

JOINT ADVANCED MATERIALS & STRUCTURES  
CENTER OF EXCELLENCE

# Crashworthiness of Composites - Certification by Analysis

2015 Technical Review

Gerardo Olivares

J. F. Acosta

National Institute for Aviation Research, WSU



WICHITA STATE  
UNIVERSITY

# Crashworthiness Certification by Analysis

- Principal Investigators & Researchers
  - G. Olivares Ph.D. (PI)
  - S. Keshavanarayana Ph.D.
  - J.F. Acosta Ph.D.
  - Chandresh Zinzuwadia, Nilesh Dhole.....
  - NIAR Computational Mechanics
- FAA Technical Monitor
  - Allan Abramowitz
- Other FAA Personnel Involved
  - Joseph Pellettiere

# Crashworthiness of Composites - Certification by Analysis

- Motivation and Key Issues

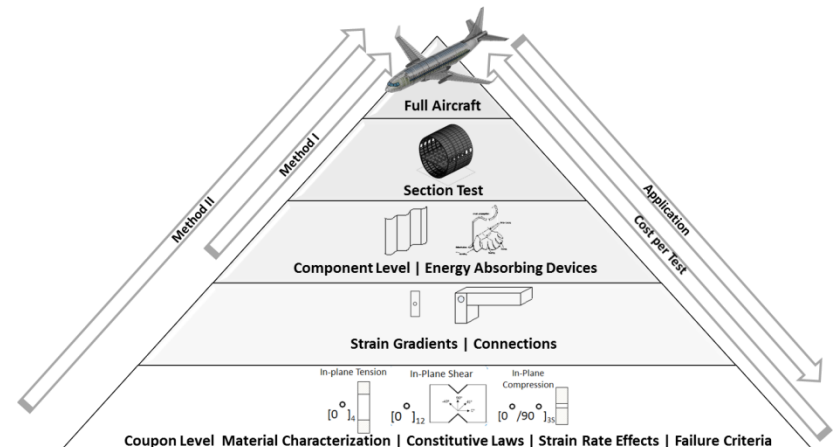
- The introduction of composite airframes warrants an assessment to evaluate that their crashworthiness dynamic structural response provides an equivalent or improved level of safety compared to conventional metallic structures. This assessment includes the evaluation of the survivable volume, retention of items of mass, deceleration loads experienced by the occupants, and occupant emergency egress paths.

- Objective

- In order to design, evaluate and optimize the crashworthiness behavior of composite structures it is necessary to develop an evaluation methodology (experimental and numerical) and predictable computational tools.

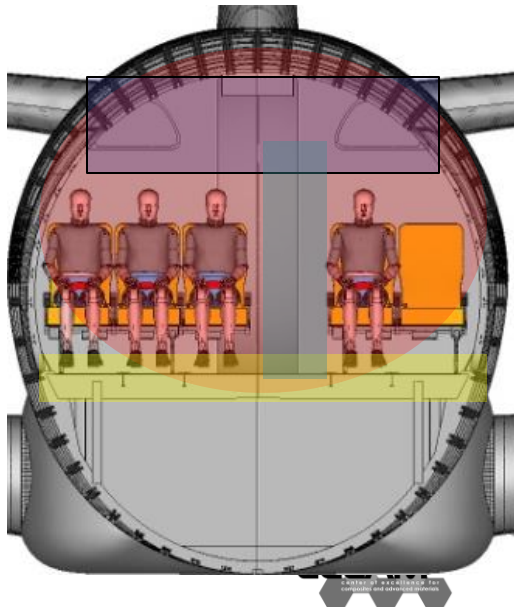
- Approach

- Building Block Methodology Development

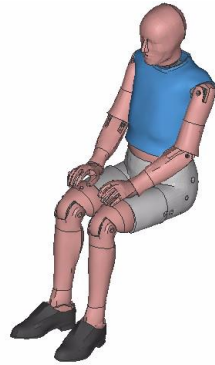


# Aerospace Structural Crashworthiness

- **Crashworthiness performance of composite structures to be equivalent or better than traditional metallic structures**
- **Crashworthiness design requirements:**
  - Maintain survivable volume
  - Maintain deceleration loads to occupants
  - Retention items of mass
  - Maintain egress paths
- **Currently there are two approaches that can be applied to analyze this special condition:**
  - **Method I: Large Test Article Approach**
    - **Experimental:**
      - Large Test Articles (Barrel Sections)
      - Component Level Testing of Energy Absorbing Devices
    - **Simulation** follows testing – Numerical models are “**tuned**” to match large test article/EA sub-assemblies results. Computational models are only predictable for the specific configurations that were tested during the experimental phase. For example if there are changes to the loading conditions (i.e. impact location, velocity, ..etc.) and/or to the geometry, the model may or may not predict the crashworthiness behavior of the structure.
  - **Method II: Building Block Approach**



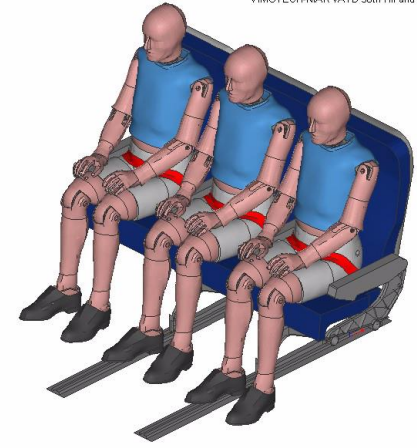
# Technical Approach – Aerospace Crashworthiness CBA



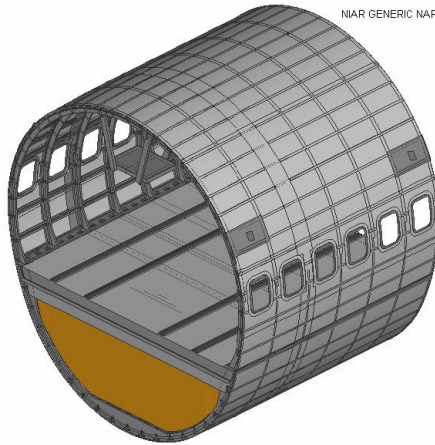
10 ft - Fuselage Section  
VIMOTECH-NIAR vATD 50th HII  
Time = 0.000000



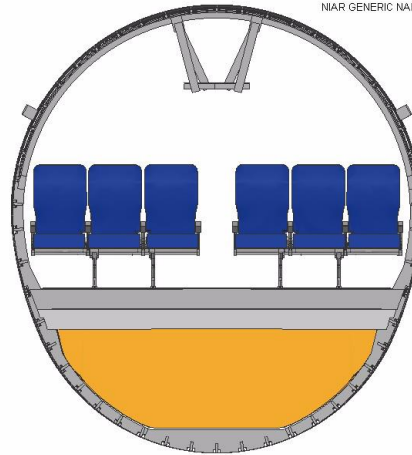
10 ft - Fuselage Section  
3 PLACE SEAT NIAR  
Time = 0.000000



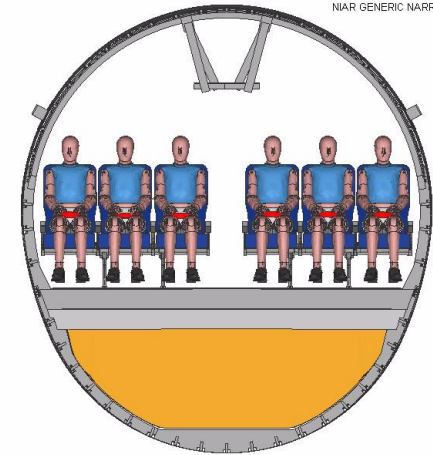
10 ft - Fuselage Section  
VIMOTECH-NIAR vATD 50th HII and 3 PLACE SEAT NIAR  
Time = 0.000000



10 ft - Fuselage Section  
NIAR GENERIC NARROW BODY - 30 ft/sec  
Time = 0.000000

