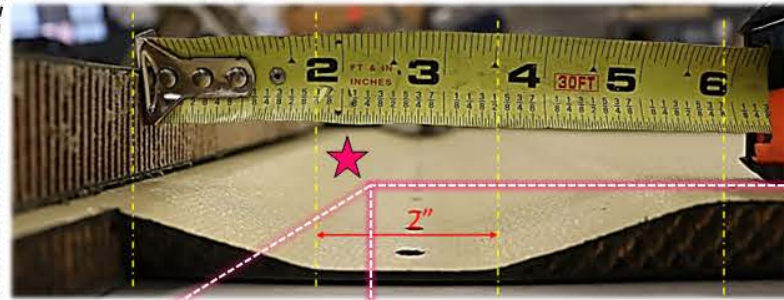


Analysis for Design Considerations in Sandwich Constructions

A. Structural Design Assessment

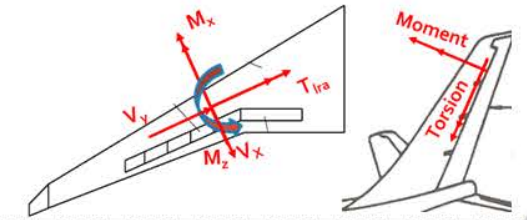


B. Critical Design Features

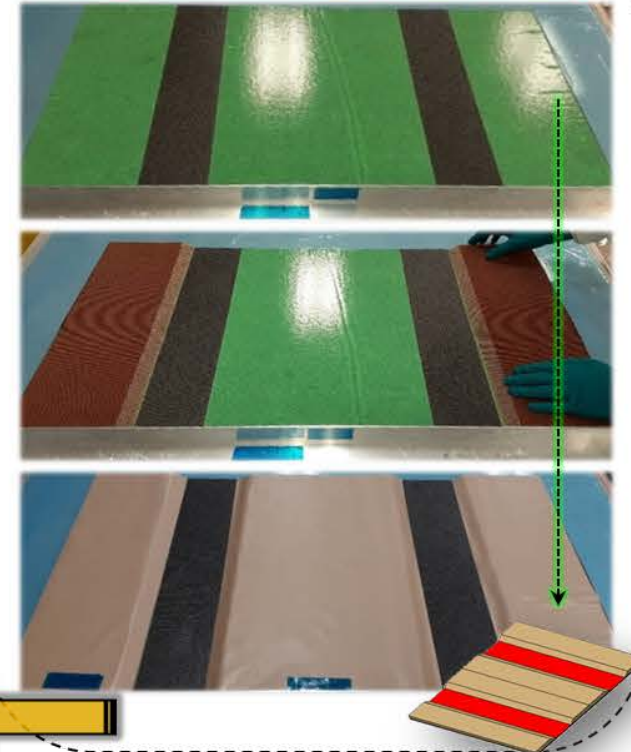


★ Ramp Angle, Radius, Materials, etc.

C. Loading Considerations

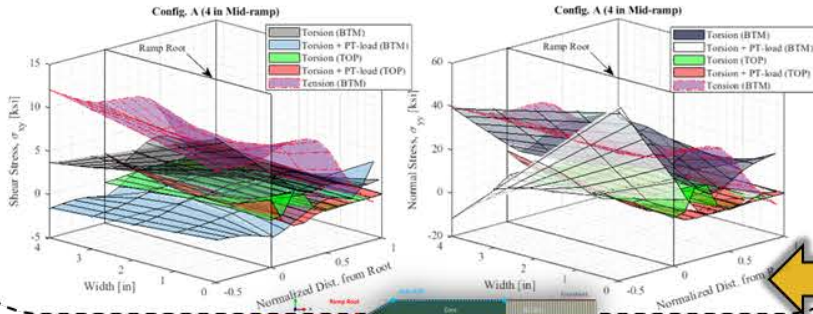
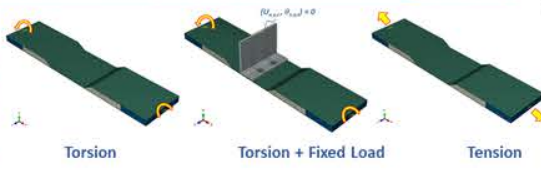


D. Specimen Design and Fab

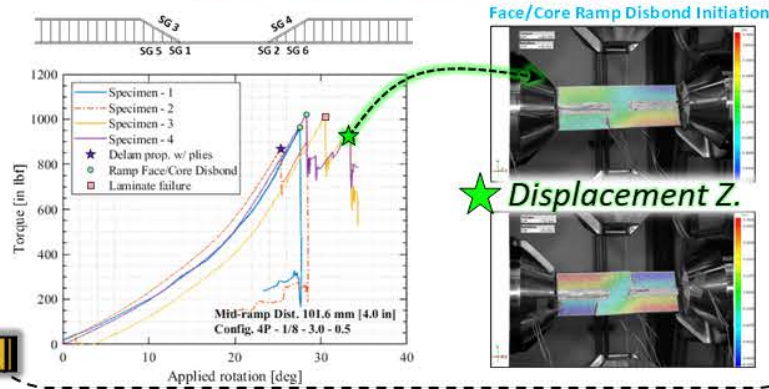


F. Interface Shear & Normal Stress Compared

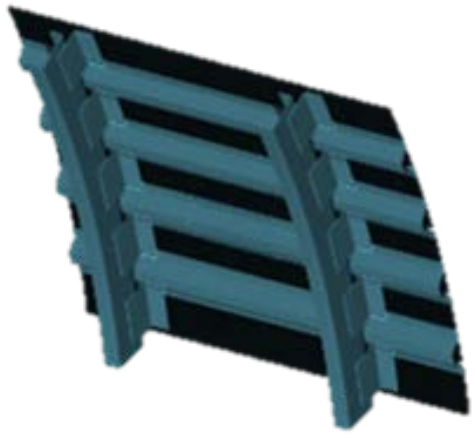
★ High asymmetrical shear and normal stresses in Torsion & Torsion + Pt. Load Case



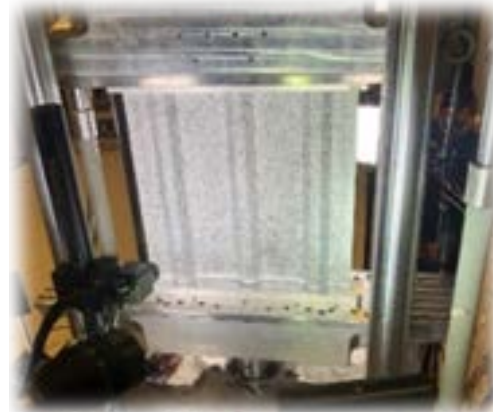
E. Mechanical Testing



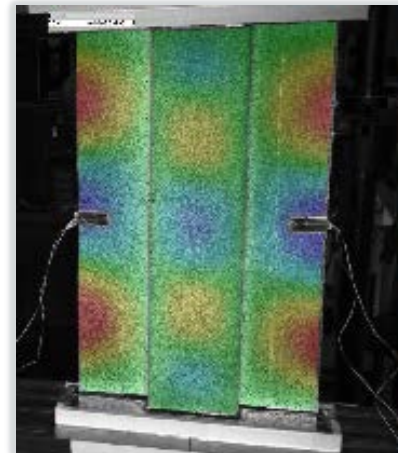
Evaluation of Fuselage Section: Top-Down Fragmented Testing



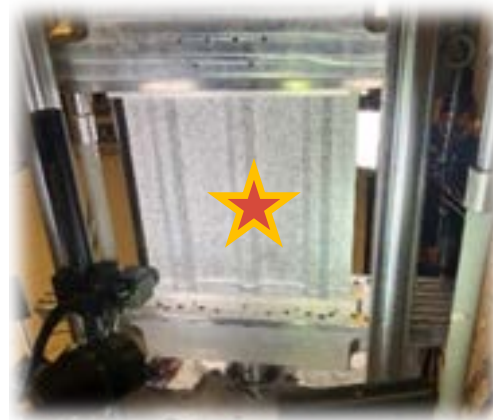
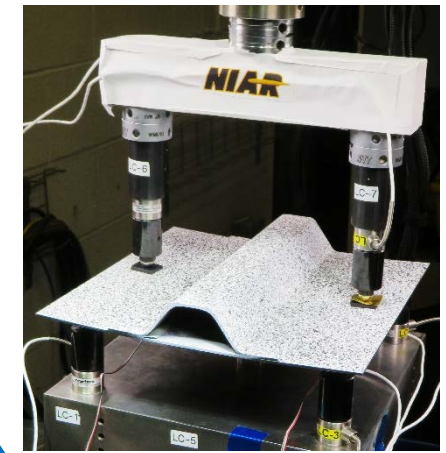
Defect Sensitivity = Low



