

Characterizing Mechanical Property Variability in Ti6Al4V produced by Laser Powder Bed Fusion (LPBF) Additive Manufacturing

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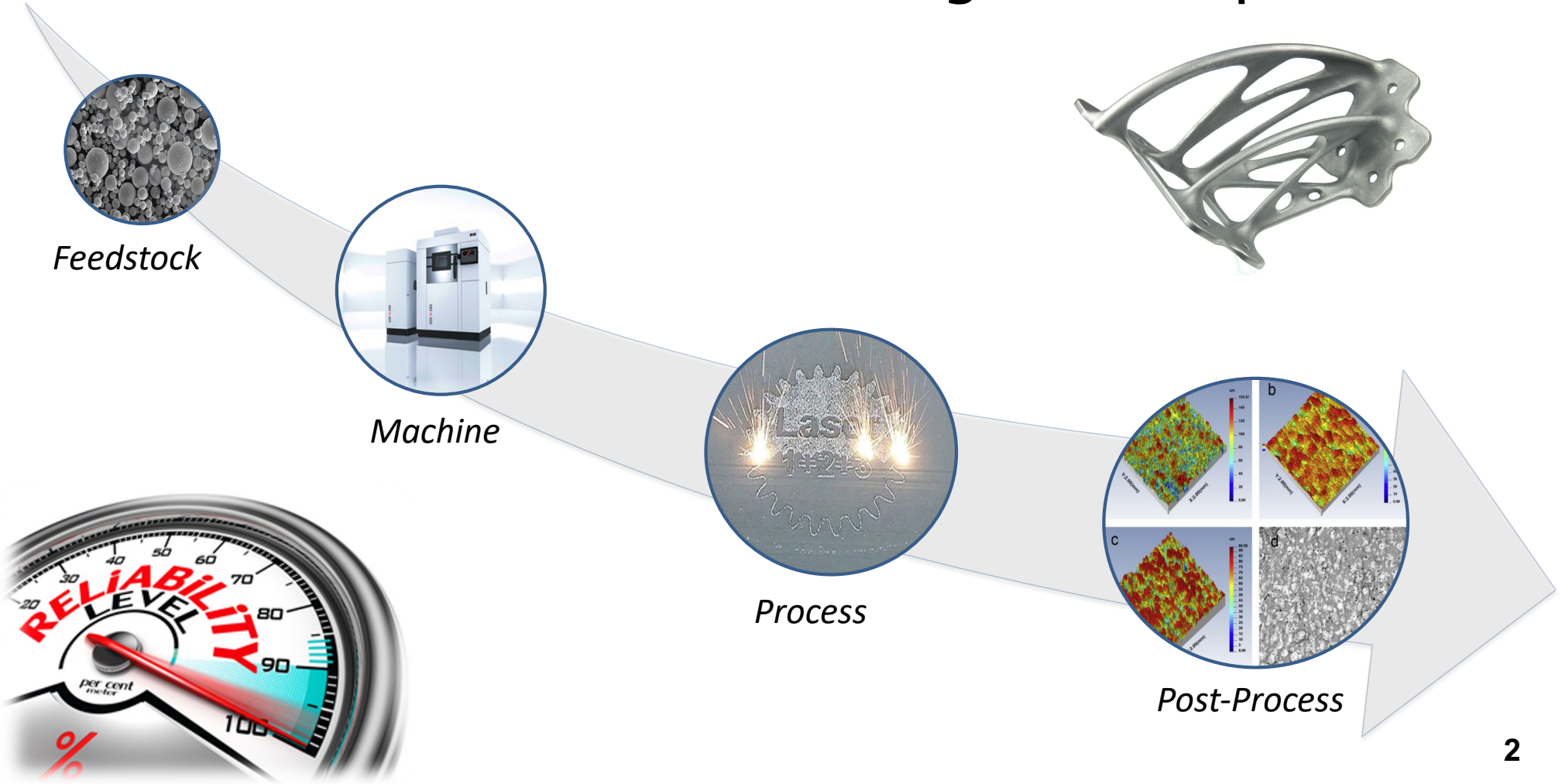
FAA Tech Monitor: Kevin Stonaker / FAA Sponsors: Cindy Ashforth & Michael Gorelik



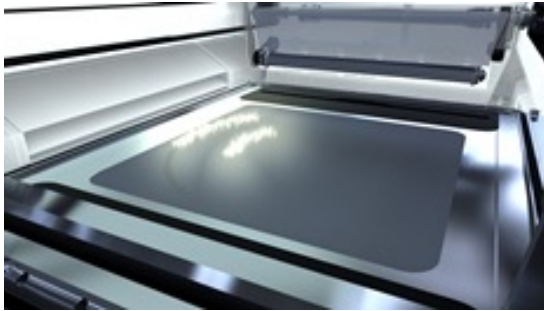
April 18th, 2023



LPBF Additive Manufacturing in Aerospace



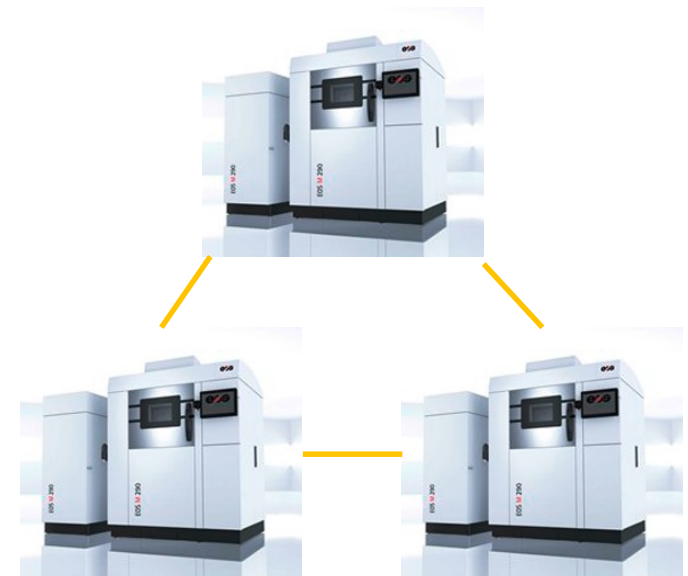
Categories of Process Variability in LPBF



I. Intra-Build



II. Inter-Build



III. Inter-Machine



Objective and Aims

Overall Objective: Characterize the variability in microstructure and durability of Ti-6Al-4V resulting from LPBF involving multiple identical make/model machines under fixed primary- and post-process conditions.

Aim 1: Characterize the intra-build variability

Aim 2: Characterize the inter-build variability

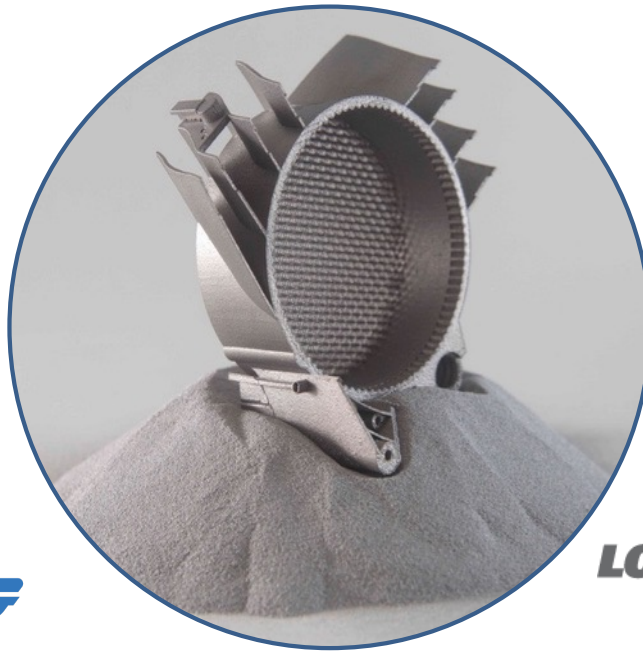
Aim 3: Characterize the inter-machine variability

Round Robin Partners

W

'TORAY'
Toray Precision Co., Ltd.

 **BOEING**



EOS

 **3D LOGICS**

LOCKHEED MARTIN 
oerlikon

Overview of Program and Approach

- All partners operating an EOS M290
- Single lot of powder for all partners (EOS Grade 5 Ti6Al4V)
- Single Process Control Document (PCD) for all partners
- All partners use same process parameters (Ti6Al4V)
- All partners follow same build design

Process Control Document

University of Washington Round Robin (UWRR):
Property Variability in AM of Ti6Al4V by SLM

Process Control Document

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10/22/2020

Prepared for: Inner Core Participants

University of Washington (lead)
The Boeing Company
EOS
Lockheed Martin
Toray Precision Company
3D Logics

Partner Questionnaire (Powder + Machine)

University of Washington Round Robin (UWRR):
Property Variability in AM of Ti6Al4V by SLM

Process Parameter Survey

Note: This survey is provided in order to establish understanding between the inner core participants and The University of Washington (UW) team about the participant operating conditions for this study. Please answer the following prompts to the best of your ability and email the response to Dr. Dwayne Arola (darola@uw.edu).