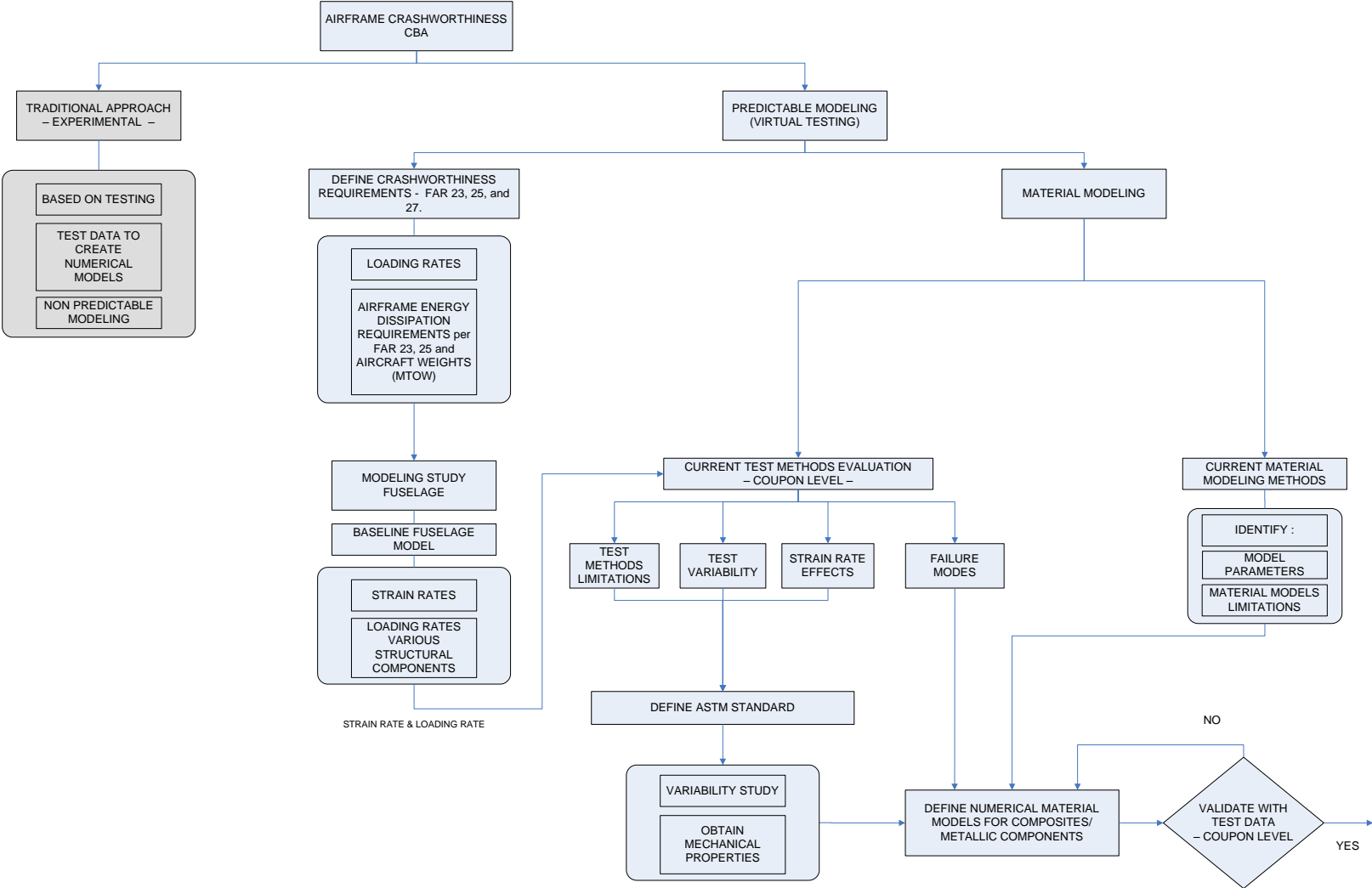


10 ft - Fuselage Section  
NIAR GENERIC NARROW BODY - 30 ft/sec  
Time = 0.000000

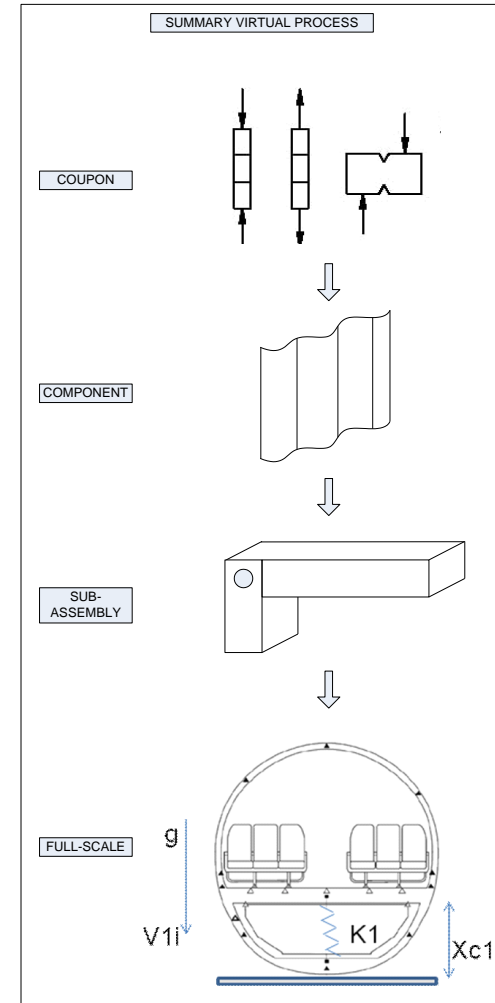
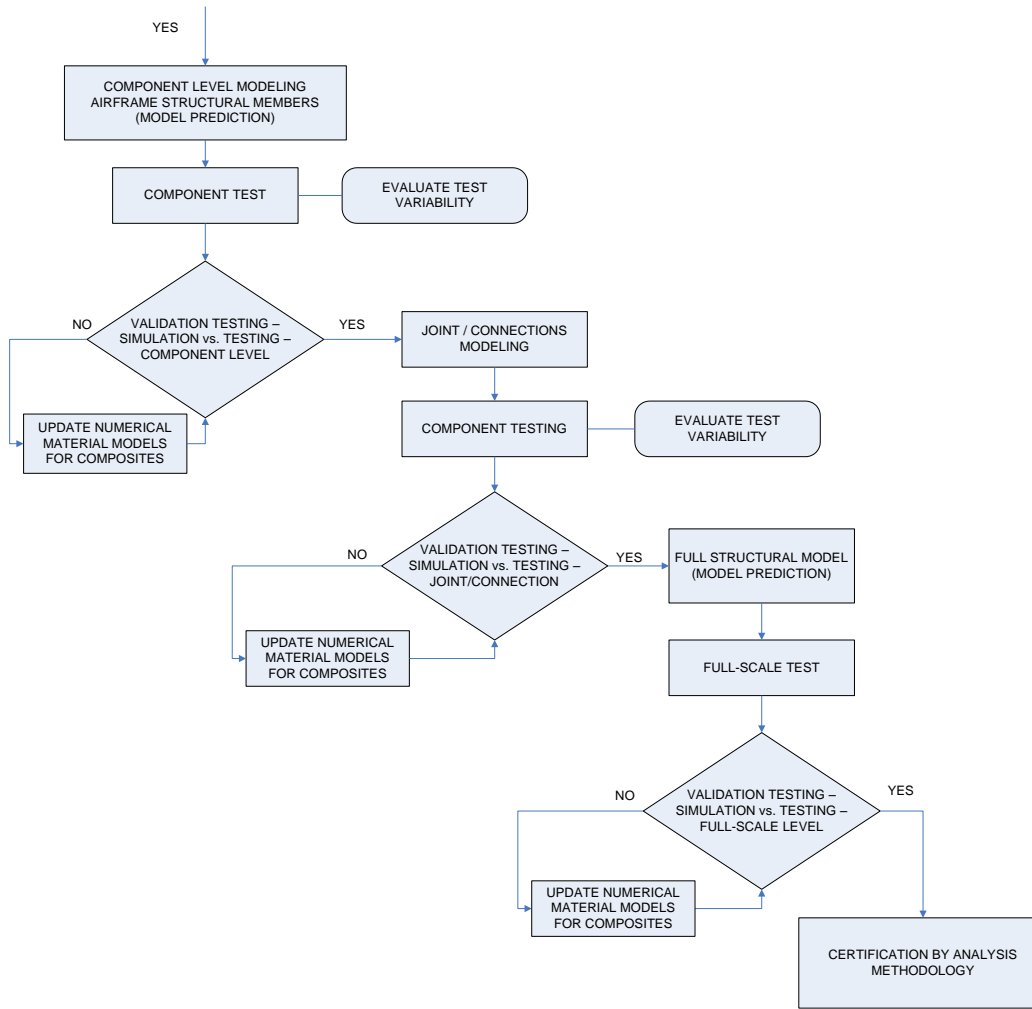