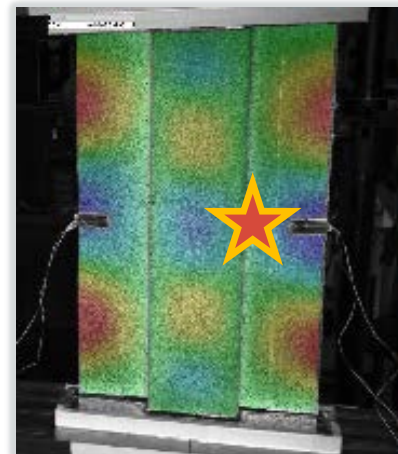
Defect Sensitivity = Medium



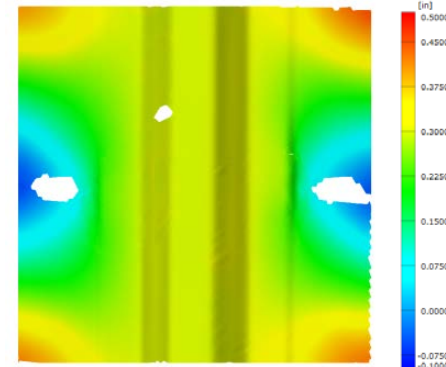
Defect Sensitivity = High



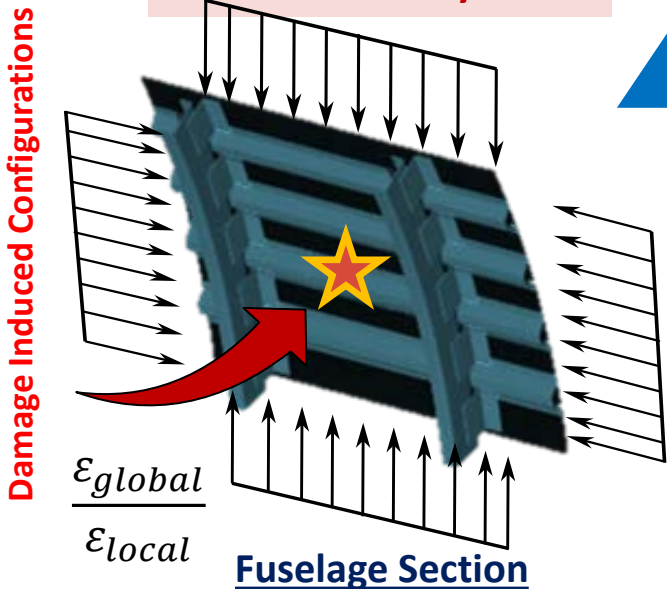
Multi-Stringer Compression



Single-Stringer Compression

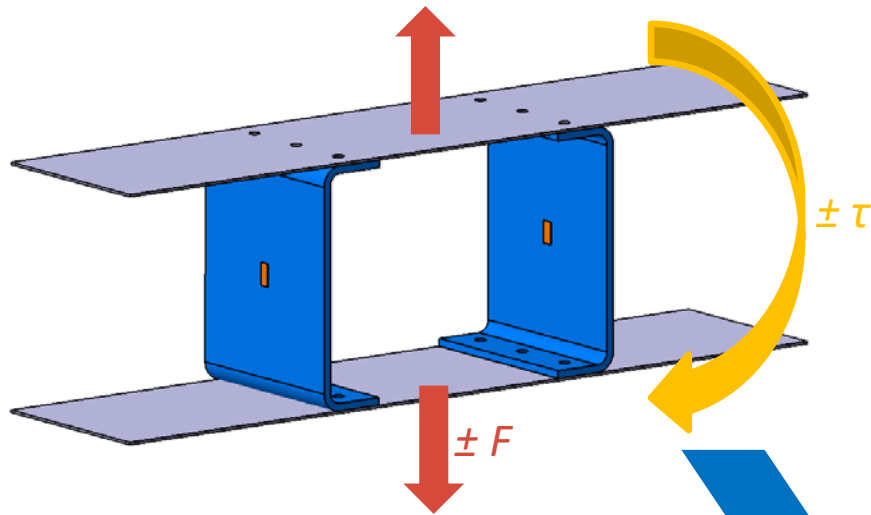


Skin/Stringer 7PB



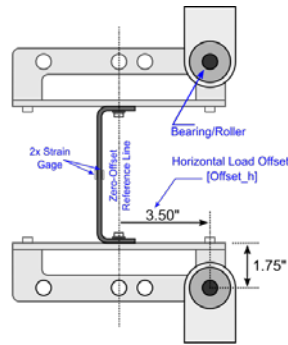
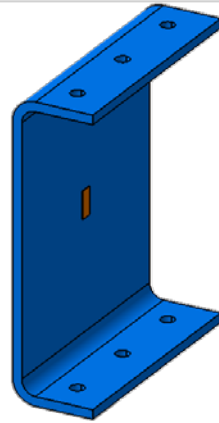
Conservatism in design based on lower-level allowable vs higher-level building block testing

Evaluation of Wing-Box Structure | Top-Down Fragmented Testing



Defect Sensitivity = Low

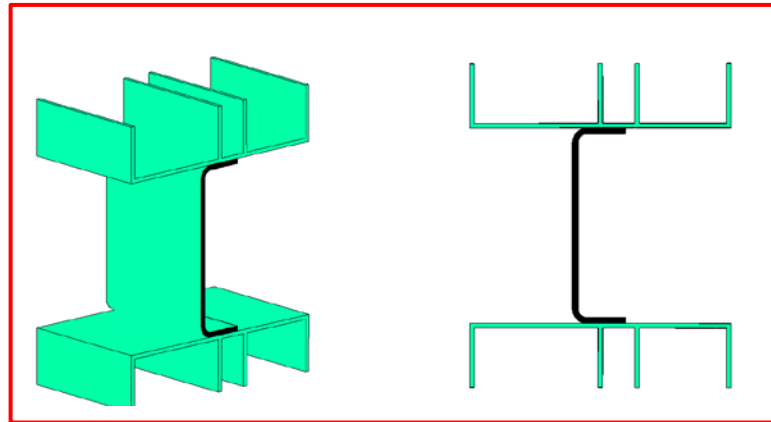
- Less Web Bending
- Complex/realistic loading



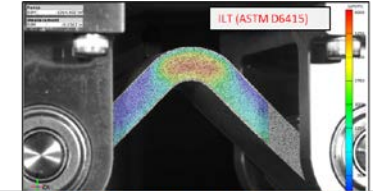
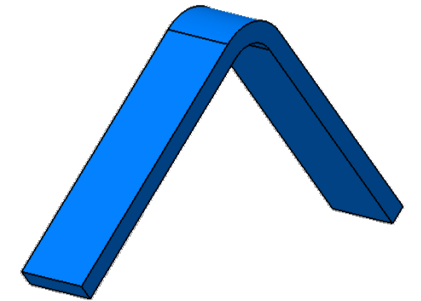
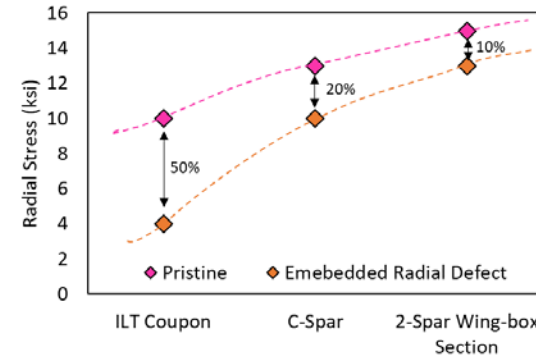
Material System	Horizontal Load Offset, Offset_h (in)			
IM7/5320-1	0.0"	1.0"	3.5"	-3.5"
IM7/5250-4	0.0"	1.0"	3.5"	N/A

Defect Sensitivity = Medium

- Excessive Web Bending!

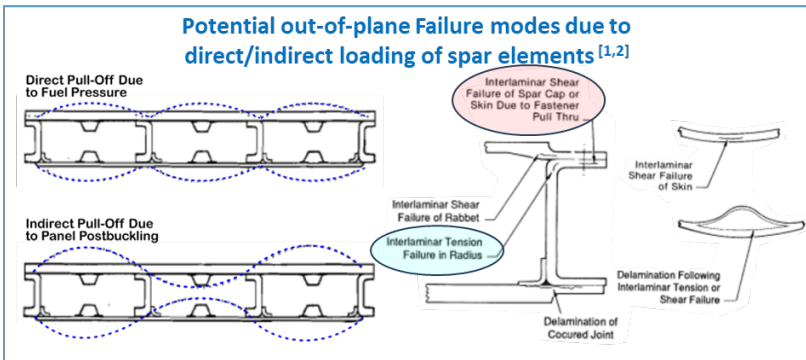
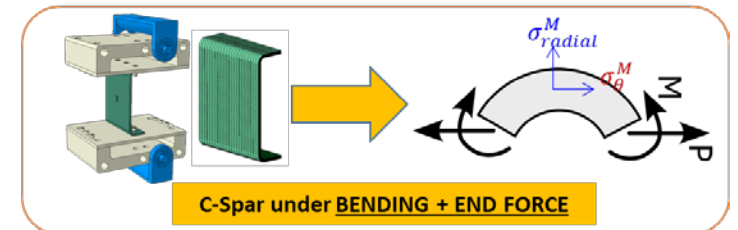
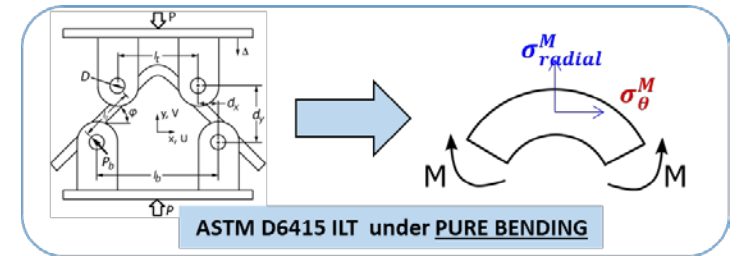