Participant Company Name: _____

Primary Operator Name and Email: _____

A Powder Storage Conditions

Storage temperature: _____ Humidity control: Yes No

Storage humidity: _____

Please describe the powder storage containers (original containers, explosion proof, or other):

B Machine Conditions

Machine Operating Environment

Operating room temperature: _____ Humidity control: Yes No

Powder used prior to April, 2020: Ti-6Al-4V Other (please specify below)

(if used material other than Ti-6Al-4V) Materials: _____

Last use: _____

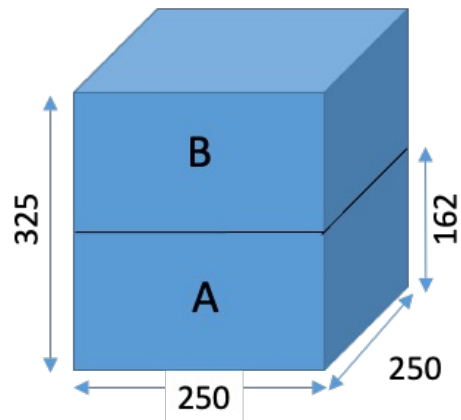
Plan on using other powder during this study on this machine: Yes No

Have a machine cleaning SOP to prevent cross-contamination: Yes No

Willing to share this SOP with UW: Yes No

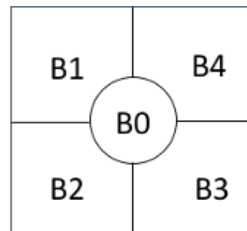
Any details about machine cleaning SOP:

Build Design and Discretization

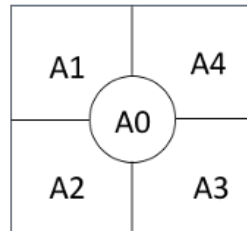


Oblique View

Two Levels (A, B)



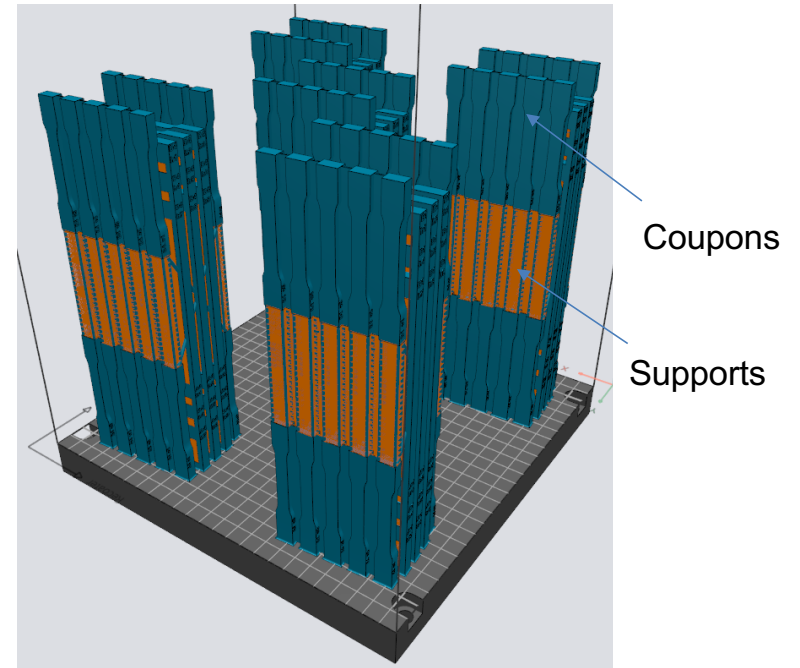
Top View – Level B



Top View – Level A

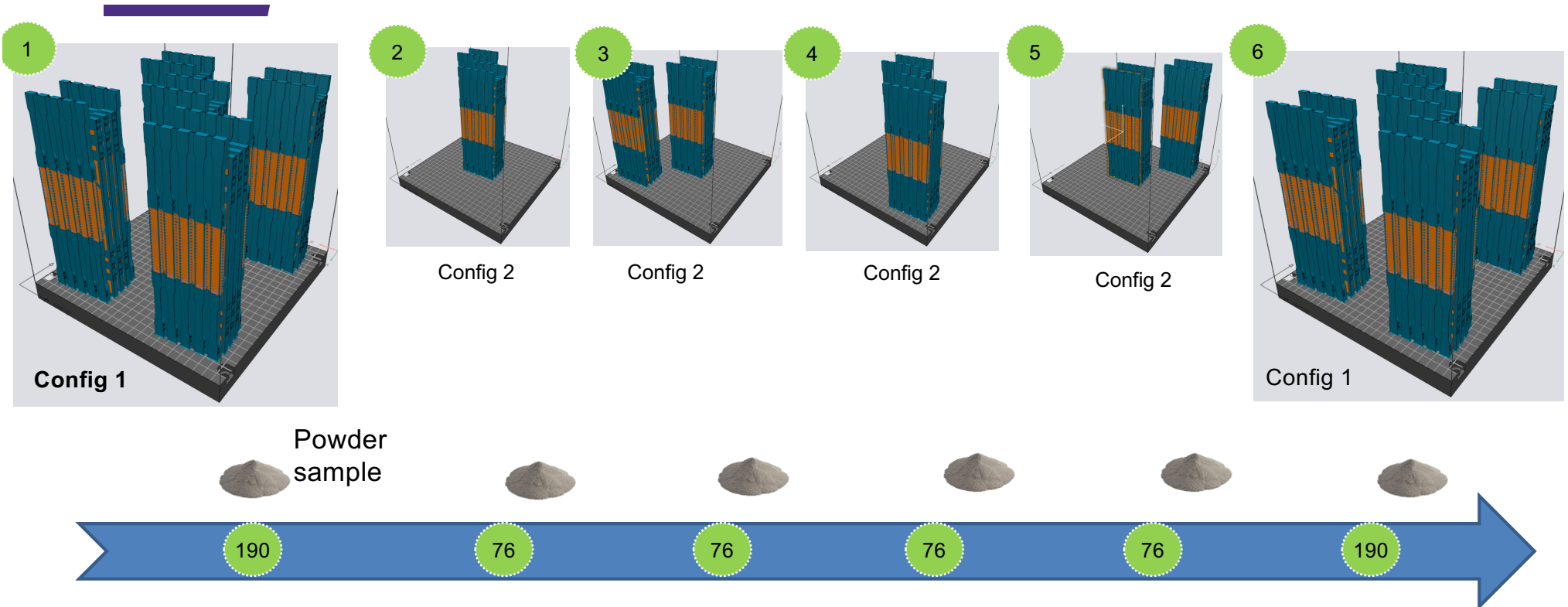
Five Zones per level
(0, 1, 2, 3, 4, 5)

Build Envelope Discretization



Build Design (5 zones, 2 levels)

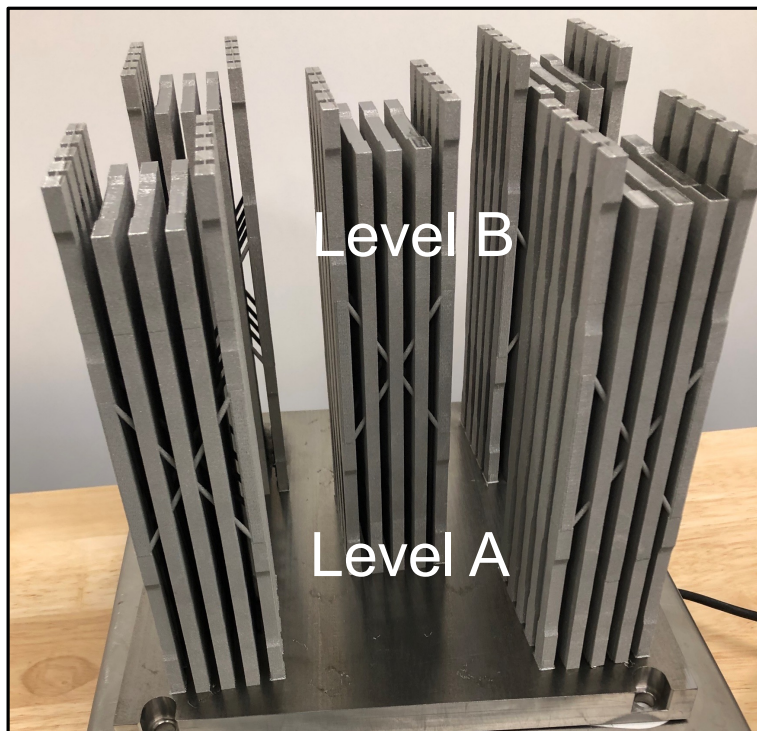
Round Robin Build Sequence



Total specimens per partner = 684

Total Specimens = 684 per partner x 6 partners = 4104

Progress of Partners and Program: Phase I



| | B1 | B2 | B3 | B4 | B5 | B6 |
|----|----|----|----|----|----|----|
| P1 | ■ | ■ | ■ | ■ | ■ | ■ |
| P2 | ■ | ■ | ■ | ■ | ■ | ■ |
| P3 | ■ | ■ | ■ | ■ | ■ | ■ |
| P4 | ■ | ■ | ■ | ■ | ■ | ■ |
| P5 | ■ | ■ | ■ | ■ | ■ | ■ |
| P6 | ■ | ■ | ■ | ■ | ■ | ■ |

□ Underway ■ Completed

Post-Processing Facilities

Heat Treatment



Nabertherm LH 120/12 w/
P470 controller and gassing
box (Argon treatment)

Machining



Omax 2652 Abrasive
Waterjet



HAAS CNC Mill
(TM-1P)

745°C for 2 hours with furnace cool

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Metal Characterization Facilities

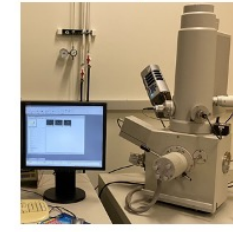
Microscopy



Optical/Stereo Microscopes
Olympus
BX 51M



Olympus
SZX16



Scanning Electron Microscopes
Philips XL-30 Sirion (+EDS)
TFS Apreo var-press (+EDS + EBSD)



Spectroscopy



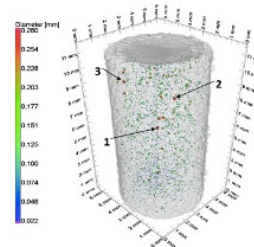
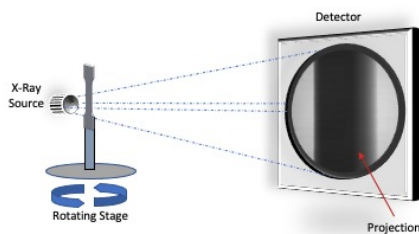
X-Ray Fluorescence
Bruker
M4 Tornado

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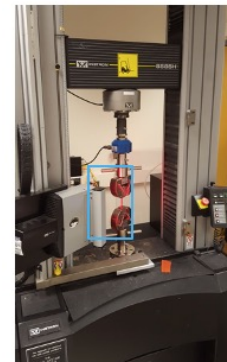
Micro Computed Tomography

X-Ray Micro Computed Tomography:

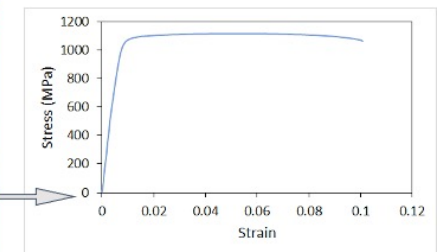
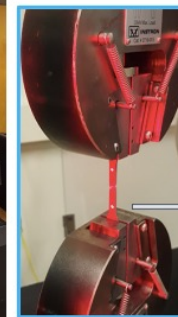
- North Star Imaging system, microCT, X5000, Rogers, MN, USA
- 360° x-ray scans and 3D reconstruction



Mechanical Property Characterization (Static and cyclic)