10 ft - Fuselage Section  
NIAR GENERIC NARROW BODY - 30 ft/sec  
Time = 0.000000

# Technical Approach – Airframe Crashworthiness



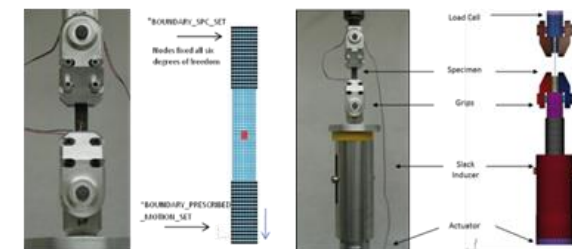
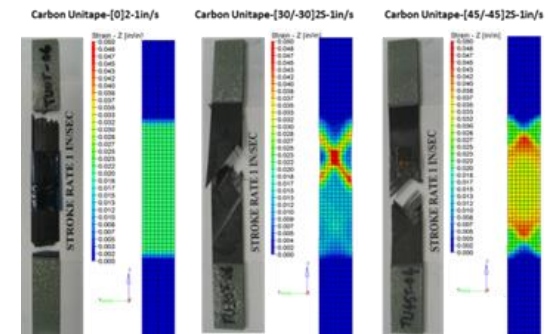
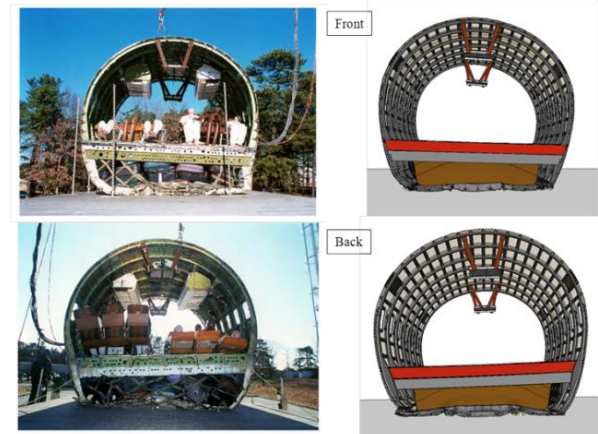
# Technical Approach – Airframe Crashworthiness



# Phase III – Aerospace Crashworthiness Structural Requirements

The following working packages were defined to develop NIAR Building Block Approach Methodology:

- WP 1. Aerospace Crashworthiness Structural Requirements Scope:**
  - Develop Detailed FE models of metallic narrow-body transport aircraft to study the crashworthiness behavior of typical metallic aircraft structures during survivable impacts on hard surfaces, soft soil, and water.
  - Study dynamic response and energy absorbing capabilities of the individual structural members (i.e. stanchions, frames, stringers, skin)
  - Effect on the structural response of various cargo (empty to full cargo configurations) and impact surfaces (rigid, soil, & water) configurations.
  - Results defined range of typical energy absorbing requirements, loading, and strain rates for the various airframe structural components.
  - Quantify Boundary Condition effects on the crashworthiness response from full aircraft models to half barrel type vertical drop test configurations.
- WP 2. Coupon Level R&D:**
  - Designers require dynamic material properties that take into account the material response at strain rates higher than quasi-static.
  - Dynamic material properties are generated from coupon level testing. Not from component level testing.
  - Coupon-level tests were conducted over a range of strain rates for which testing techniques have not yet been standardized.
  - Round Robin Exercise to develop High Rate Tension Testing.

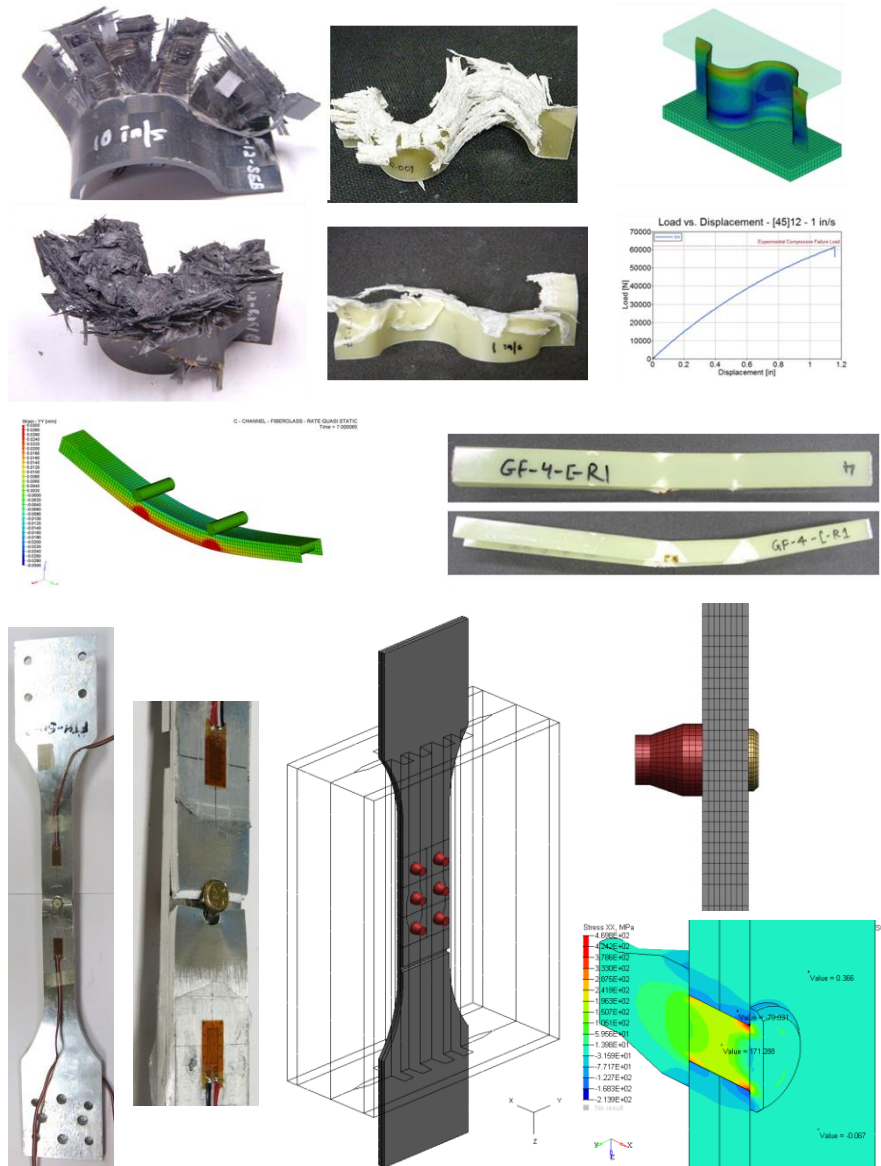




# Phase III – Aerospace Crashworthiness Structural Requirements

Working packages for NIAR Building Block Approach Methodology:

- **WP 3. Component Level R&D:**
  - Used to validate the coupon level material data generated in WP2
  - Study the strain rate sensitivity of these composite material systems at the component level.
  - Pin-Bearing, C-Section Beams, and Sine Wave Beams.
  - Results obtained in WP0 defined component level testing protocols (loading rates, strain rates, energy absorbing requirements and component level test configurations).
- **WP 4. Joints and Connections R&D:**
  - Understand limitations of different modelling techniques that can be used to join the various airframe structural members.
  - Evaluate single and multiple point load transfer mechanisms between airframe structural members.
  - Characterize the effect of loading rates.
  - Evaluate various modeling techniques and validate them with test data.