Vertical Displacement & Induced Rotation

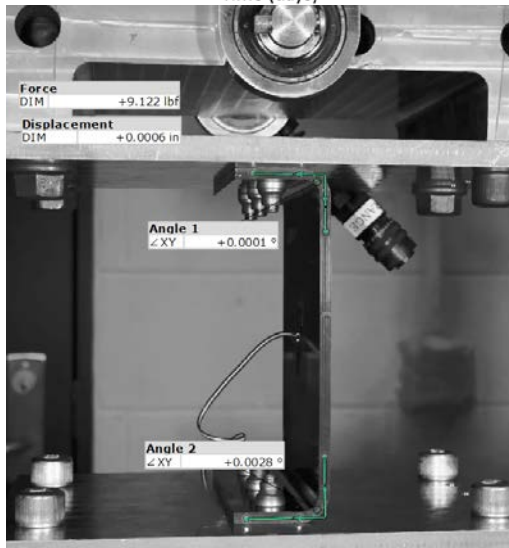
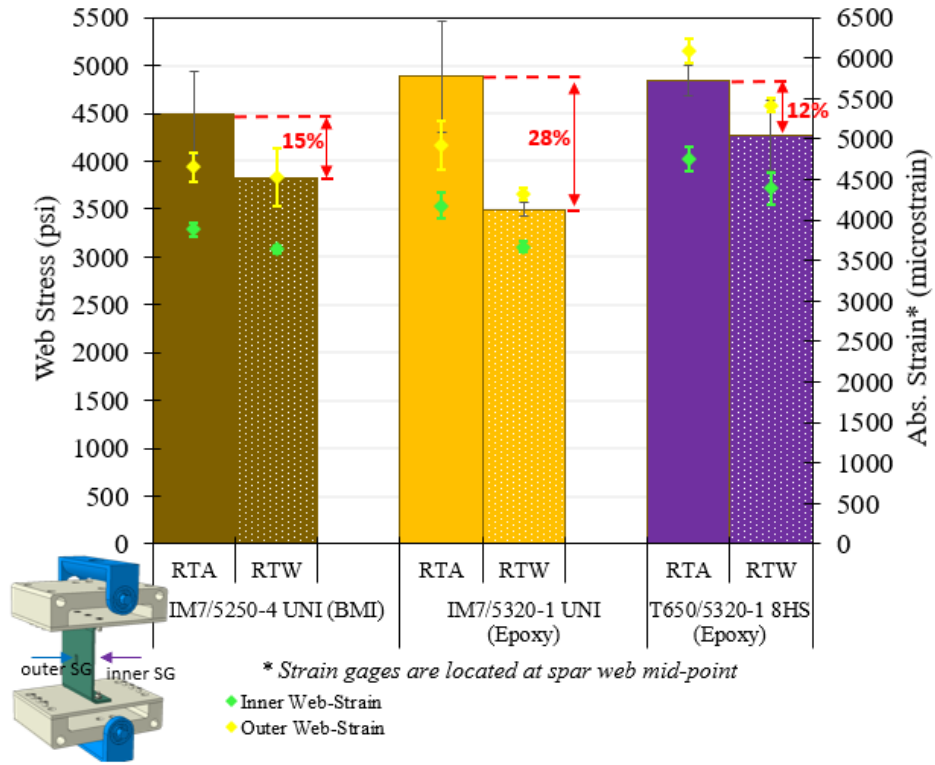
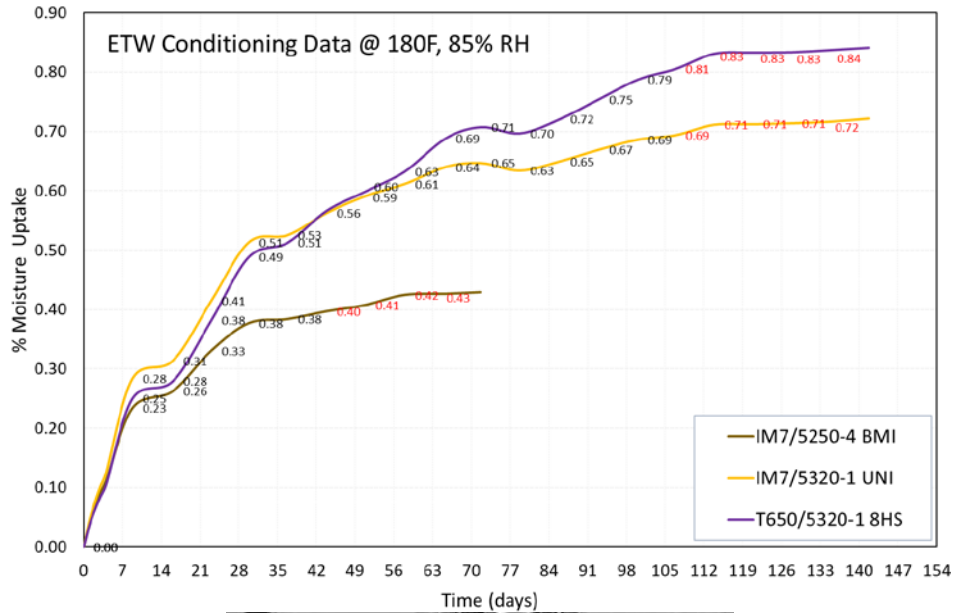


Uniform Strain distribution in typical ILT Specimen under bending. Centrally aligning peak ~ 30% though thickness (Hard Layup IM7/5250-4)

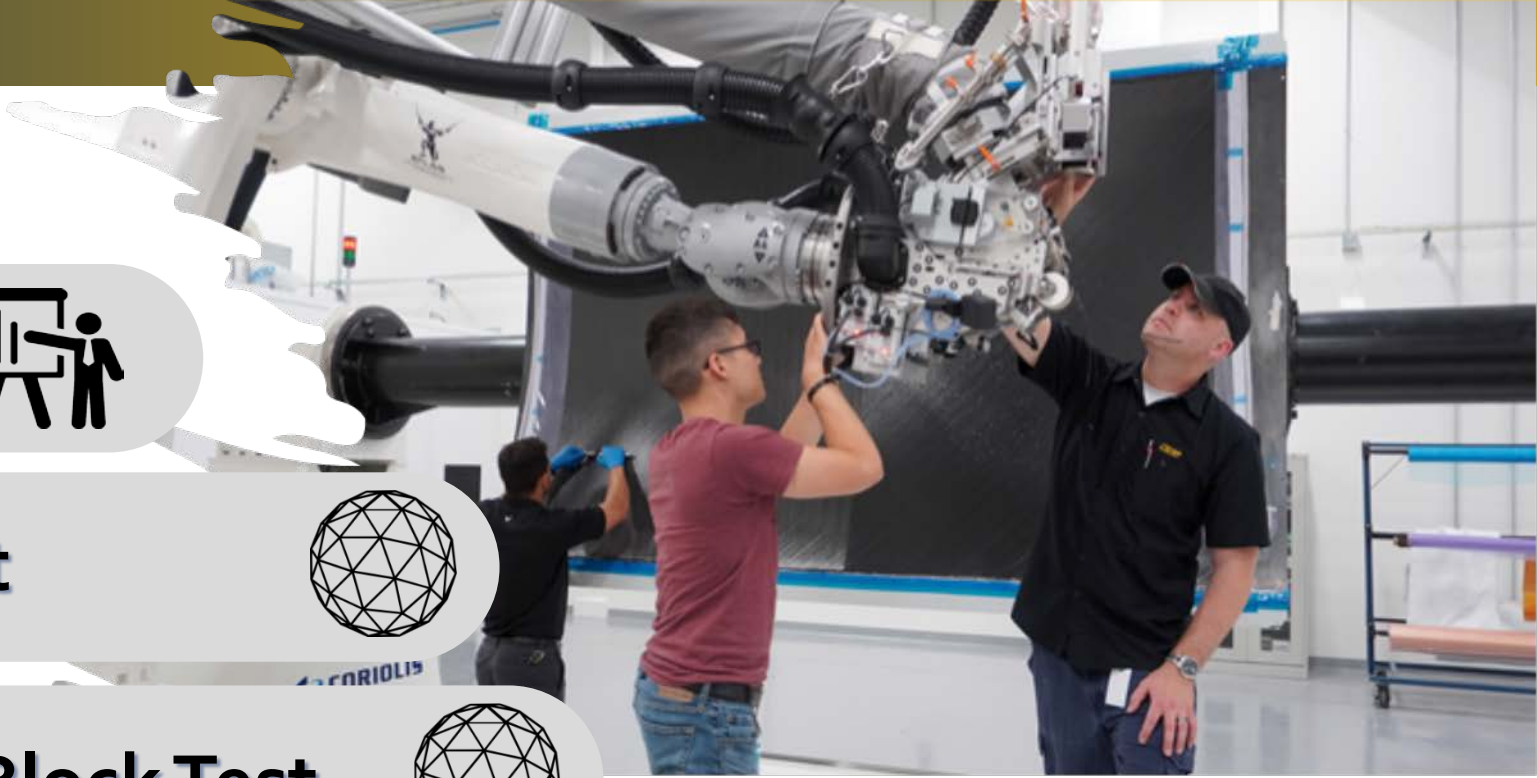
Defect Sensitivity = High



C-Spar Static – Environmental Conditioned and Tested @ RTA [RTW]



C-spars were preconditioned at 180°F, 85% RH and tested at room temp. Additionally, testing will be conducted at elevated temp. (220F) condition.