Universal Testing System:
Instron Model 5585H; Norwood, MA



ASTM E8 based procedures

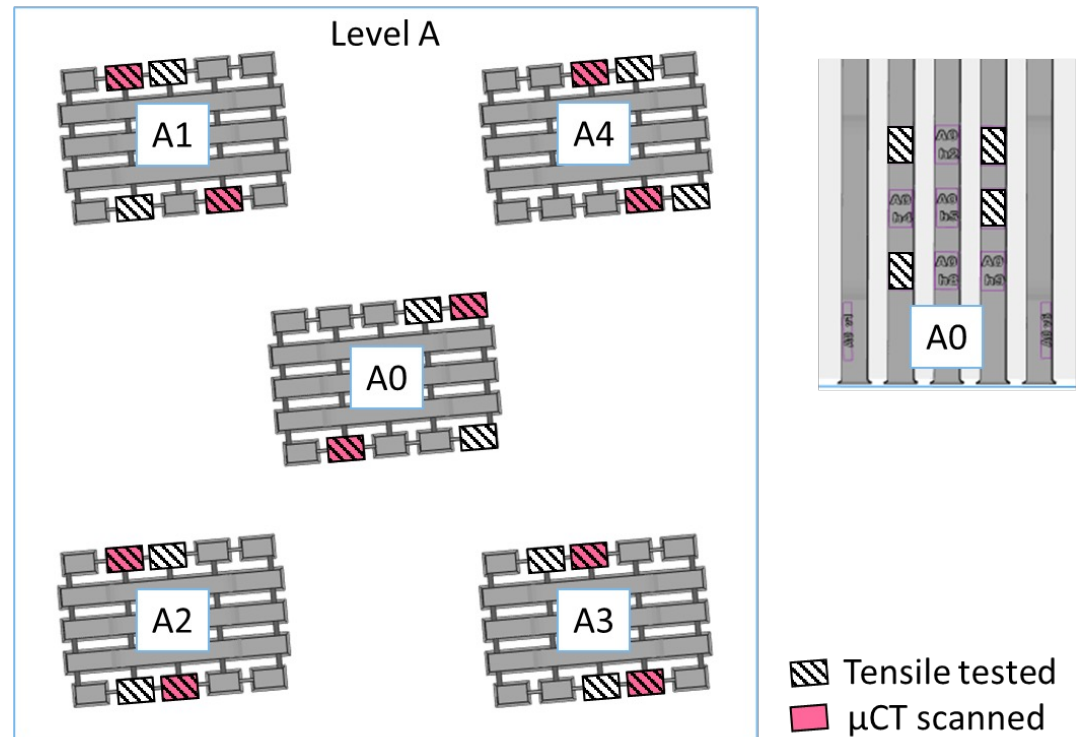
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Methods - Characterization of Metal and Powder

| | <u>Characterization Technique</u> | <u>Properties of Interest</u> |
|--------|---|---|
| Metal | Tensile Testing | Mechanical behavior (ductility, strength, toughness, etc.) |
| | Micro Computed Tomography (μ CT) | Porosity ($\sim 8\mu\text{m}$ voxels) |
| | Scanning Electron Microscopy (SEM) | Microstructure |
| Powder | Light Scattering Powder Analysis (LSPA) | Particle size distribution |
| | SEM | Particle morphology |
| | Hall Flow Meter | Powder flowability |
| | Inert Gas Fusion (IGF) and XRD | Powder contaminants (oxygen, nitrogen, hydrogen, and carbon) |

Methods - Coupon Selection for Analysis

- Subset of total number of coupons used for testing to decrease testing time
- Coupons were pseudo-randomly selected from each zone. Selected coupons were kept identical across the participants.
- Reserved coupons enables other investigations to take place



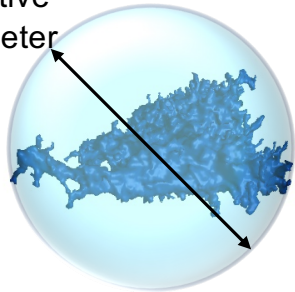
1652 coupons tensile tested
354 vertical coupons μCT scanned

Methods - microCT Analysis of Porosity

- 1) Effective Diameter
- 2) Sphericity
- 3) Large Pores Per Coupon

$$D_{\text{eff}} \geq 0.125 \text{ mm}$$

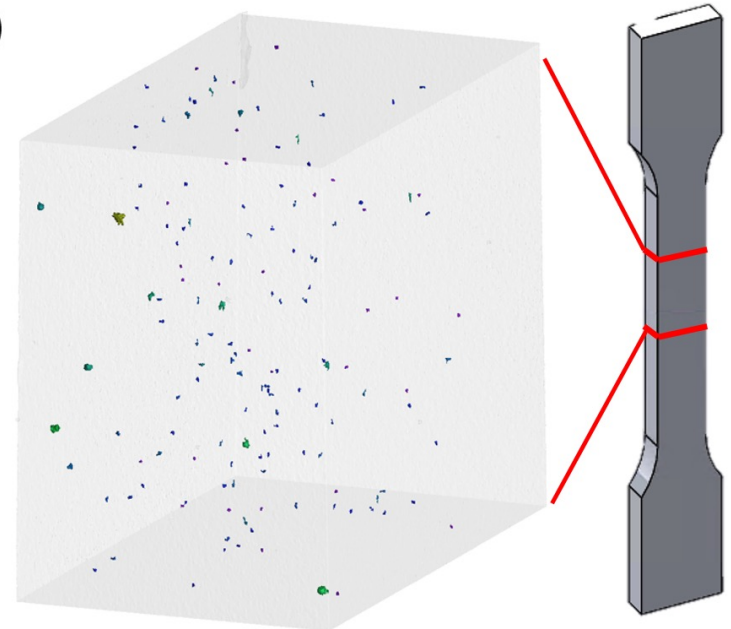
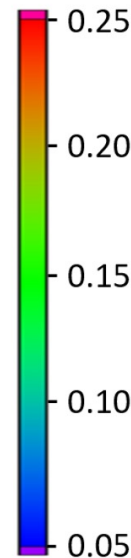
Effective Diameter



$$\frac{SA_{\text{sphere}}}{SA_{\text{pore}}} = \text{Sphericity}$$

$\ll 1$

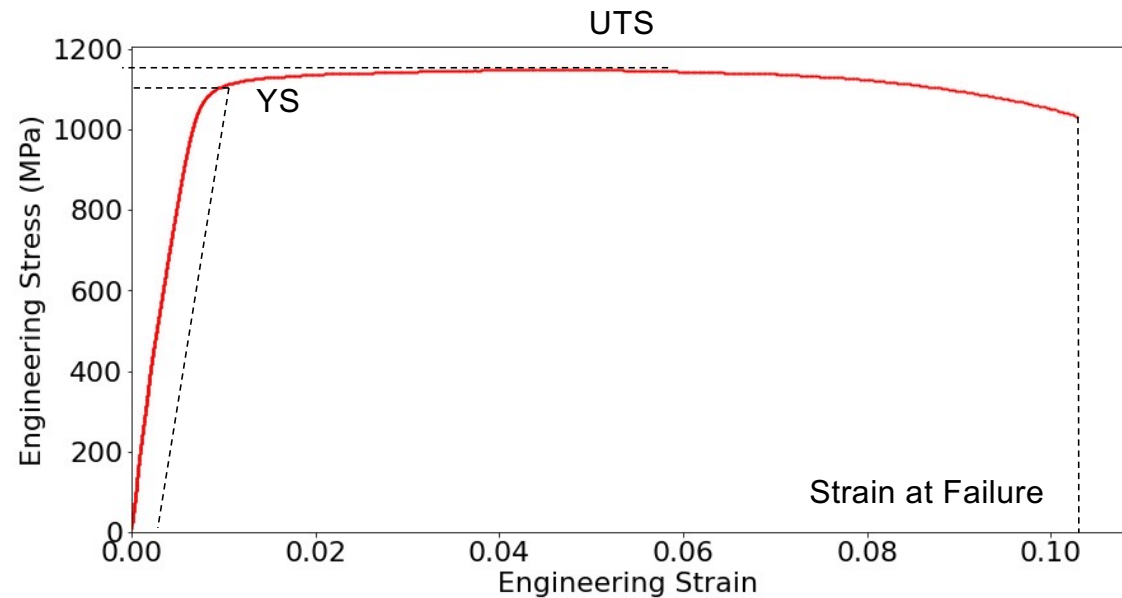
Diameter (mm)



Characterizing the Tensile Properties



ASTM E8, Subsize Coupons
Clip-on extensometer



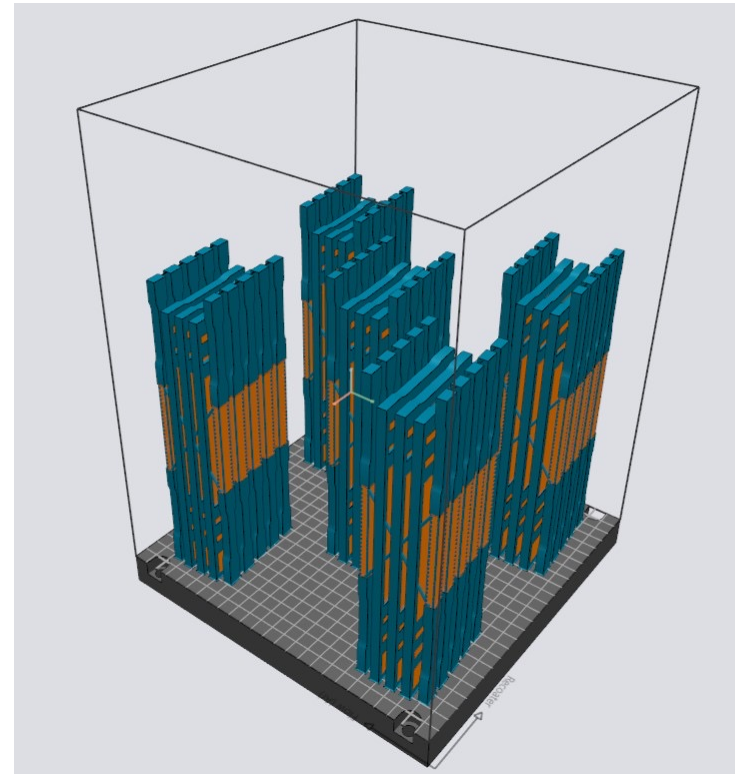
YS = Yield Strength (at 0.002 offset)