# Experimental Testing – Bolt Preload

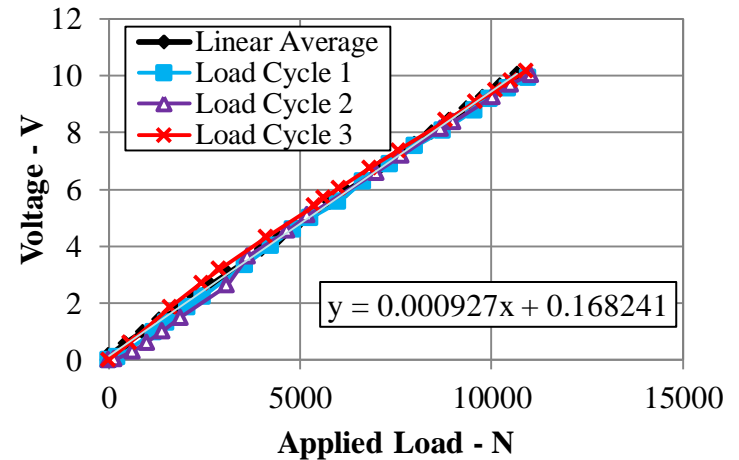
- Experimental Testing – Bolt Preload

- Test Procedure

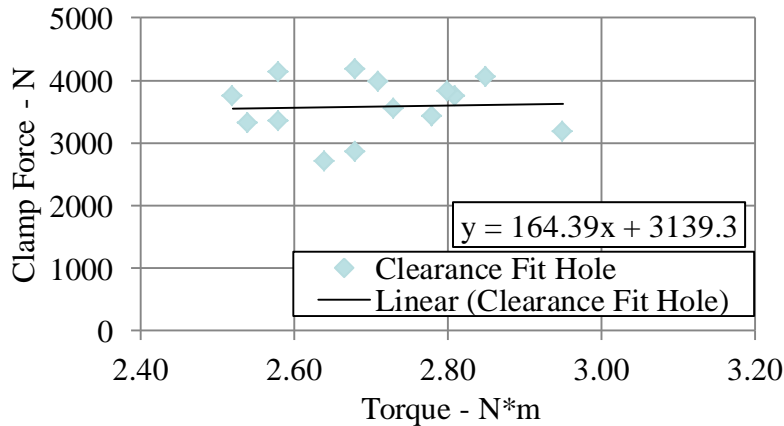
- ✓ Load Cell Verification and Signal Conditioner Calibration
    - ✓ Mounting of Test Article on Vise
    - ✓ Bolt Installation using Torque Wrench
    - ✓ Record Torque at Shear off and Voltage on Voltmeter

- Test Matrix

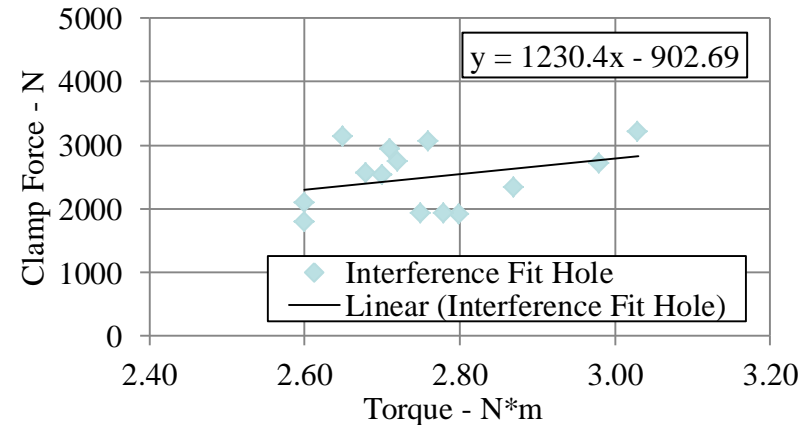
- ✓ 3 Specimen (5 Holes on Each) for Interference Fit
    - ✓ 3 Specimen (5 Holes on Each) for Clearance Fit



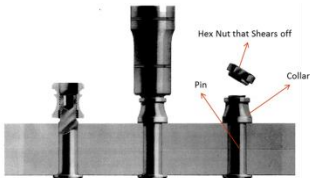
Load Cell Verification and Signal Conditioner Calibration



Clearance Fit



Interference Fit



# Experimental Testing – Material Characterization

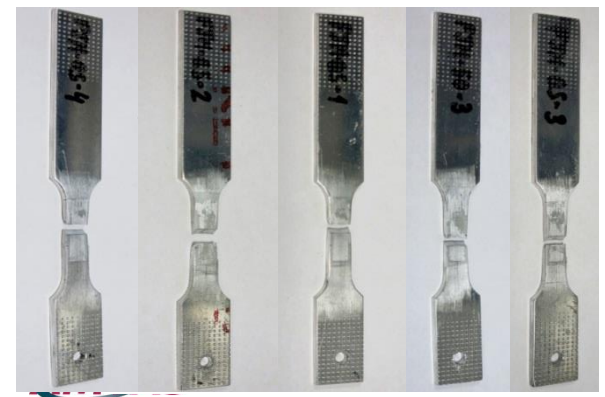
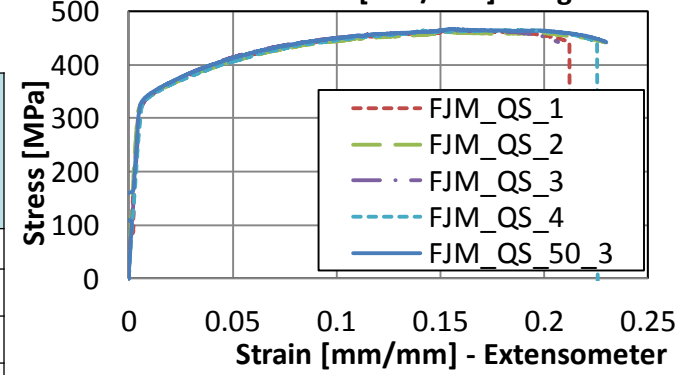
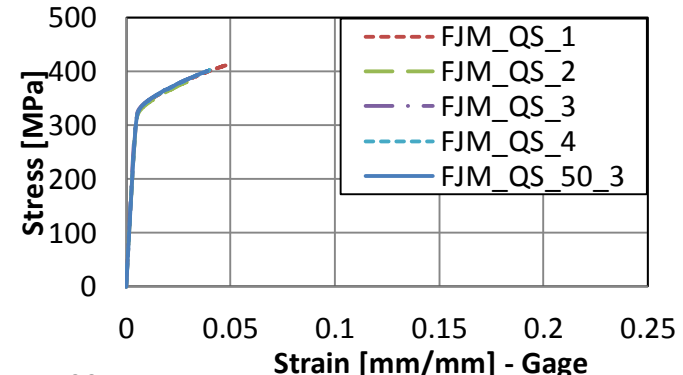
- Experimental Testing – Material Characterization

- Test Procedure

- ✓ Method – In-plane Tension
    - ✓ Rate – Quasi-static (0.0008 in/s)
    - ✓ Mount Specimen, Set-up Laser Extensometer, Load until failure