Program Overview



Mid-Level Building Block Test



"Smart" Mid-Level Building Block Test



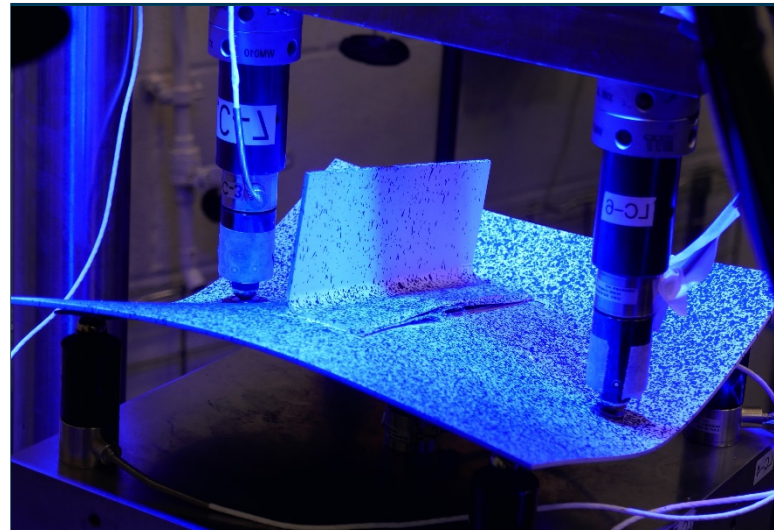
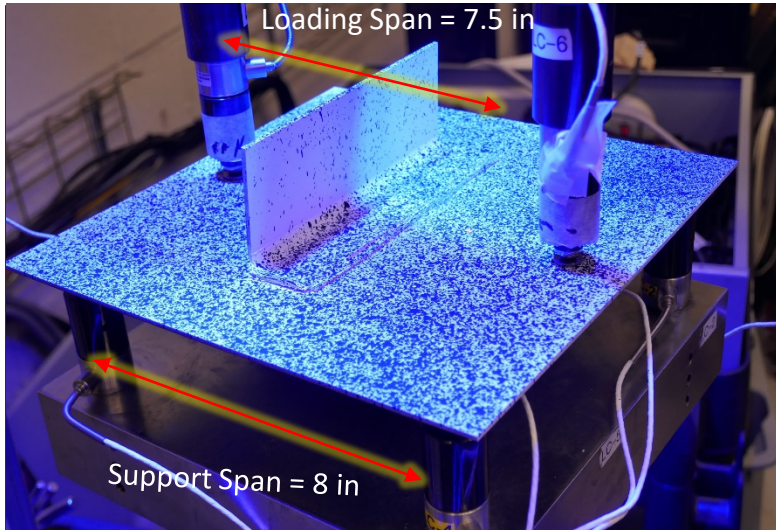
Test Performance Evaluation



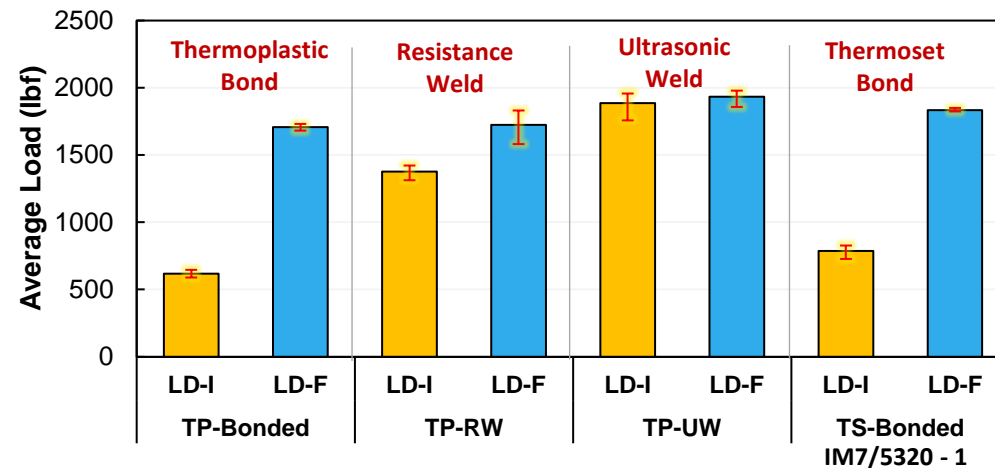
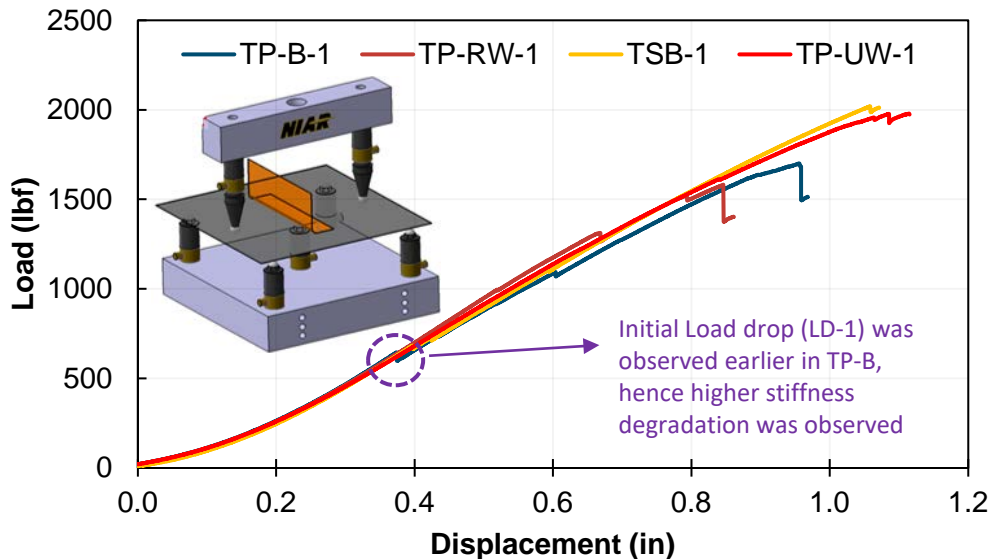
Process & Scaling Effects



7-Point Bend L-Shear Tie Configuration [TC1225/T700]



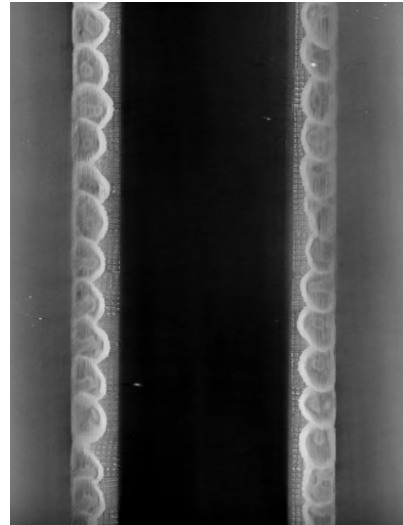
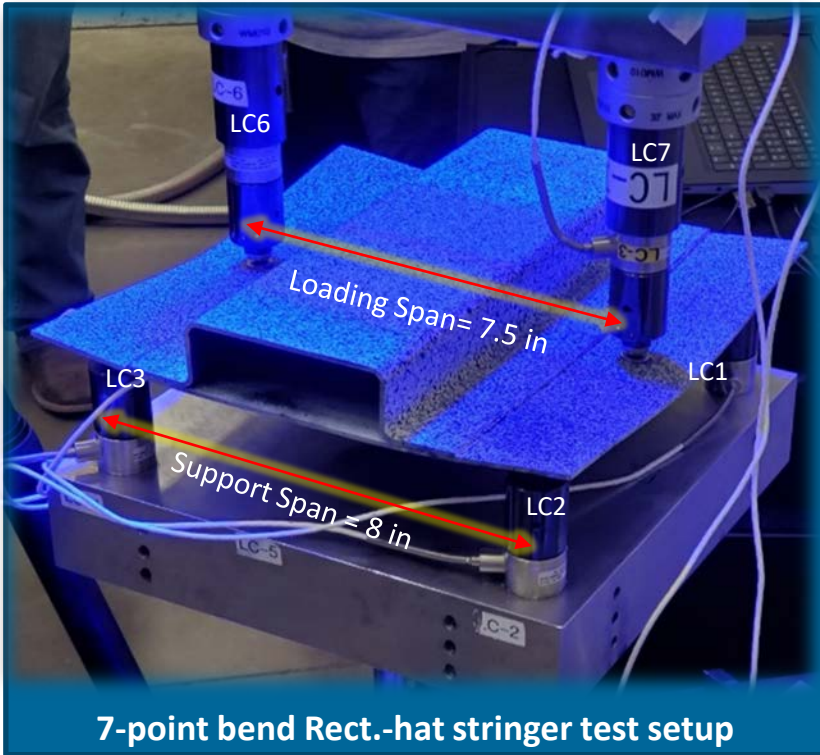
- 7PB replicates buckling modes akin to skin/stiffener compression via out-of-plane displacements
- Initial Load Drop was **higher** for Thermoplastic Weldment (TPW) than both TP and TS-Bonded
- Final Load Drop was similar for both TPW and TPB