UTS = Ultimate Tensile Strength

% el = strain at failure

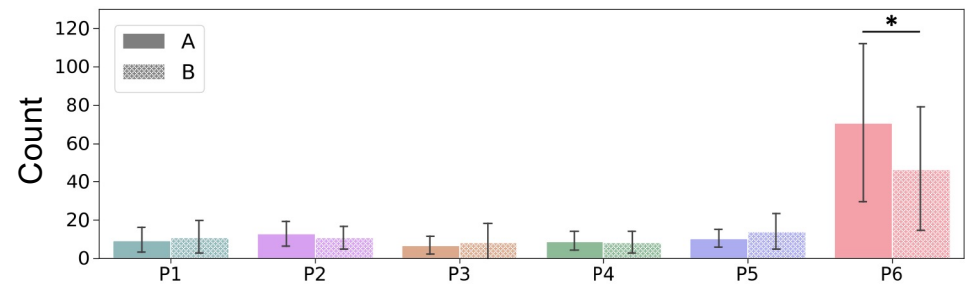
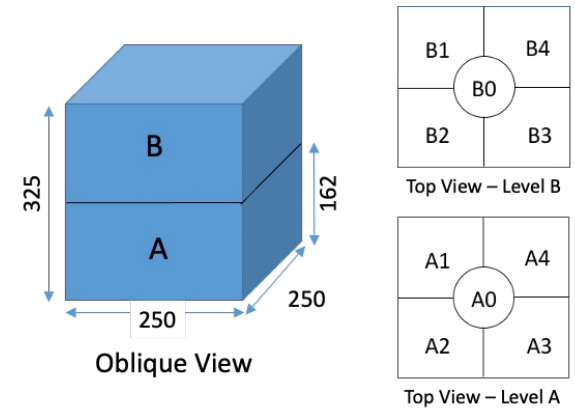
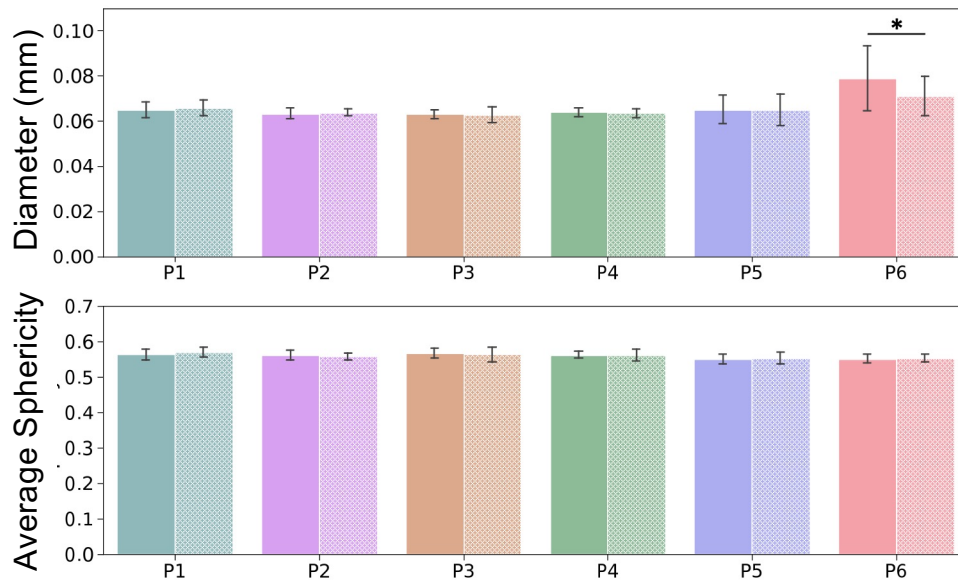
Intra-Build Analysis: Porosity and Properties

- 1) Build Height (A vs B)
- 2) Zones (0 to 4)
- 3) X and Y position



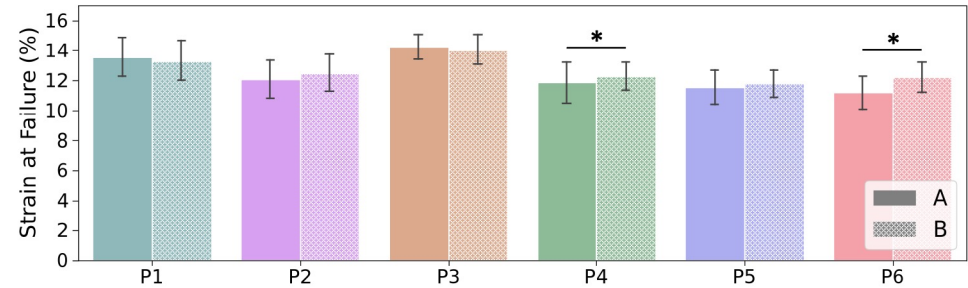
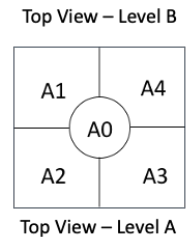
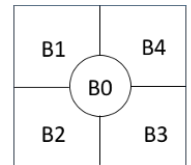
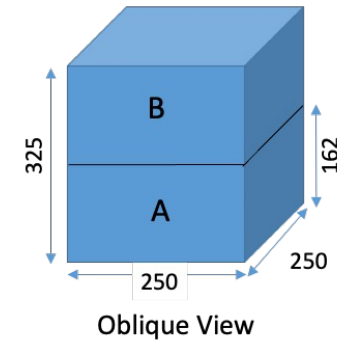
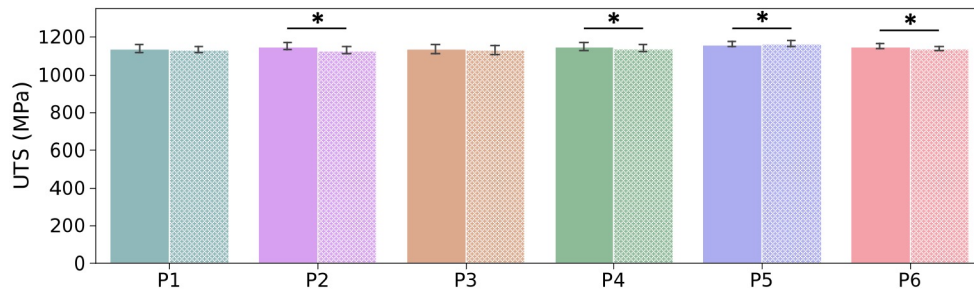
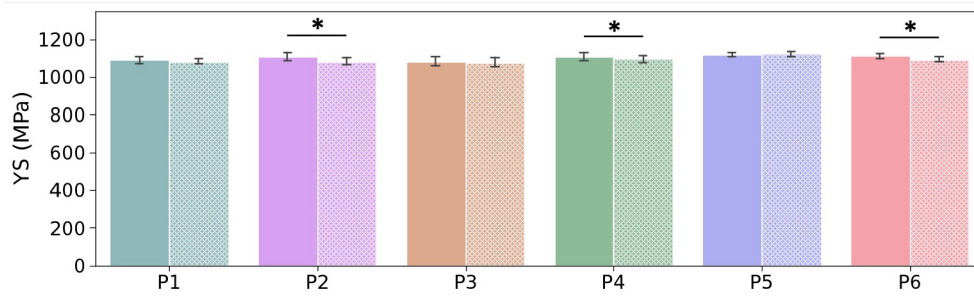
The intra-build analysis presented today includes only the vertical coupons

Intra-Build: Build Height (Porosity)



➤ Analysis of Variance (ANOVA) shows only P6 has statistical difference between A and B levels for the average diameter and count of large pores ($d \geq 0.125$ mm)

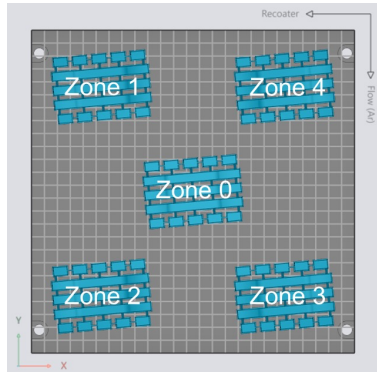
Intra-Build: Build Height (Tensile Properties)



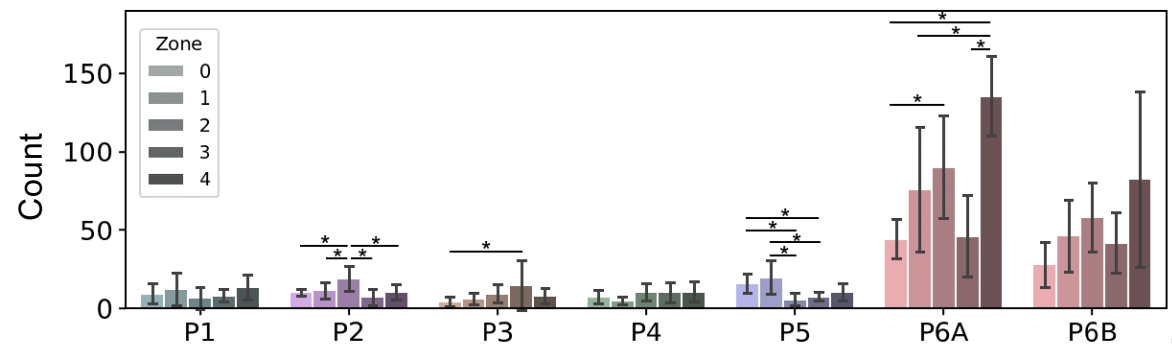
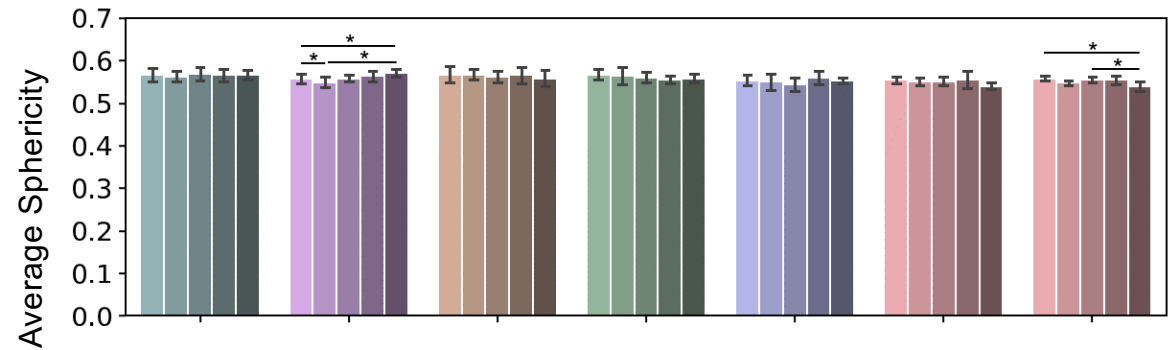
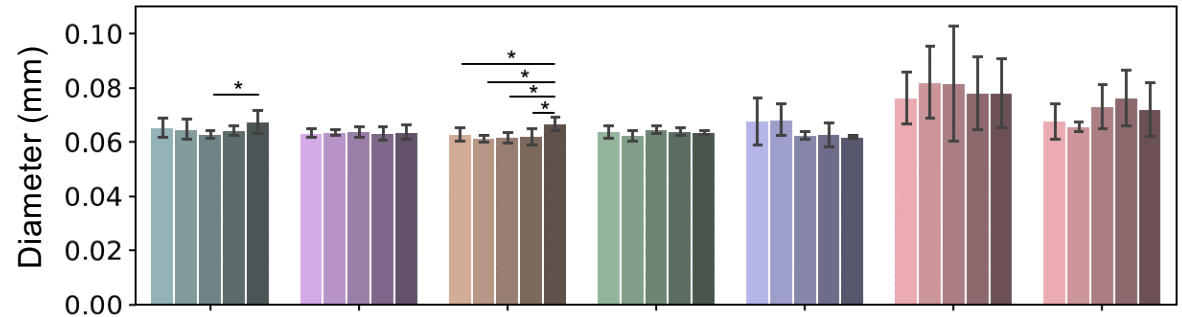
- Significant differences identified
- Magnitude of difference in strength is negligible (~10 MPa)
- Larger difference between A and B levels for strain at failure (up to 1% strain)