	Youngs Modulus (Strain Gage)	Yield Stress (Sgage)	Youngs Modulus (Ext.)	Yield Stress (Ext.)	Ultimate Stress (Ext.)	Failure Strain (Ext.)
	Mpa	Mpa	Mpa	Mpa	Mpa	Mm/mm
FJM_QS_1	69019.27	329.76	61347.23	334.00	464.17	0.2122
FJM_QS_2	68622.34	327.33	76493.22	328.11	461.33	0.2329
FJM_QS_3	72866.73	331.97	55837.36	333.57	464.87	0.2066
FJM_QS_4	69010.77	331.29	50307.26	335.98	464.42	0.2255
FJM_50_3_QS	69513.27	331.58	58026.73	338.50	466.68	0.2298
<b>Average</b>	<b>69806.48</b>	<b>330.38</b>	<b>60402.36</b>	<b>334.03</b>	<b>464.29</b>	<b>0.22</b>
Standard Deviation	1739.7	1.9	9851.4	3.8	1.9	0.0
Coefficient of Variation (%)	2.5	0.6	16.3	1.2	0.4	5.2

Note: Ext. - Laser Extensometer



Advanced Materials in Transport Aircraft Structures



# Testing – Load Transfer Tests – Setup

- Experimental Testing – Load Transfer Tests

- Test Article

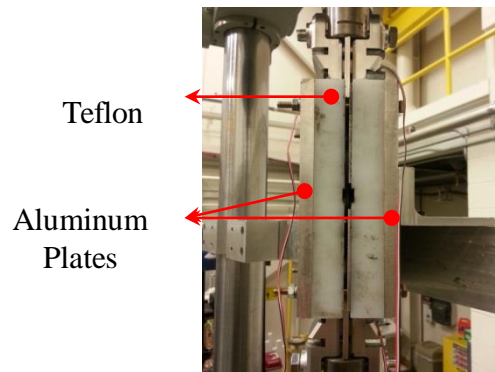
- ✓ One-Half Dog Bone Specimen
- ✓ Hi-Lok Fastener - HL18 Pin/ HL70 Nut

- Test Apparatus

- ✓ MTS High Stroke Servo-Hydraulic Machine
- ✓ Slack Inducer System
- ✓ Anti-Buckling Fixture (ABF)
- ✓ Arm to constrain ABF

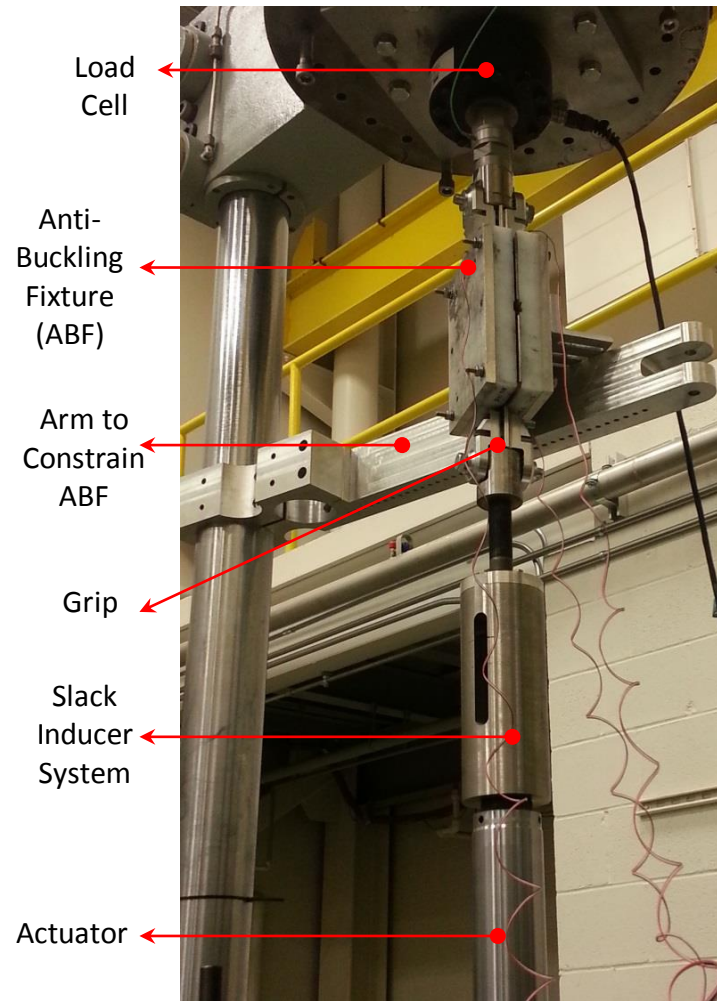
- Data Acquisition

- ✓ 11 Kip Strain Gage Based LoadCell
- ✓ 3 Axial Strain Gages – CAE-06-250UN-350



Teflon

Aluminum  
Plates



Load  
Cell

Anti-  
Buckling  
Fixture  
(ABF)

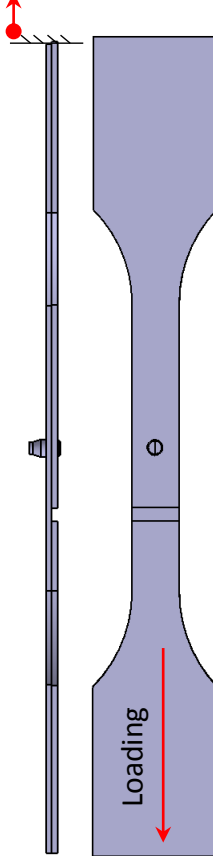
Arm to  
Constrain  
ABF

Grip

Slack  
Inducer  
System

Actuator

Fixed End

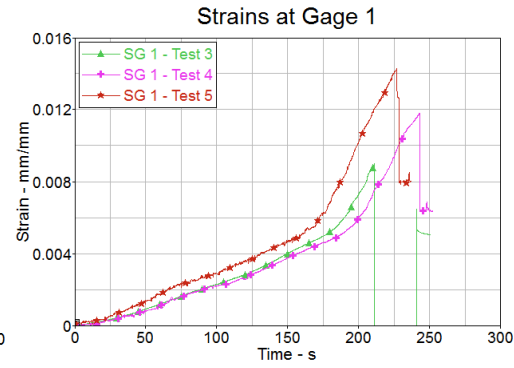
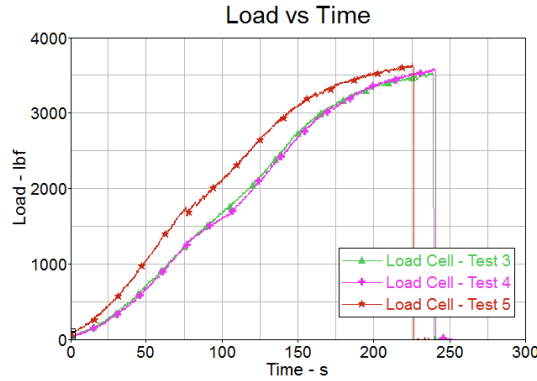
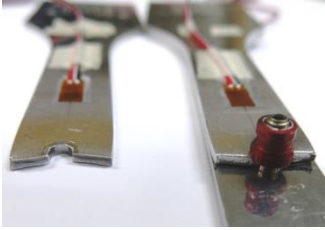


Test  
Specimen

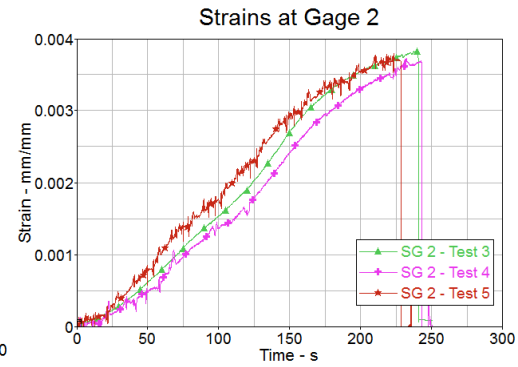
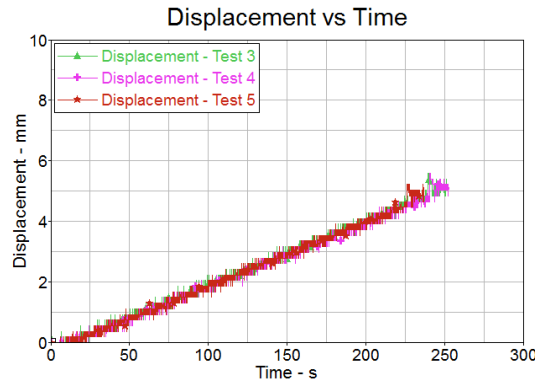
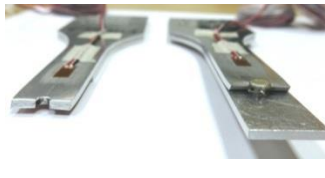