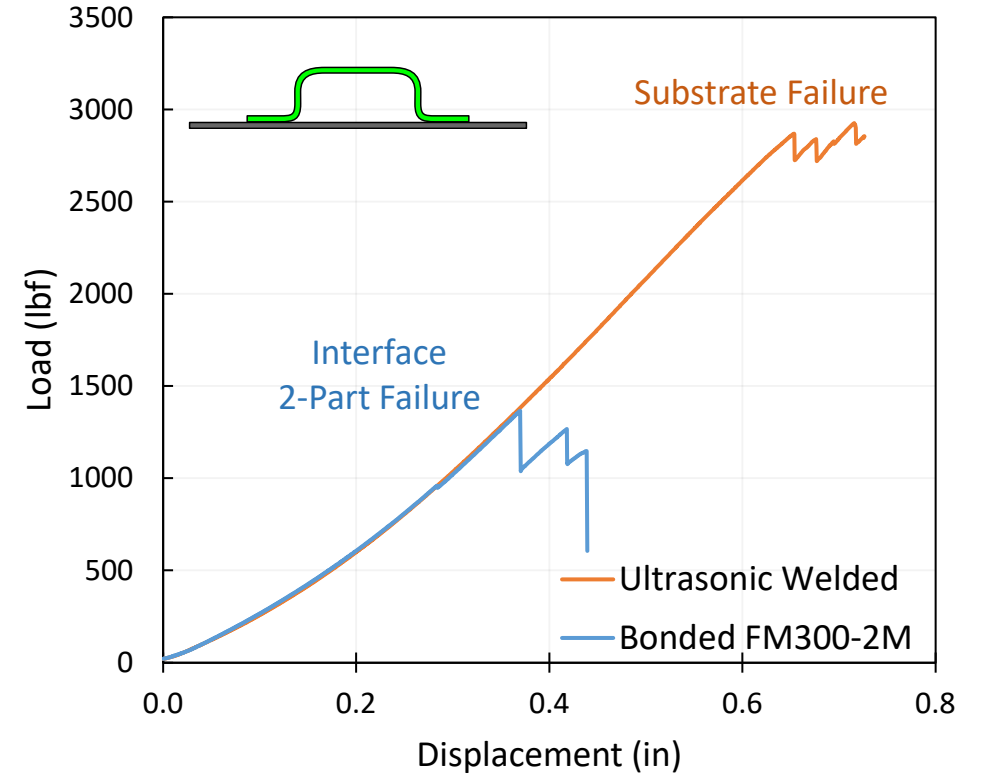
Initial Load Drop

Final Load Drop

7-Point Bend Rectangular-Hat Stringer [APC/AS4D]



XCT image of sequentially welded R-hat stringer stiffened skin at the interface

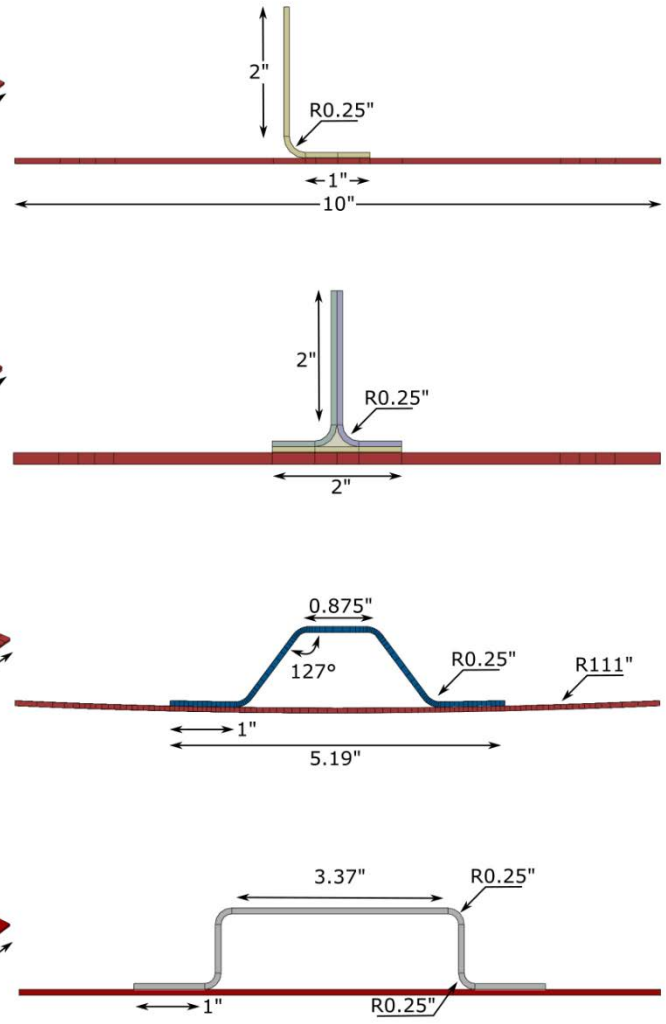
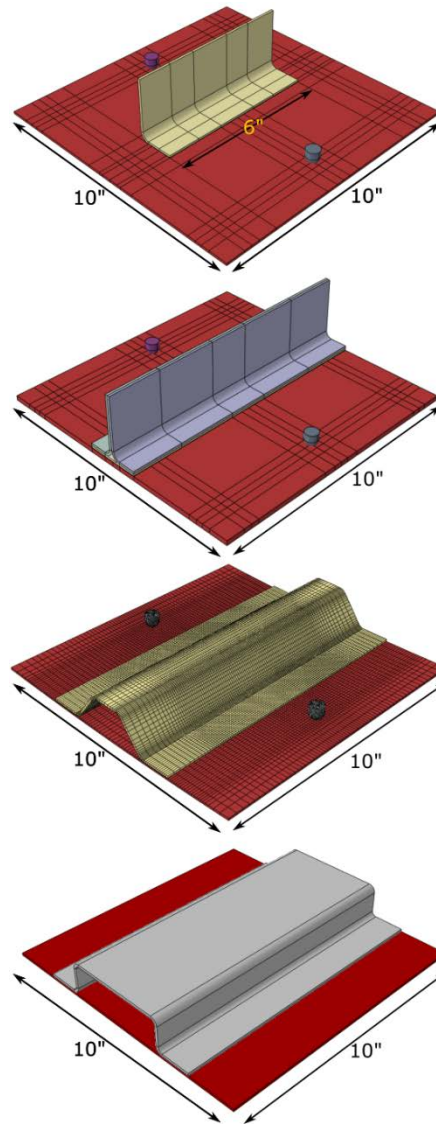
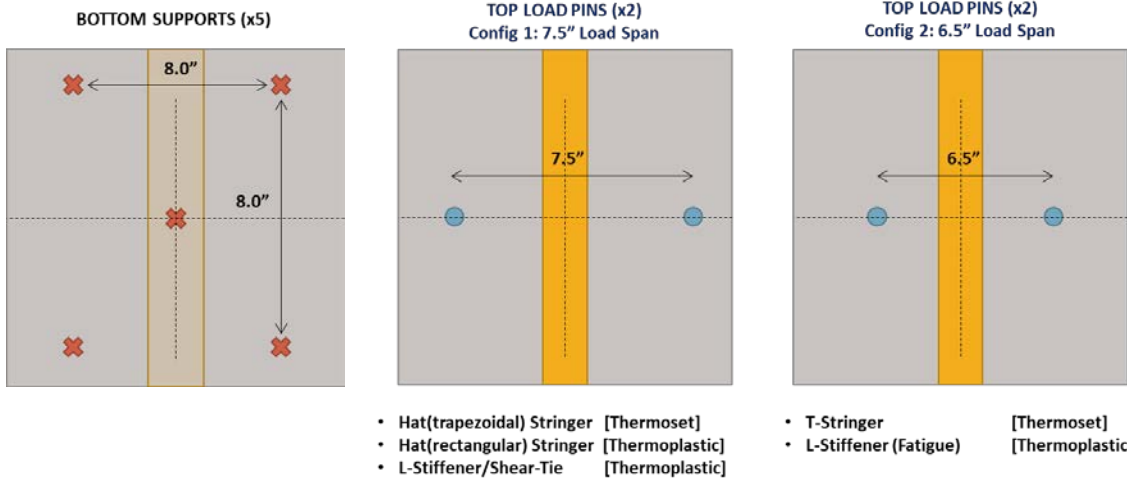


➤ **TP-UW** failed at **50% higher load** than TP-Bonded.