Intra-Build: Zones

Pore Characteristics

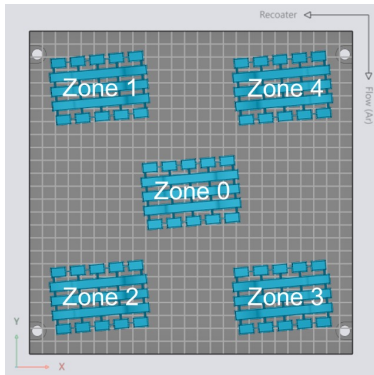


- Analysis of P6 metal separated for height levels
- Some significant differences. Inconsistent zones between machines

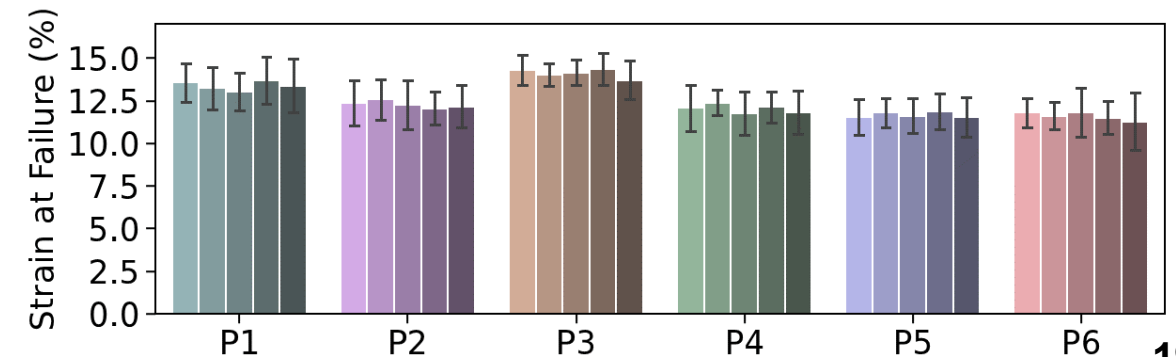
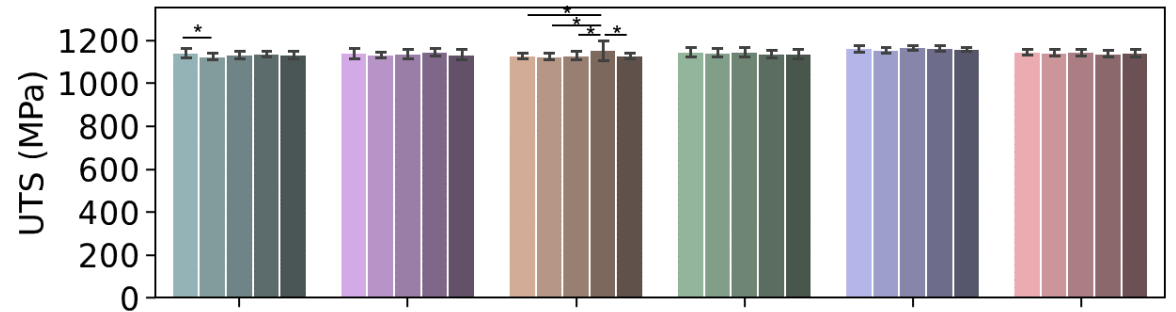
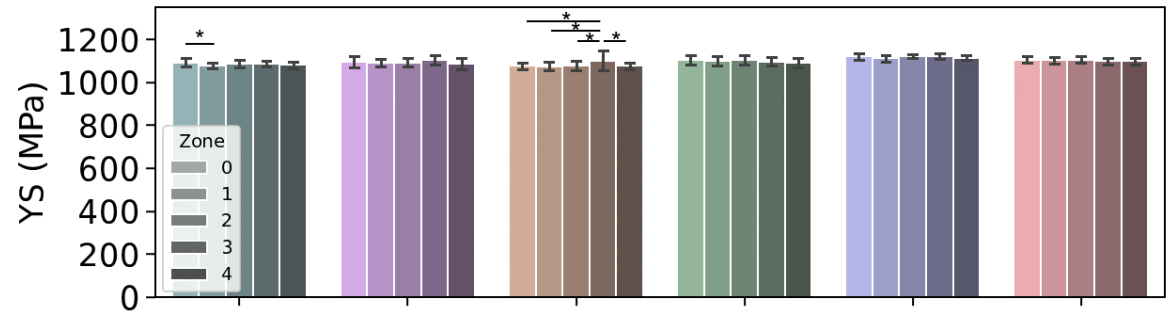


Intra-Build: Zones

Tensile Properties

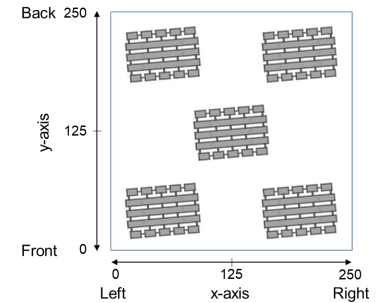


- Few significant differences between zones
- Significant differences always include Zone 0, independent of machine.

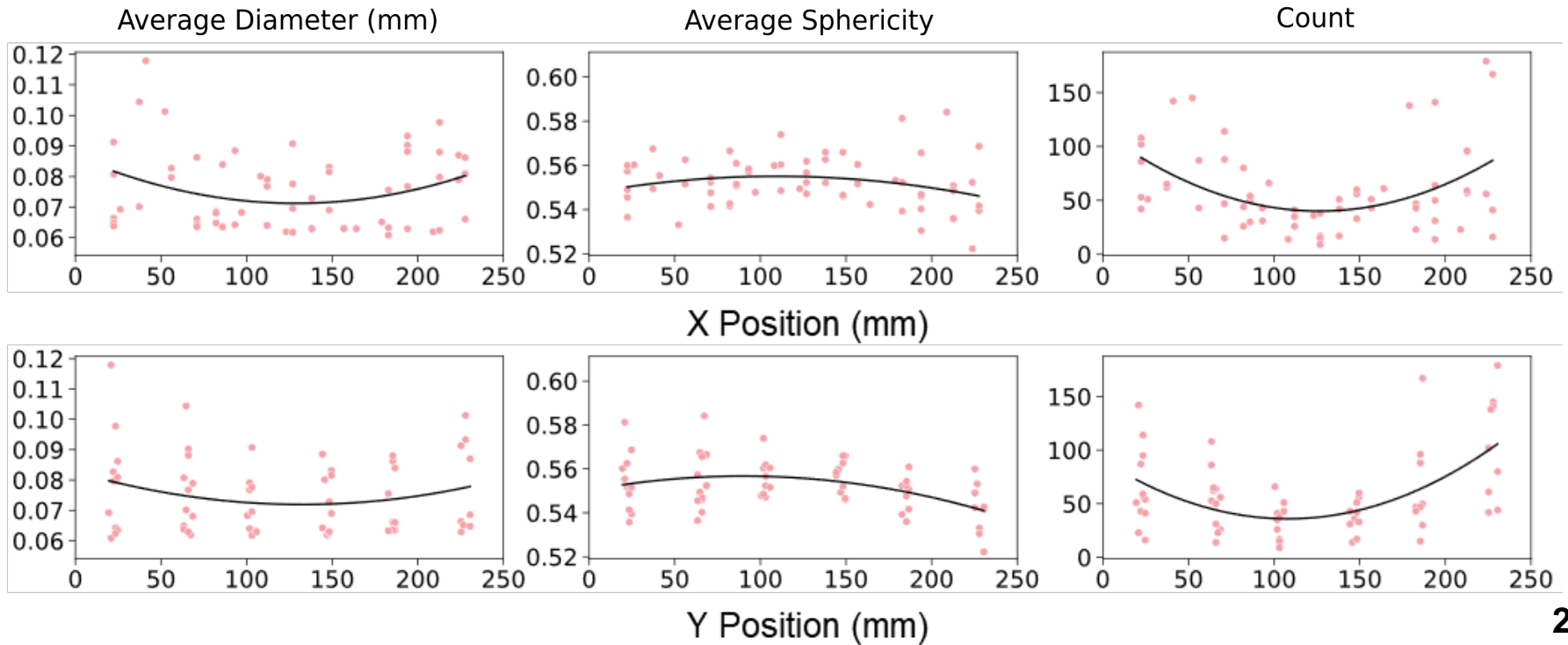


Intra-Build: Exact Position (Porosity)