# Testing – Load Transfer Tests - Results

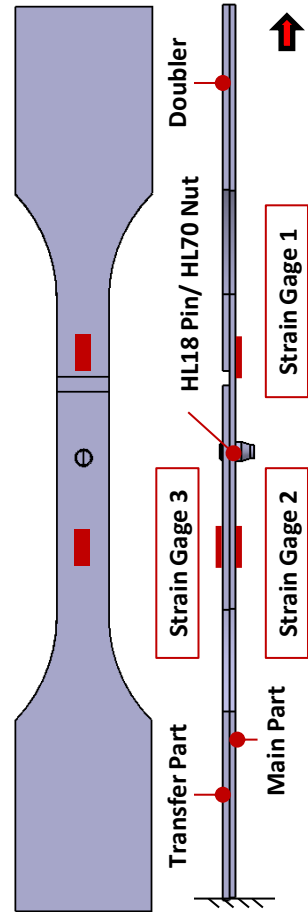
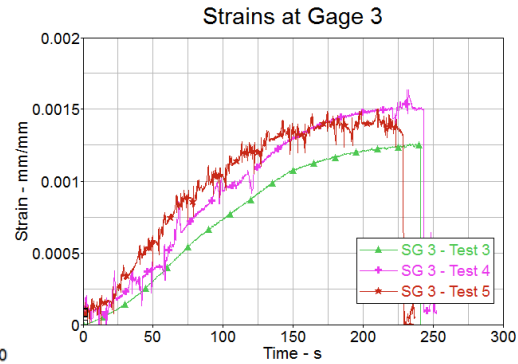
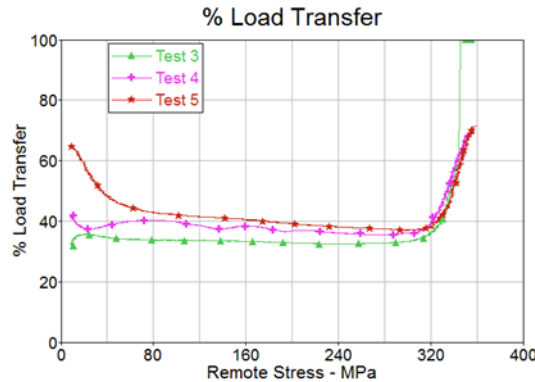
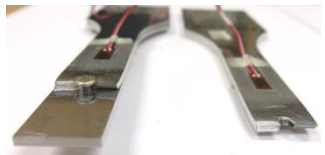
Test 3



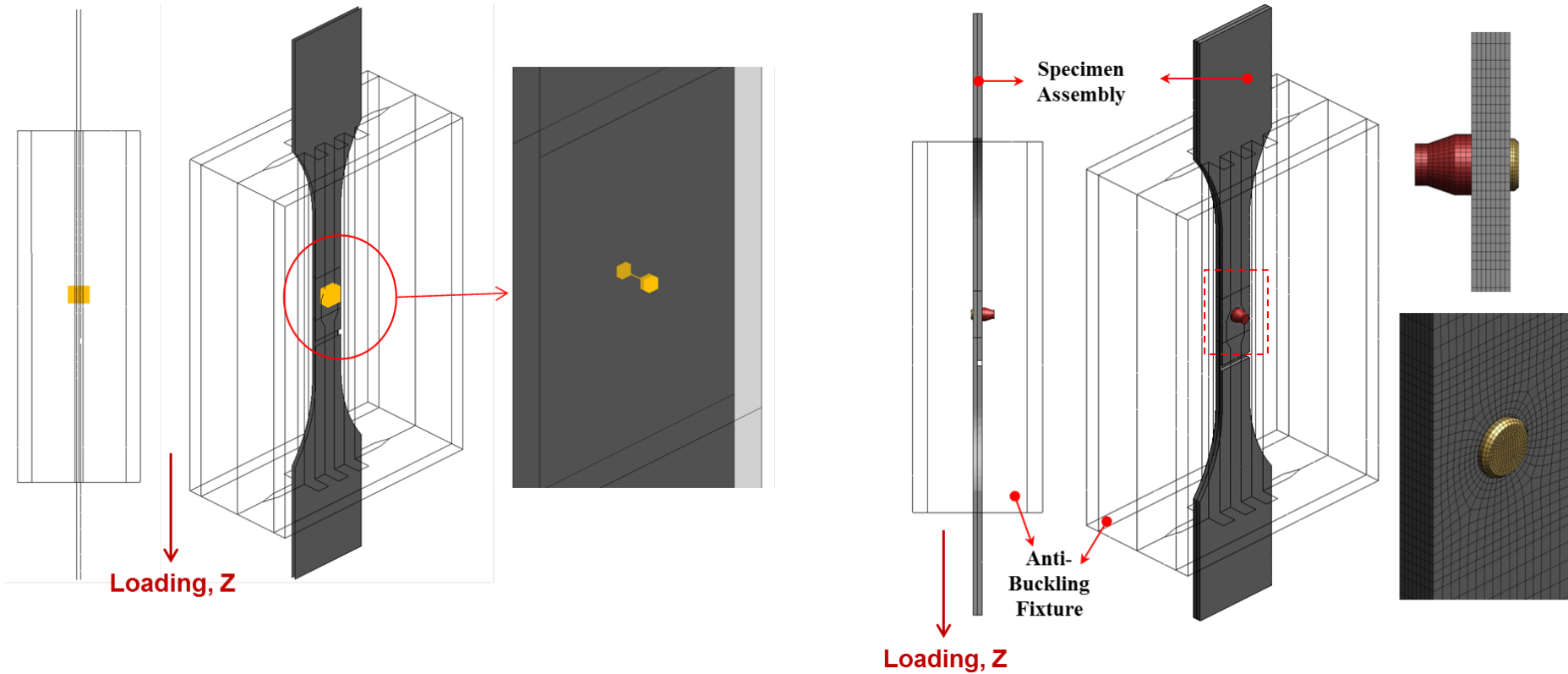
Test 4



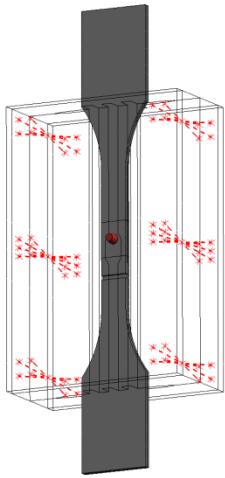
Test 5



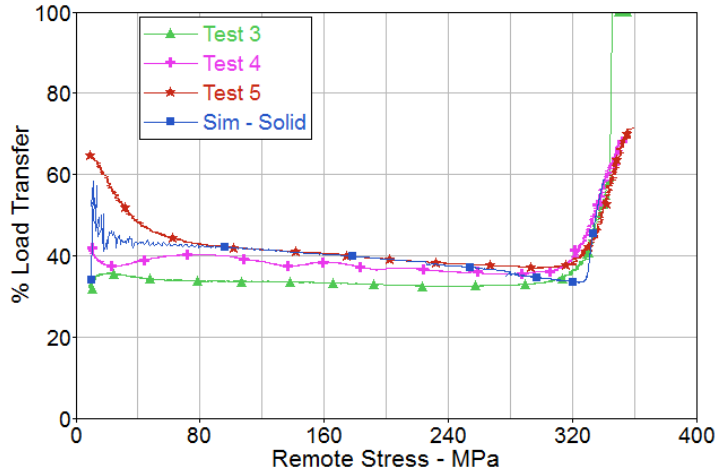
# FE Model – Solid and Spot-weld Beam Models