7PB Testing Configurations

TP – B : [FM300-2] Thermoplastic Adhesive Bond
 TS – B : [EA7000] Thermoset Adhesive Bond
 Secondary bonded unless specified as Co-bonded (Co)

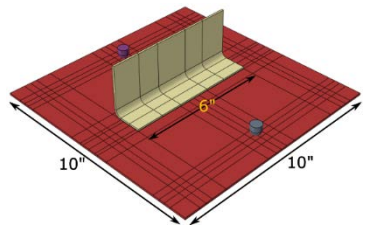
RW : Resistance Weld (TP)
 UW : Ultrasonic Weld (TP)



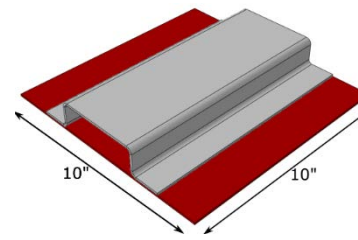
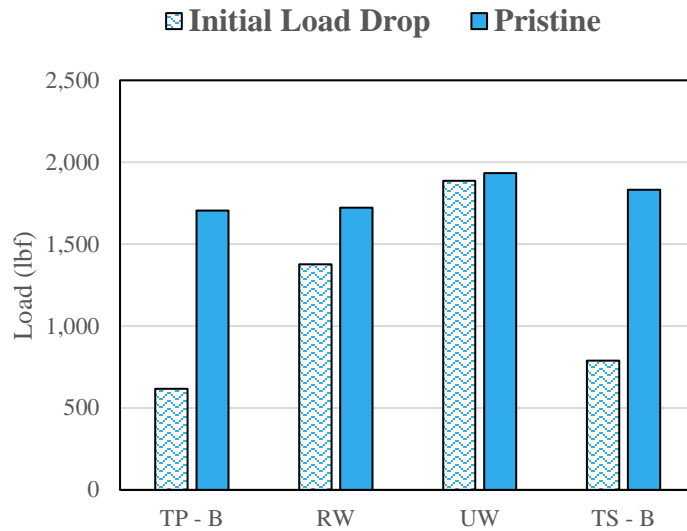
Configuration	Material	Interface	Adhesive	Static		
				Pristine	Pre-Crack	Impacted
T-Stiffener	Thermoset [T800/3900-2]	Co-Bonded	EA 7000	X	X	X
		Secondary-Bonded		X	X	X
Co-Bonded		X		X	X	
Secondary-Bonded		X		X	X	
Hat-Stiffener with curved Skin (Omega Hat Configuration)	Thermoplastic [APC/AS4D] [TC1225/T700]	Bonded	FM 300-2	X		
		Fusion by Weldment		X		
L-Stiffener/Shear Tie	Thermoplastic [APC/AS4D] [TC1225/T700]	Bonded	FM 300-2	X		
		Fusion by Weldment		X		

**** Pre-Crack = 2" x 1" Disbond Region Centrally on Each Flange**

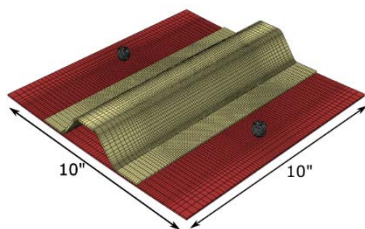
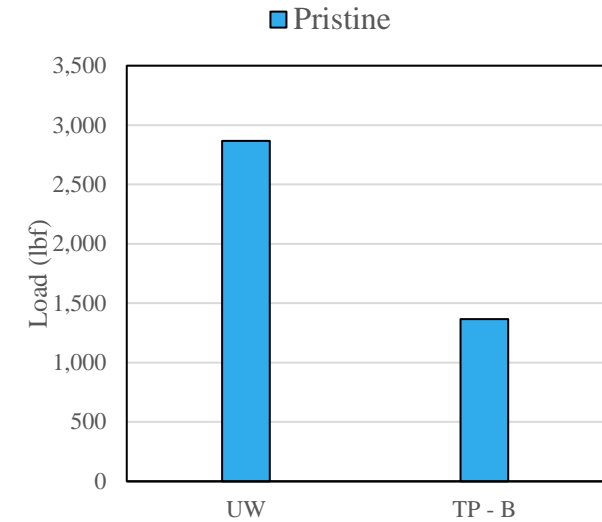
7PB Performance – Materials, Configurations & Joining Methods



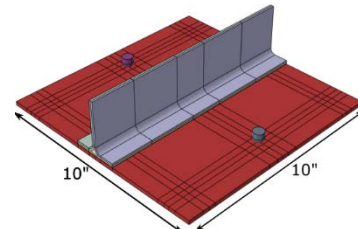
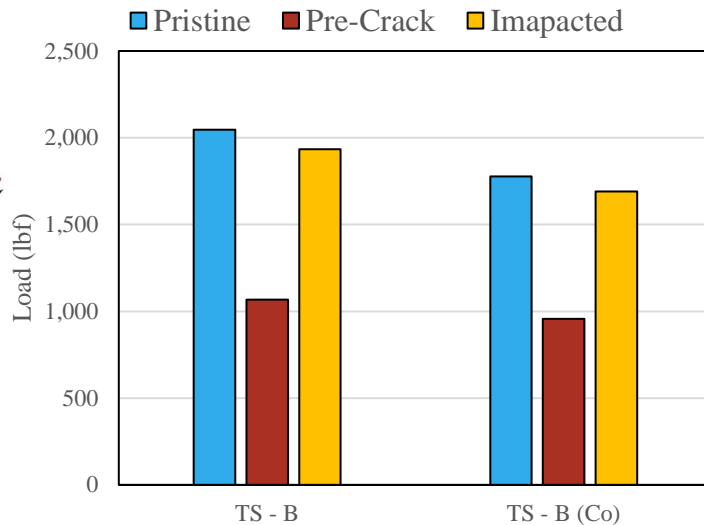
Layup / Ply	16 QI
Material	TC1225/T700 IM7/5320-1
Adhesive	FM300-2M
Load Distance	7.5"



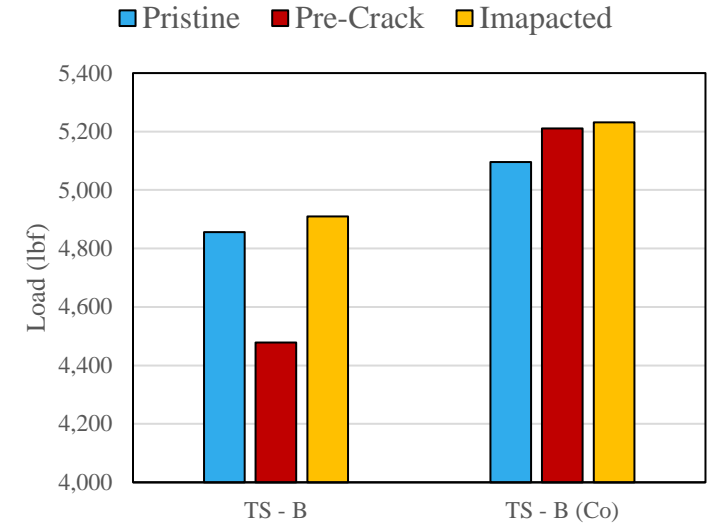
Layup / Ply	16 QI
Material	APC/AS4D
Adhesive	FM300-2M
Load Distance	7.5"