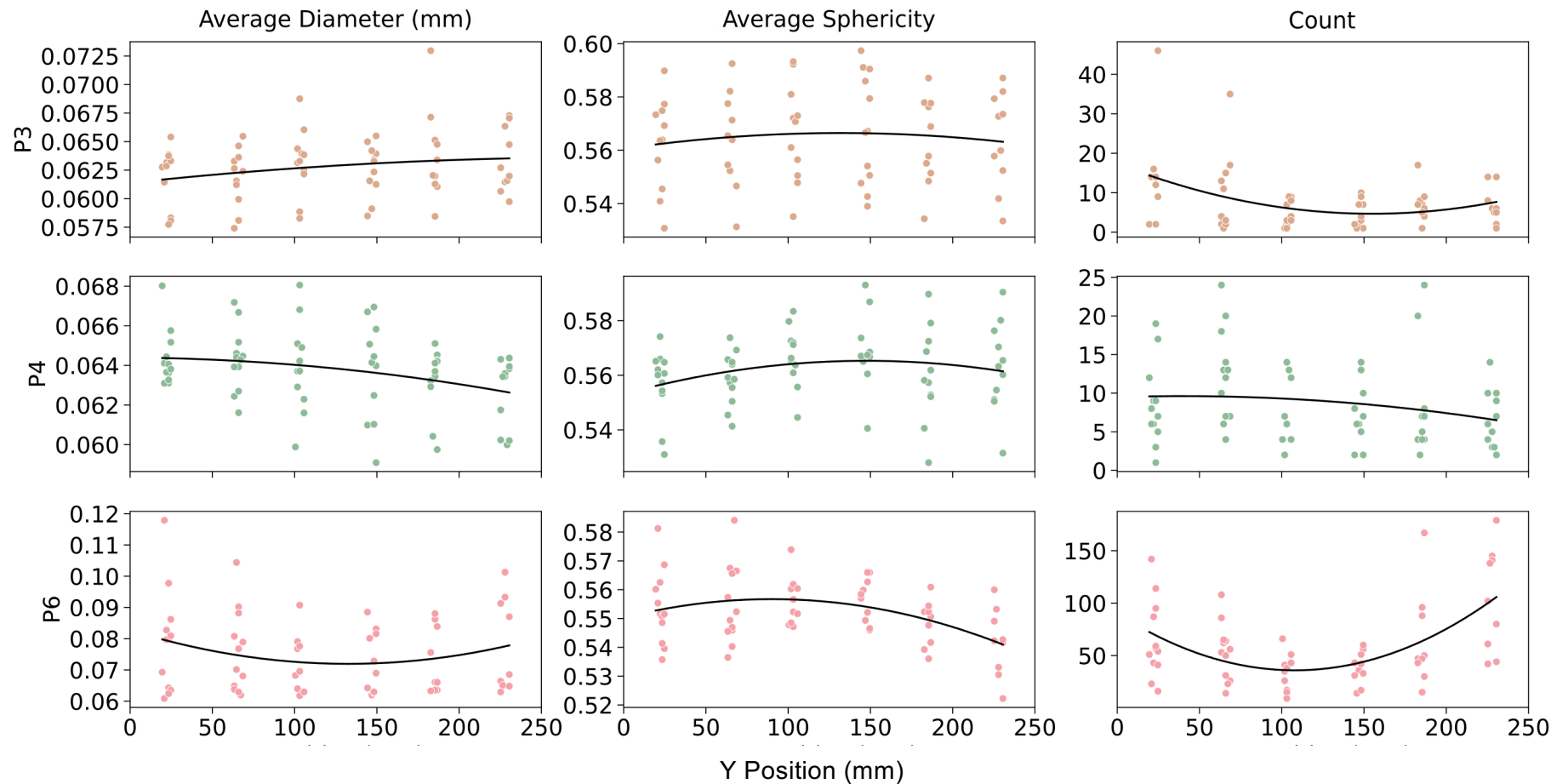
- Process physics can result in spatial distributions.
- Pore distribution of P6 is approximately radially symmetric



P6



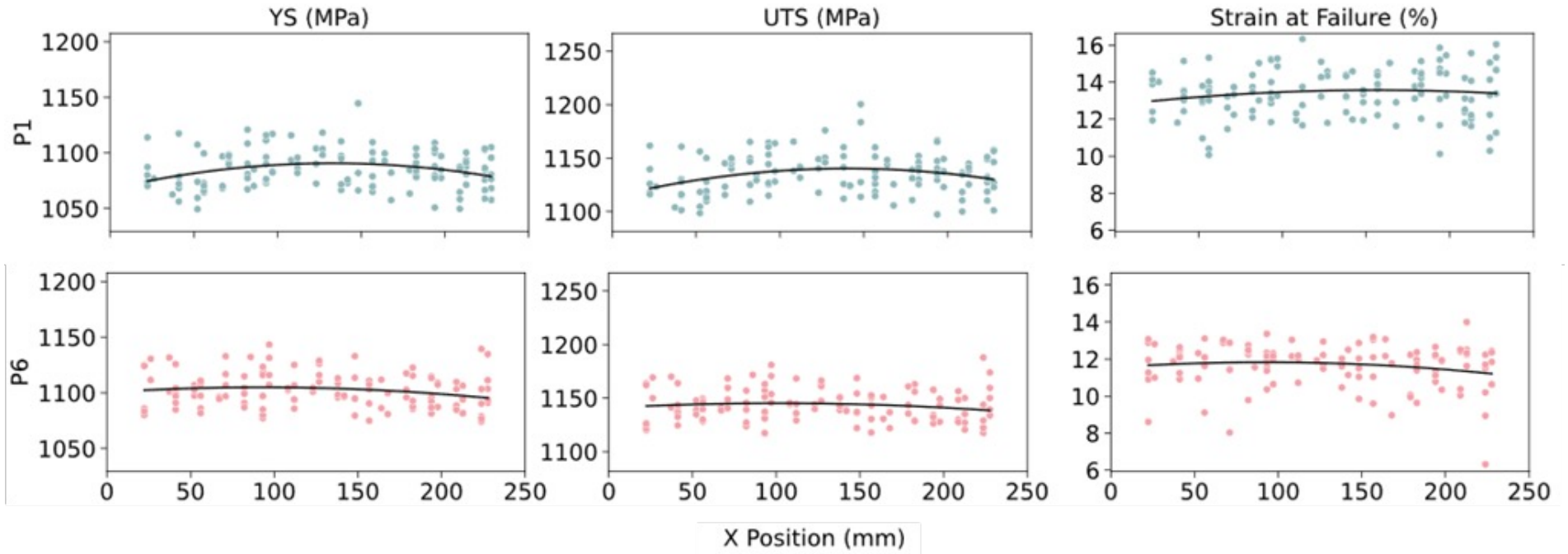
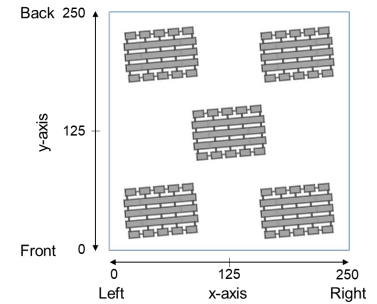
Intra-Build: Unique Porosity Distributions



➤ 3 machines have trends along y-axis of varying strength

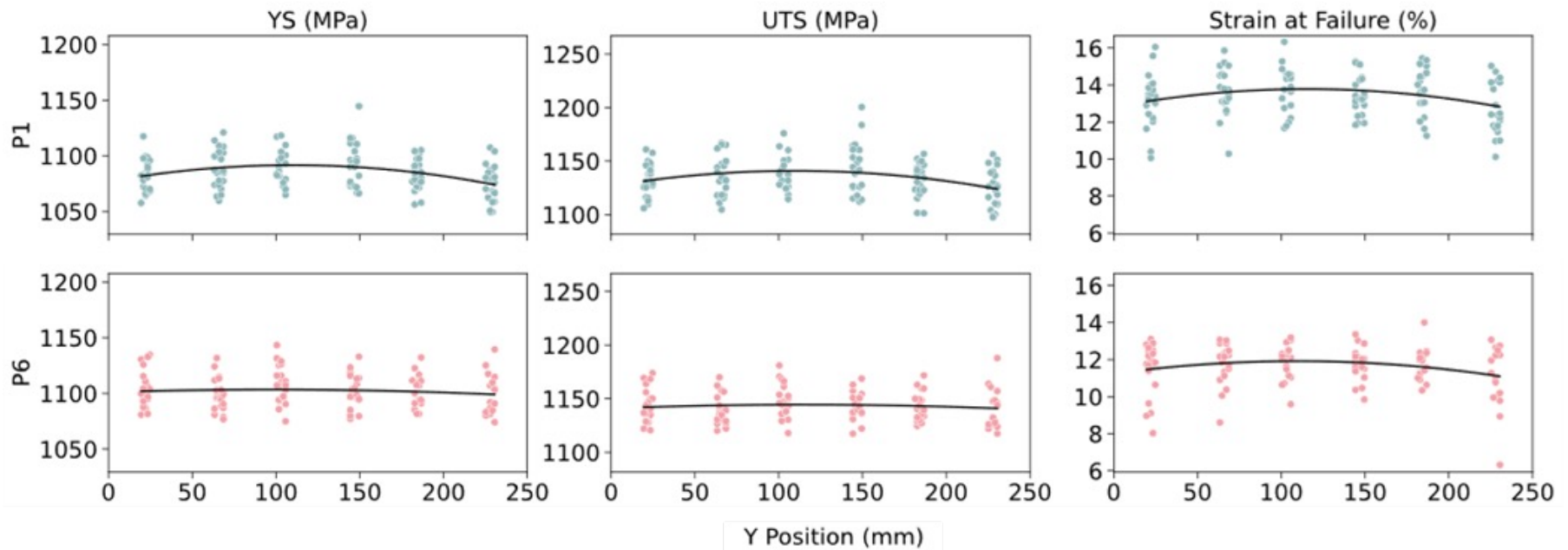
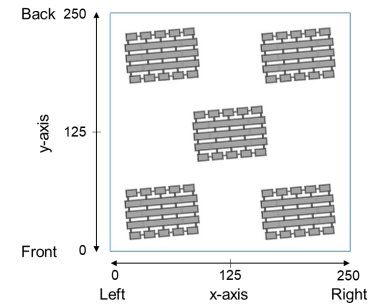
Intra-Build: Tensile Properties

➤ P1 and P6 are the only machines with an x-axis dependency



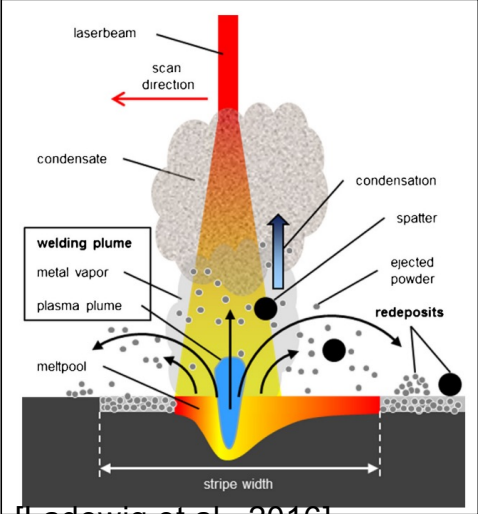
Intra-Build: Tensile Properties

- P1 and P6 have strongest y-axis dependency
- Gas flow and radial laser incidence angle may explain these trends