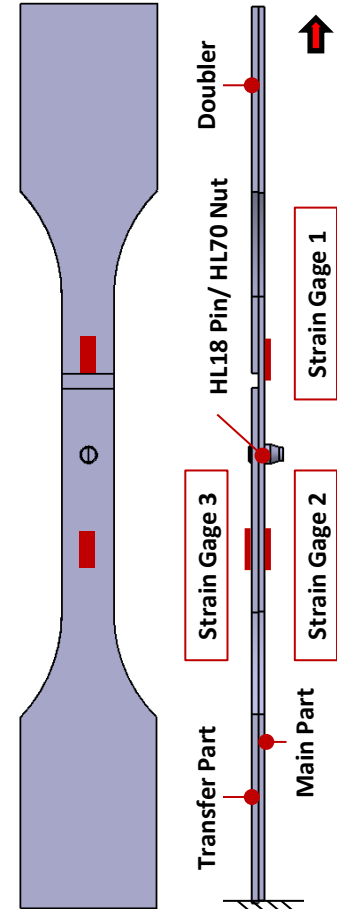
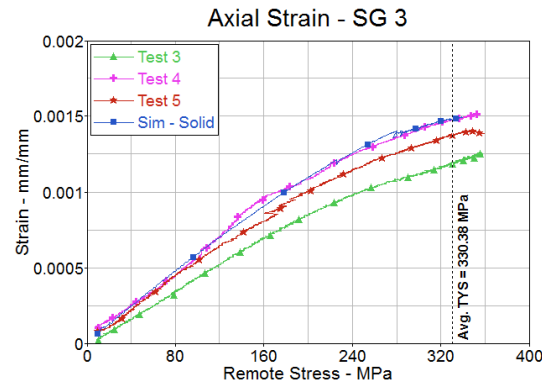
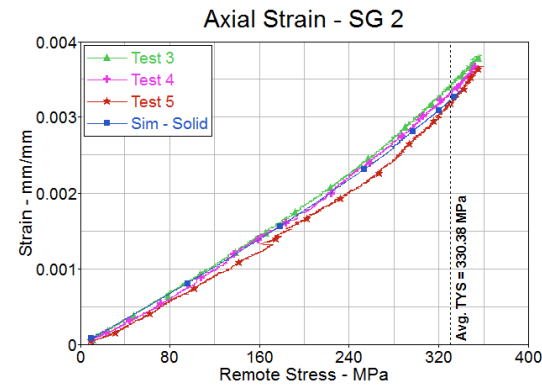
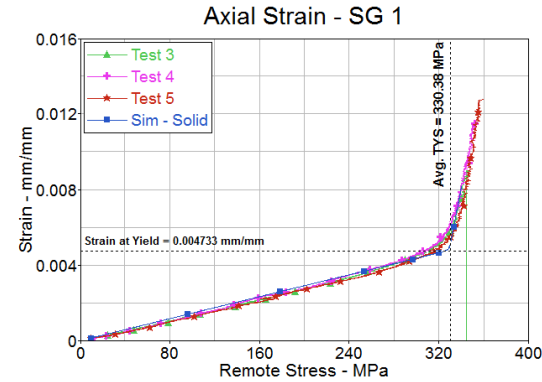
# FE Model – Validation of Modeling Methods



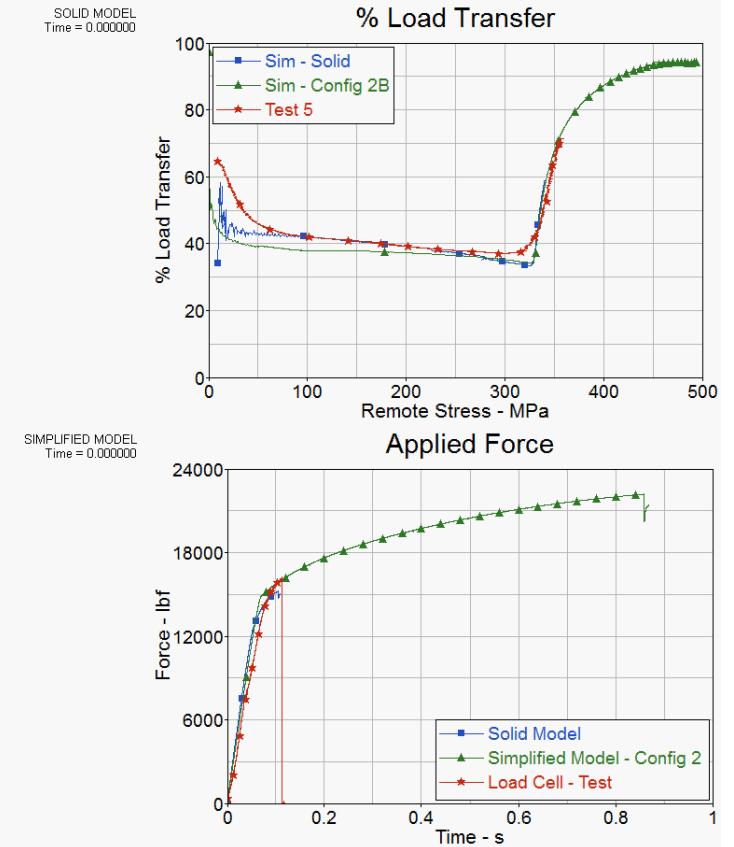
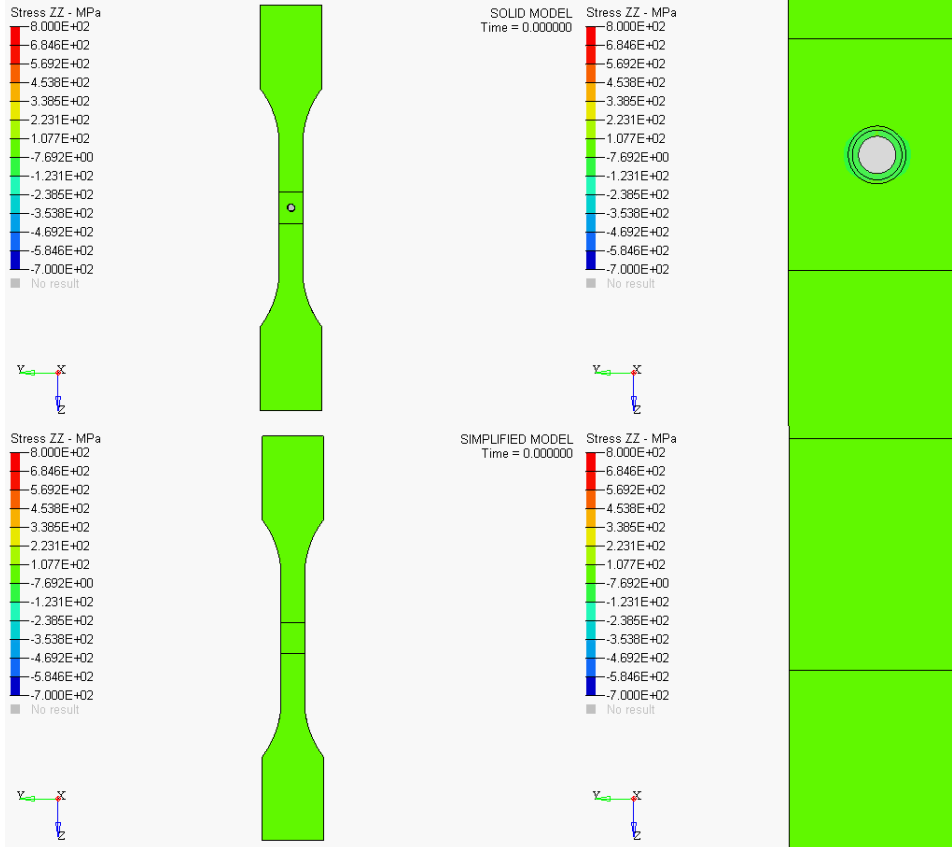
% Load Transfer



$$\% \text{ Load Transfer} = \left[ 1 - \left( \frac{SG\ 2}{SG\ 1} \right) \right] \times 100\%$$