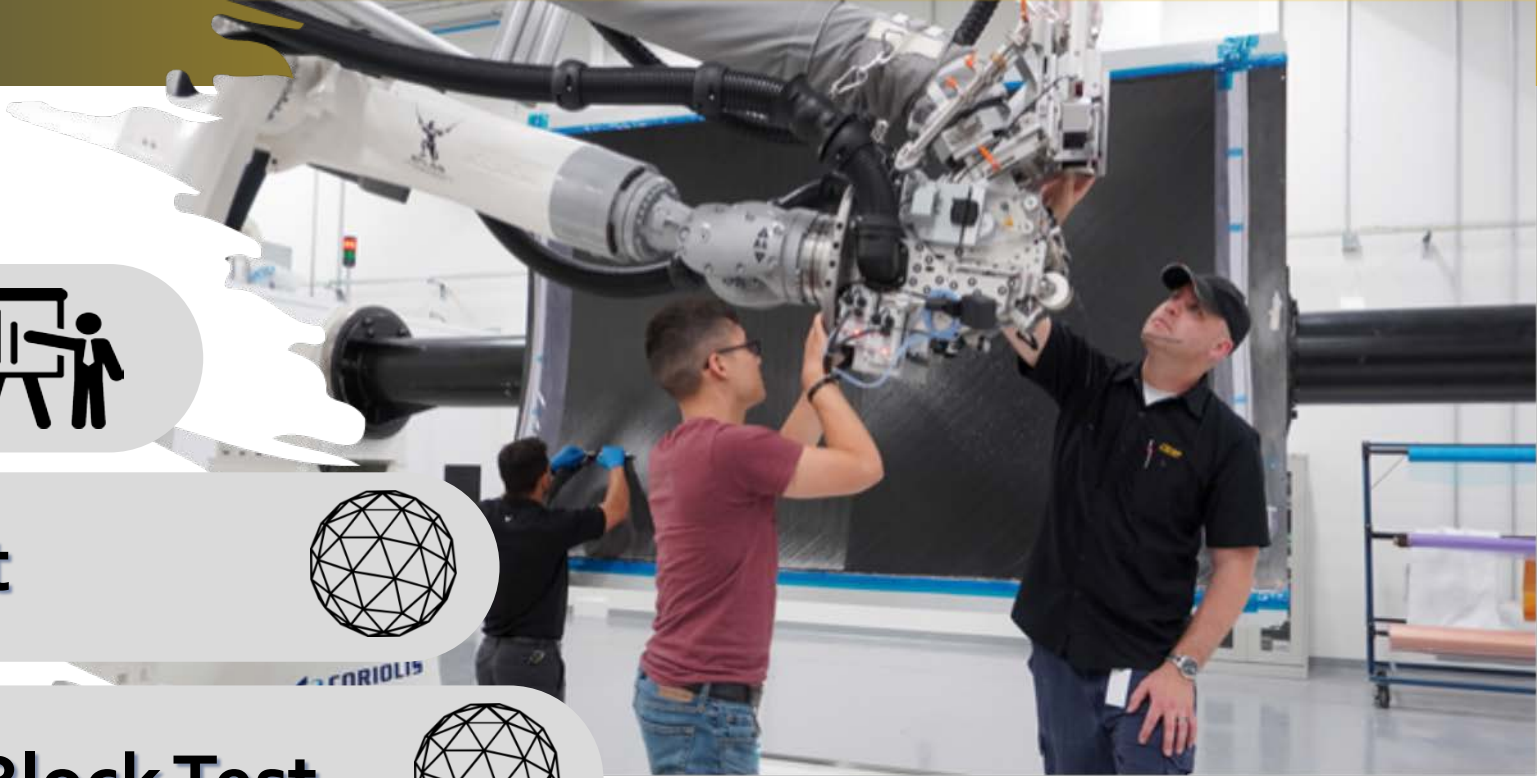


Layup / Ply	10/11 Plies
Material	T800/3900-2
Adhesive	EA7000
Load Distance	7.5"



Layup / Ply	24 QI
Material	T800/3900-2
Adhesive	EA7000
Load Distance	6.5"





Program Overview



Mid-Level Building Block Test



"Smart" Mid-Level Building Block Test



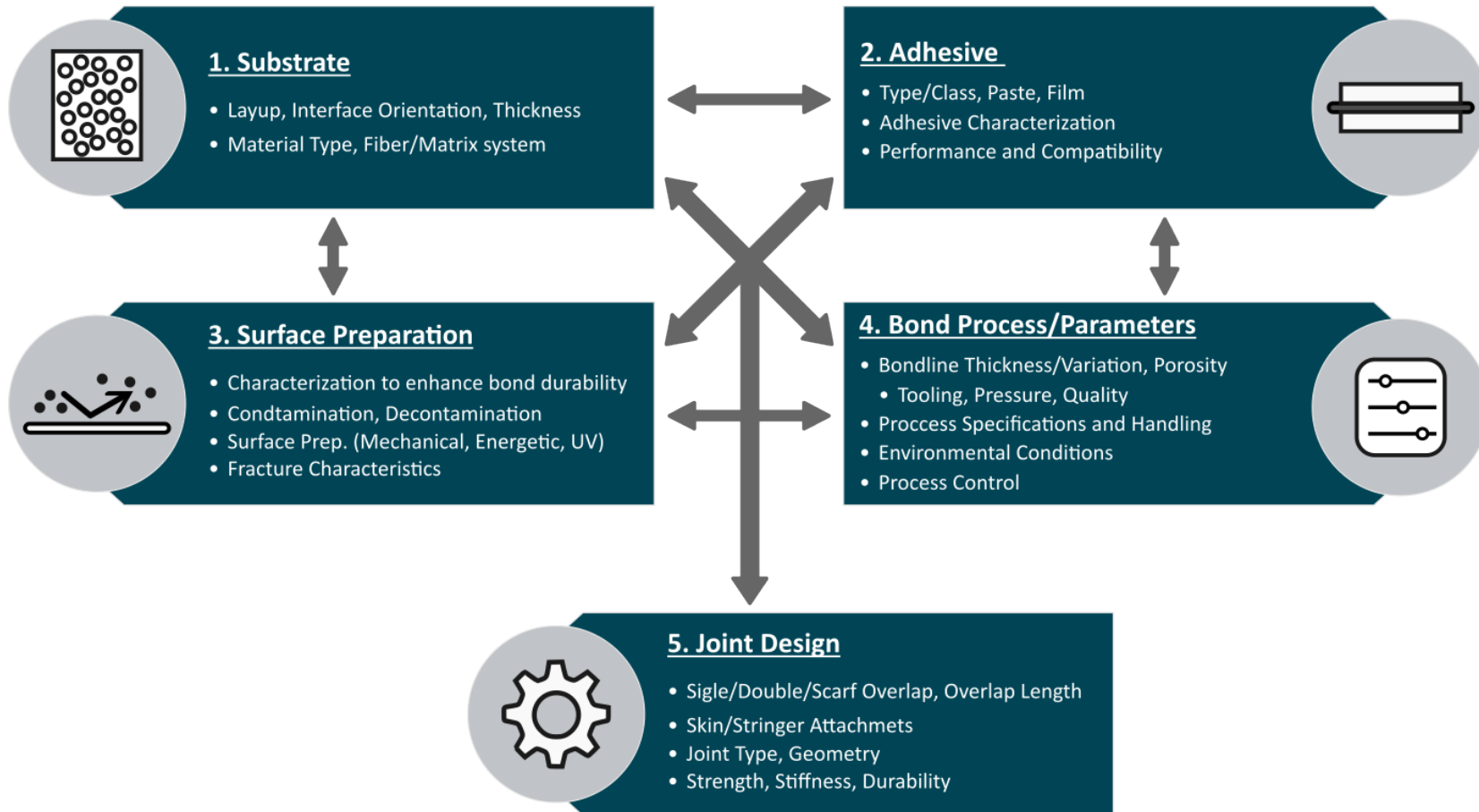
Test Performance Evaluation



Process & Scaling Effects



Adhesive Joints as a System



Key Characters for Joint System

- **Substrate Material/Configuration**
- **Adhesive Type and Compatibility**
- **Surface Preparation Methods**
- **Surface Contaminants**
- **De-contamination Methods**
- **Environmental Conditions**
- **Mfg. Procedure (Co/Sec. Bond)**
- **Joint Design, Load Cases/Intensity, Mode Mixity Ratios**

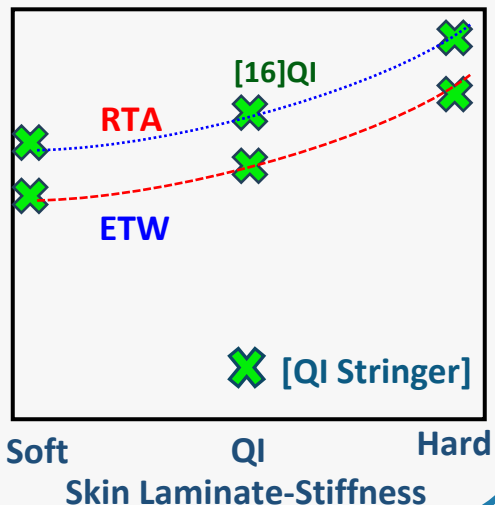
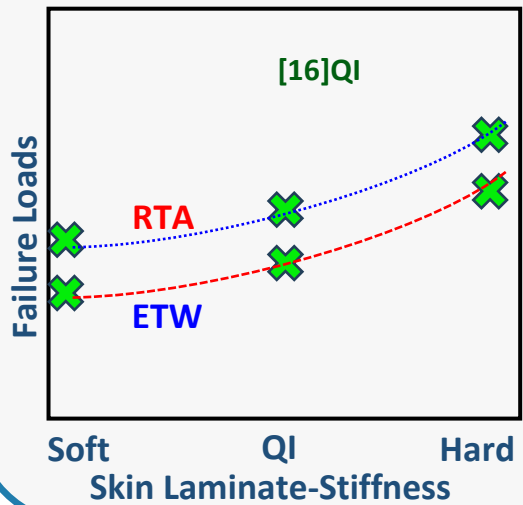
Bond Process Qualification at Scale – 7 pt Bend Test

Joint-System	Key Parameters	#1	#2	#3
1. Substrate	Substrate Material	IM7/5320-1	Thermoplastic	
	Substrate Config.	Soft	QI/Custom	Hard
2. Adhesive/Interface	Adhesive	FM300-2 (film)	EA9394 (paste)	
	Surface Preparation	Mech. Abrasion	Energetic (APT)	UV Ablation
3. Surface Preparation	Surface Contamination	Pristine	Contaminant	
	Process	Co-Bonding	Secondary Bonding	
4. Bond Process	Process	Co-Bonding	Secondary Bonding	
5. Design Feature	Joint Desing	Hat-Stiffener (Omega)	T-Stiffener	
Conditioning	Test Environment	RTA	ETW/Moisture	

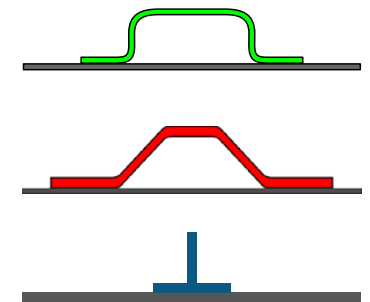
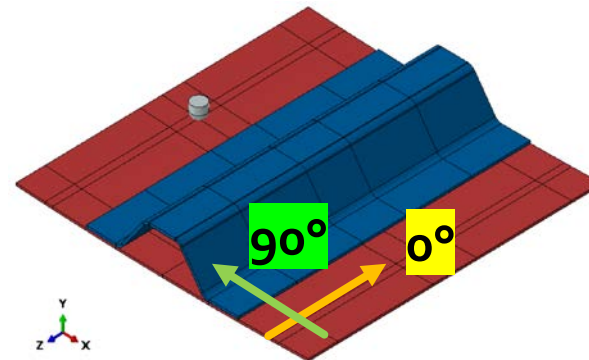
[Secondary Bonding]

[Mech. Abrasion]

[Energetic (APT) Prep.]