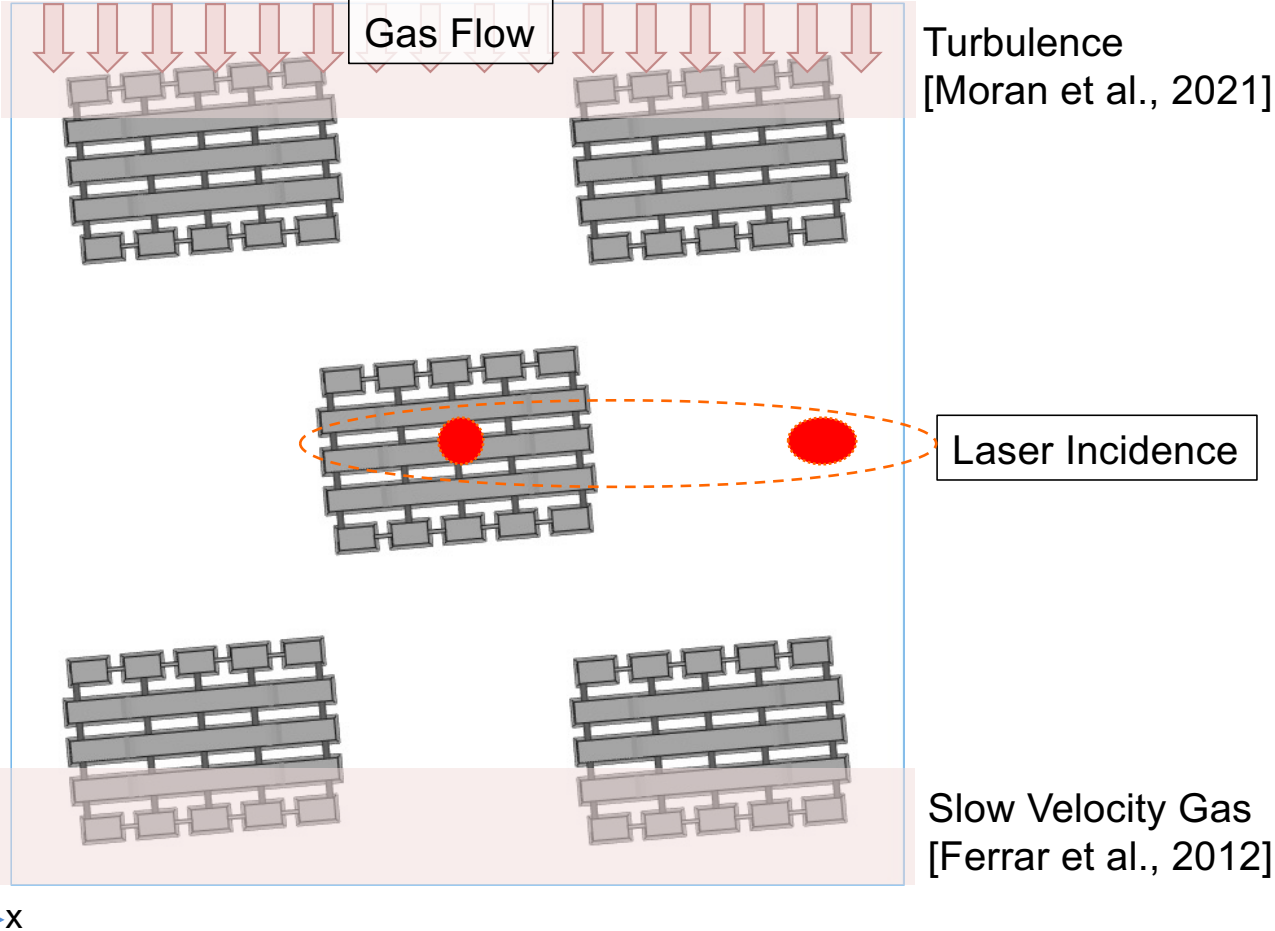


Intra-Build: Contribution of Shielding Gas

Root Cause



[Ladewig et al., 2016]

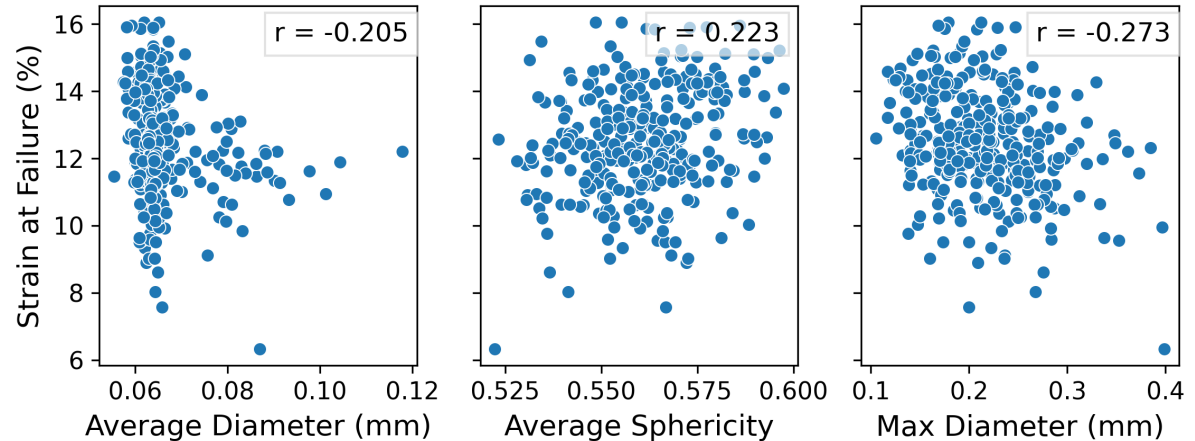


Turbulence
[Moran et al., 2021]

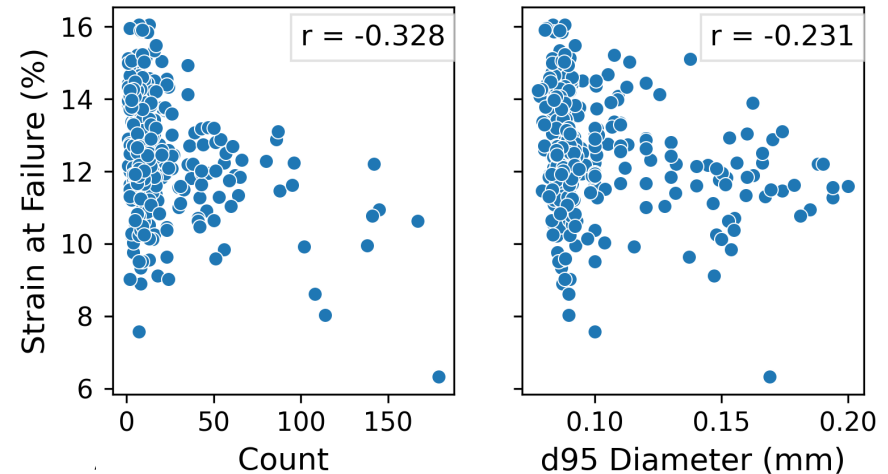
Laser Incidence

Slow Velocity Gas
[Ferrari et al., 2012]

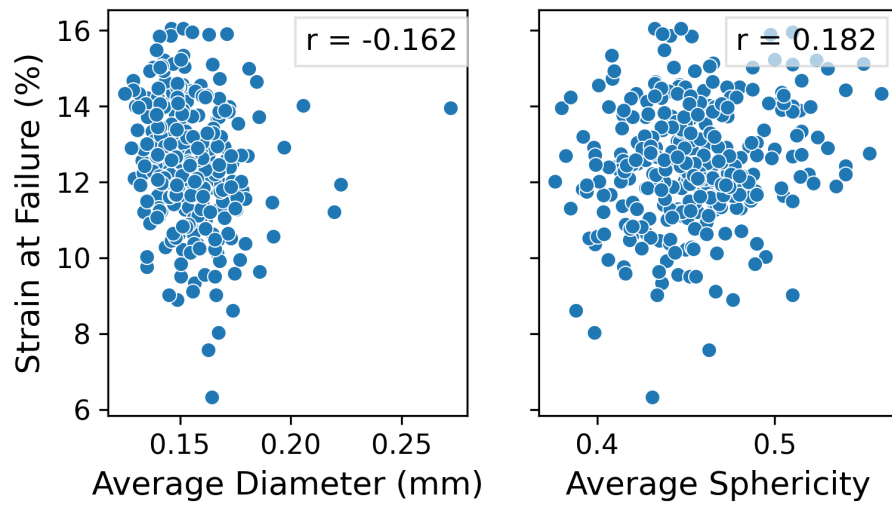
Porosity and Strain at Failure Correlations



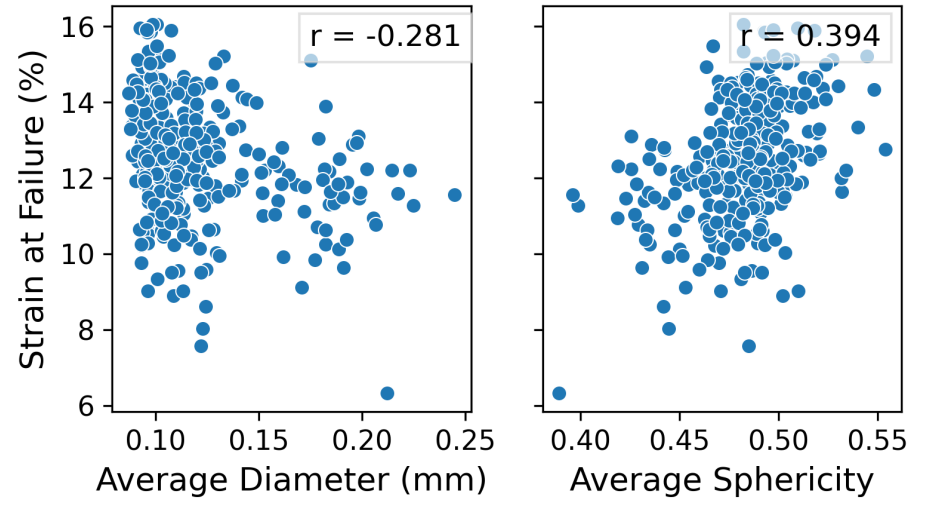
- No correlation between porosity metrics and strain at failure
- Pores on the surface are not registered as pores by μ CT which limits correlation
- Do not capture multiple pore characteristics simultaneously (i.e., size, shape, location, clustering)



Porosity and Strain: Large Pores Only



(a) Pores ≥ 0.125 mm Diameter



(b) Pores $\geq d_{90}$ Diameter

➤ Improved correlation with d_{90} diameter, but still weak

Overall Variability in Mechanical Properties

All Machines

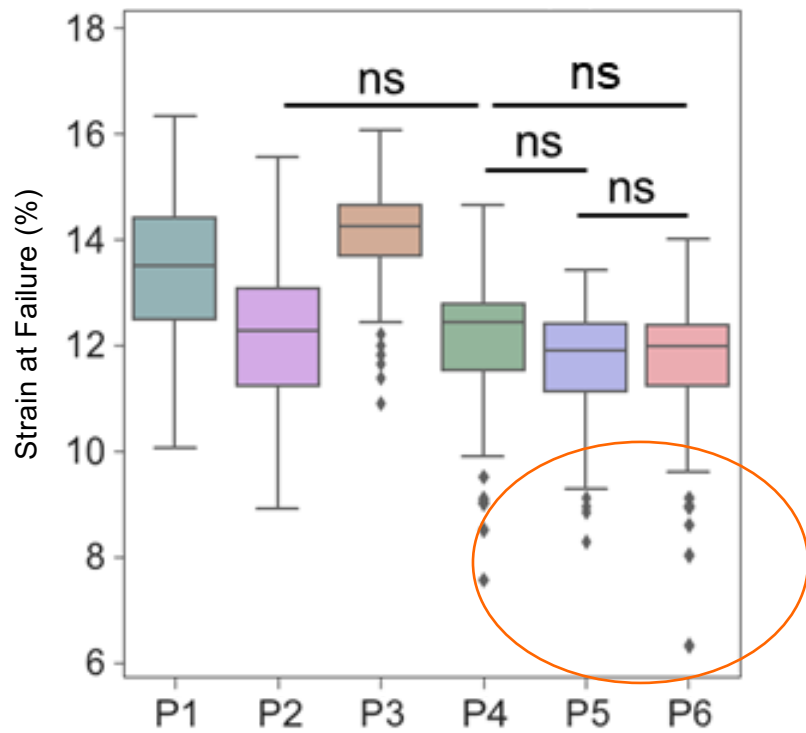
| | CoV of YS (%) | CoV of UTS (%) | CoV of Strain at Failure (%) |
|------------|------------------|-------------------|---------------------------------|
| Vertical | 2.1 | 1.9 | 11.8 |
| Horizontal | 2.2 | 1.9 | 14 |
| Wrought | 1.8 | 1.8 | 8.3 |

Identically Heat Treated
(P2, P4, P5, P6)

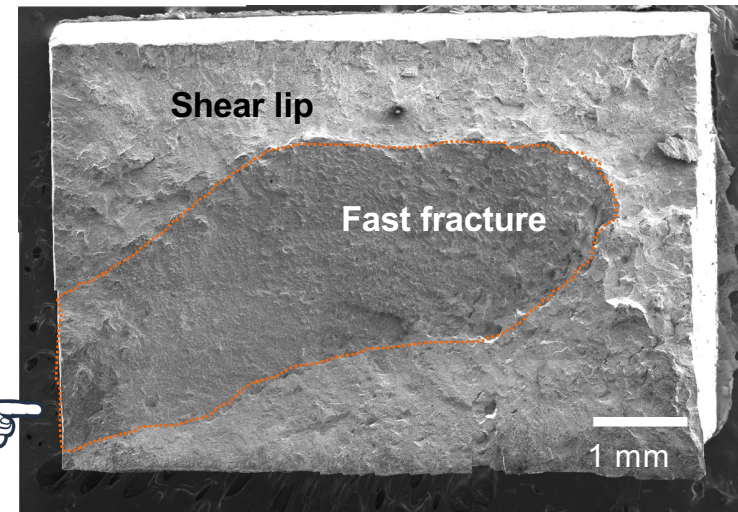
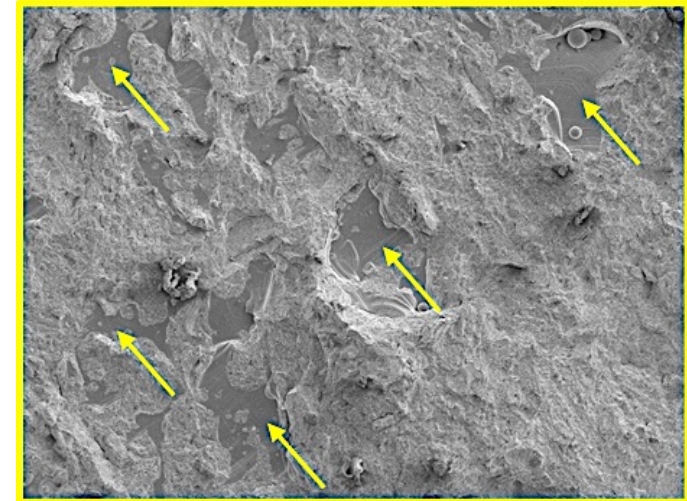
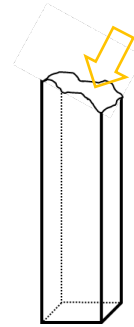
| | CoV of YS (%) | CoV of UTS (%) | CoV of Strain at Failure (%) |
|------------|------------------|-------------------|---------------------------------|
| Vertical | 1.9 | 1.8 | 10 |
| Horizontal | 1.7 | 1.6 | 12.1 |
| Wrought | 1.8 | 1.8 | 8.3 |

- 33 wrought Ti-6Al-4V coupons cut from the same sheet of metal were tested for comparison
- AM metal has similar variability to wrought form metal

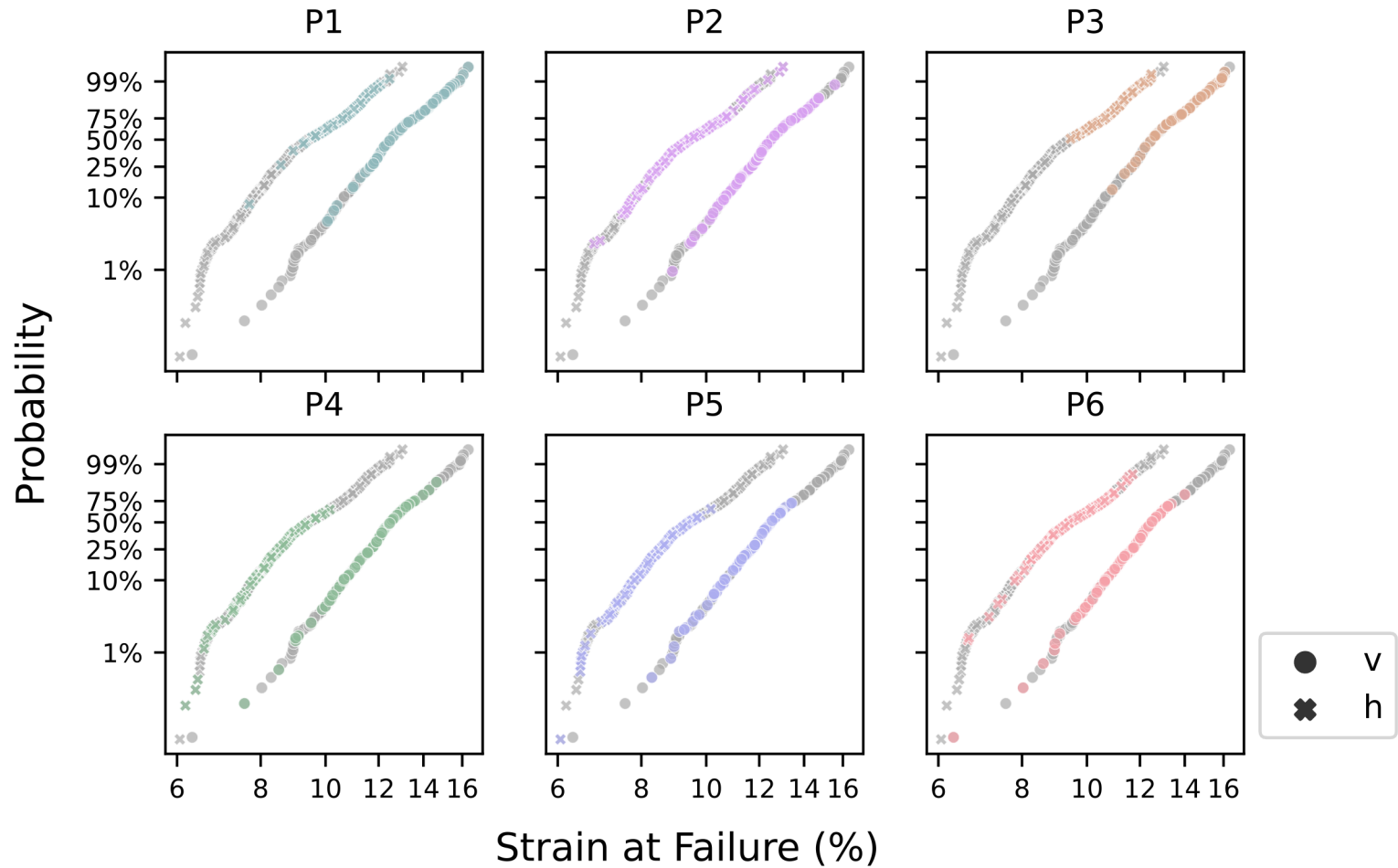
Inter-Machine: Outliers



Fracture Surface



Inter-Machine: Weibull Distributions



Conclusions

- 1) Variability exists on the intra-build, inter-build, and inter-machine levels, however the overall magnitude for the static properties is similar to that for wrought titanium
- 2) Design for additive manufacturing (DFAM) can accommodate the variability exhibited by most machines, however outlier machines do exist, necessitating individualized DFAM
- 3) Greatest sources of variability appear to originate from issues with machine maintenance or post-processing variability – fine-tuning machine maintenance may allow for broader machine equivalency

Acknowledgements



Toray Precision Co., Ltd.





Thank you!

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