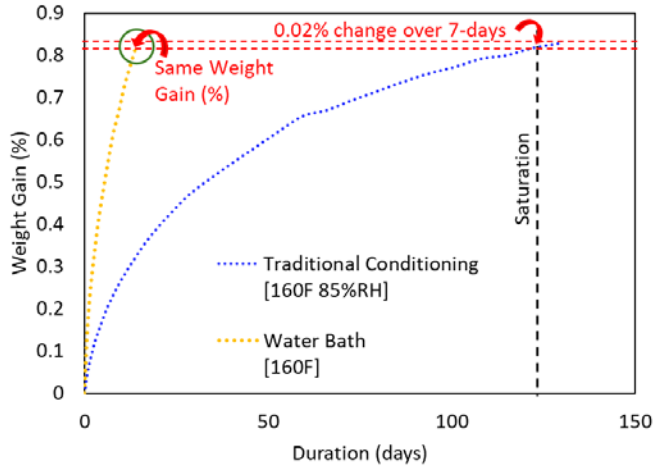
Config.	Layup	Stack-up	Distribution
Hard	[45/0/-45/0/90/0/45/0]_S	16	50% 38% 13%
QI	[45/0/-45/90]_2S	16	25% 50% 25%
Soft	[45/-45/0/45/-45/45/-45/90]_S	16	13% 75% 13%



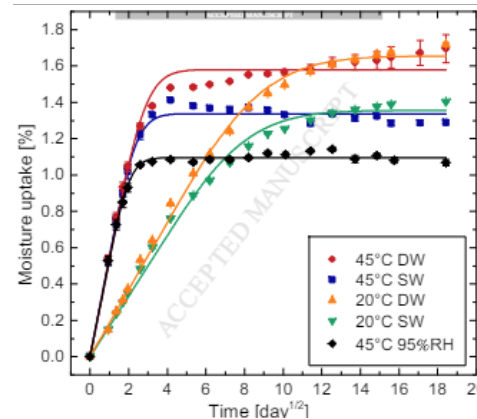
Environmental Conditioning (Moisture Saturation)

Moisture Saturations for Environmental Testing

- Effects due to moisture ingress
- Challenges with conditioning time for larger test articles
 - Bondline region saturation
- Evaluation of **Accelerated** Conditioning Approach
 - Humidity/Temperature dependence
 - Water Immersion

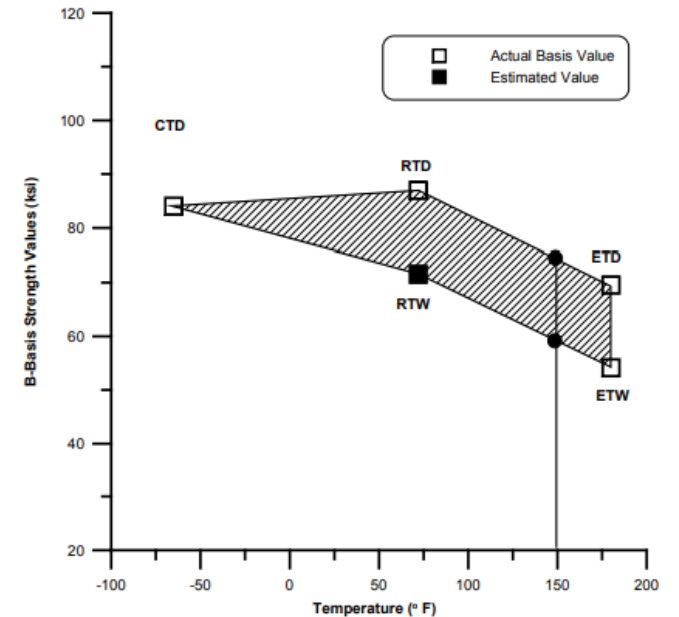


Traveler Coupons from bonded flange region to evaluate saturation rate during environmental conditioning
Traveler mass ≈ 10 g



ASTM D5229 - Moisture Absorption Properties & Equilibrium Conditioning of PMC

5.5 Vapor-exposure testing shall be used to condition the specimen when the in-service environmental condition is a vapor such as humid air. Immersion in a liquid bath should be used to simulate vapor exposure only when apparent absorption properties are desired for qualitative purposes. Properties determined in the latter manner shall be reported as apparent properties.



Tomblin, J., et al. 2001, B – Basis Design Allowables for Epoxy – Based Prepreg, Faberite 8-Harness Graphite Fabric T650 3k-135-8H / 7740

<https://agate.niar.wichita.edu/Materials/WP3.3-033051-102.pdf>

Tomblin, J., et al. 2002, A – Basis and B – Basis Design Allowables for Epoxy – Based Prepreg,

www.niar.wichita.edu/agate/Documents/Materials/WP3.3-033051-136_Rev.1.pdf

Heshmati, M., Haghani, R., & Al-Emrani, M. (2016). Effects of moisture on the long-term performance of adhesively bonded FRP/steel joints used in bridges. Composites Part B: Engineering, 92, 447–462.

Summary

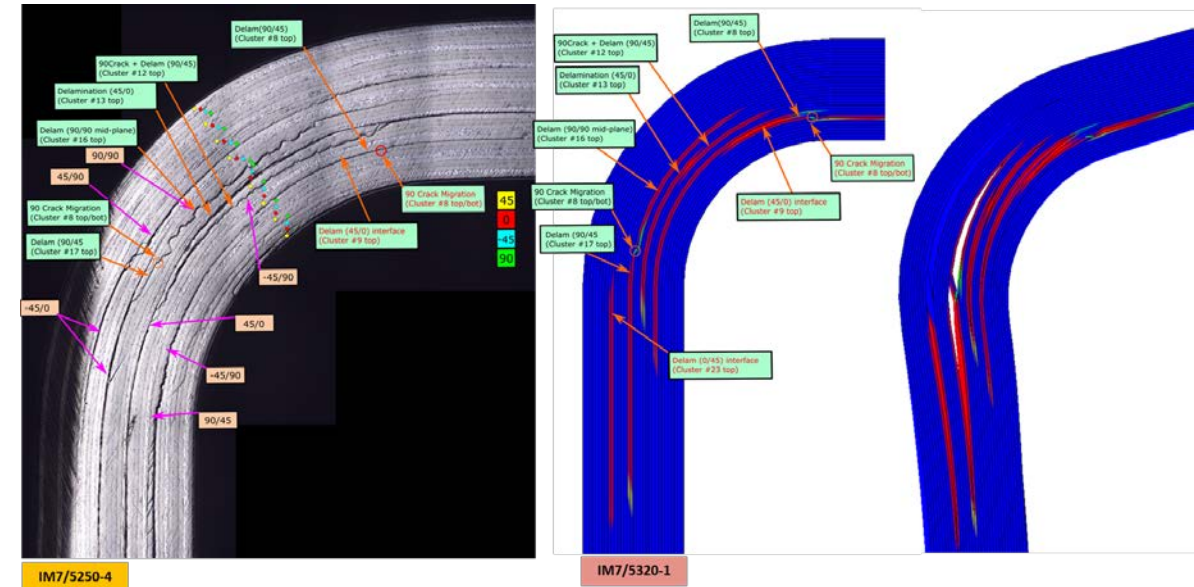
Testing & Evaluation

- The 7PB test methodology was showcased as **robust & reliable test method** for evaluation of monolithic/bonded joints (Findings were presented to the ASTM D30 sub-committee on March 2021)
- Development of 7-point bend test as a (ASTM) **standard for evaluating the sensitivity of design features and material/processes for manufacturing defects and potential aging threats at early stages of design with sufficient load complexity** without the use of costly & time-consuming structural tests
- Top-Down approach to evaluate design conservatism when based on lower-level allowables



Analysis Validations

- Expand the **continuum damage modeling** and validations for **structural details** (secondary bonds, co-bonds, and co-cured hat- and T-stiffeners)
- **Discrete damage modeling** using regularized extended finite element analysis (ReFEM) for investigating competing failure modes and crack migration.



Looking Forward / Future Work

- Benefit to Aviation
 - Development of a test methodology to evaluate various design aspects at early stages of the design and manufacturing process to mitigate risks
 - Understanding of scaling effects and design factors (scatter factor, environmental compensation factors)
- Next Steps:
 - Complete 7-point bend testing of bonded and welded thermoplastic joints (bond process qualification at scale)
 - Experimental evaluation of component-level fuselage section and fragmented testing
 - Continued discussions with ASTM D30 about the possibility of standardizing 7-point bend testing