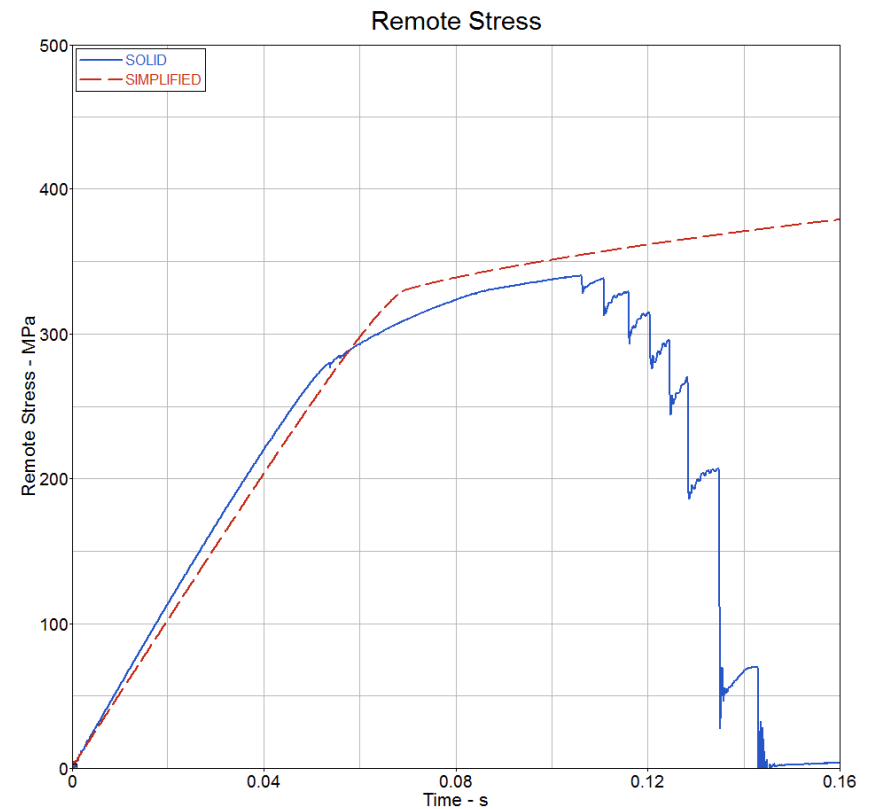
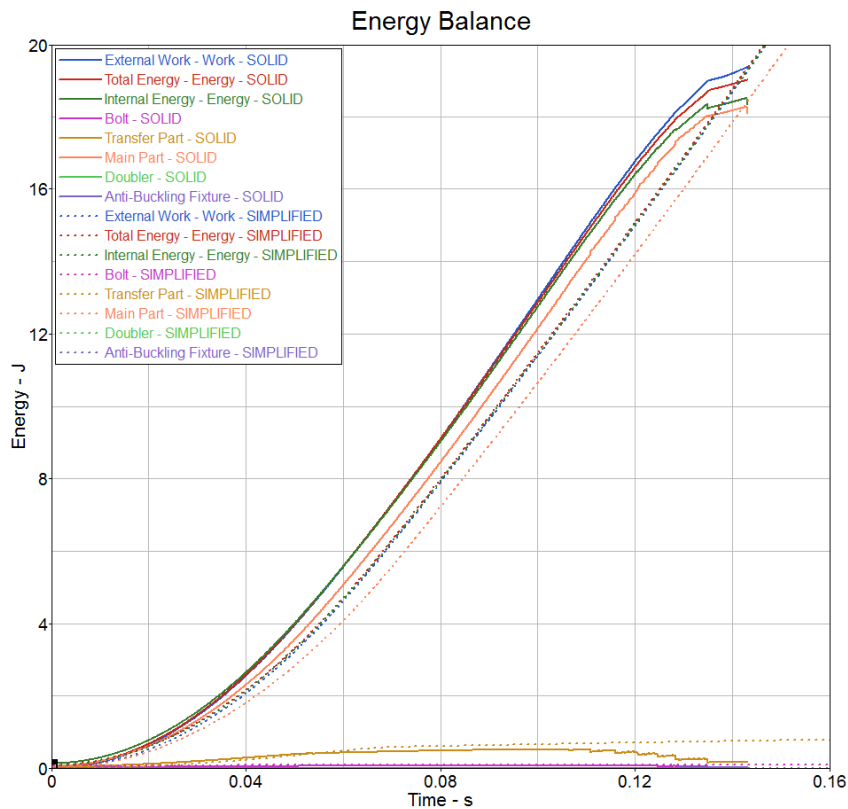
# Solid vs. Beam Spot Weld





# Single Point Load Transfer – Energy Balance

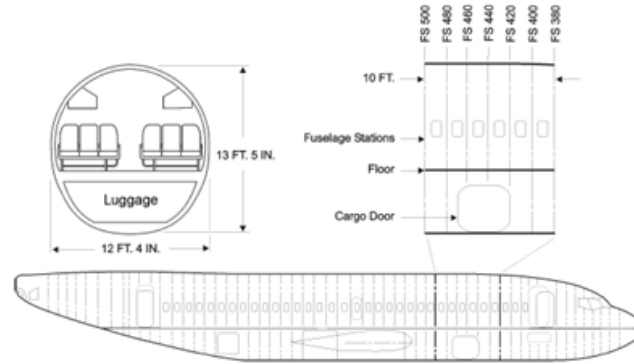
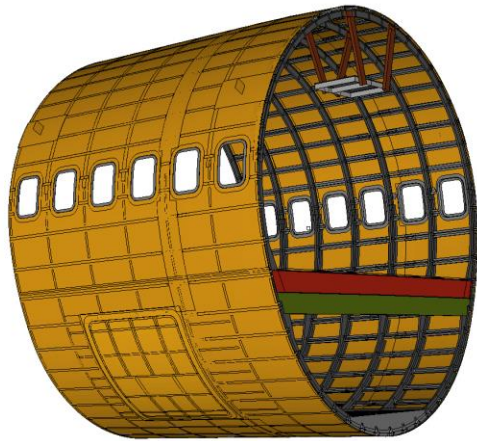
- **Solid vs. Simplified**



# Section Level – Drop Test Model Update

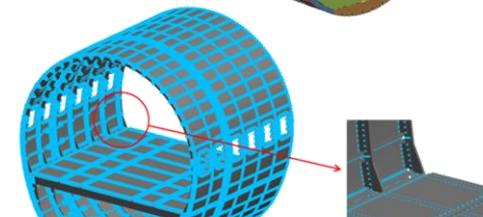
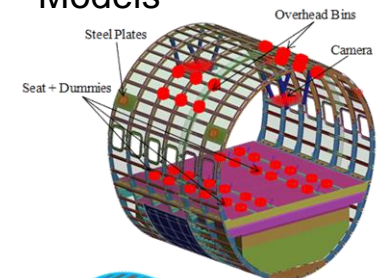
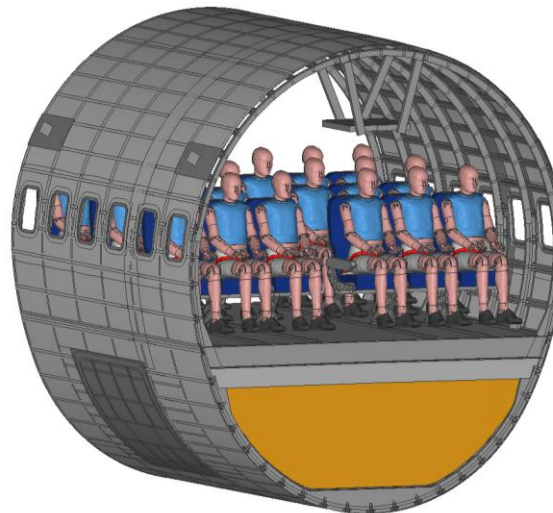
## Model Updates:

- **Coupon Level R&D:**  
Updated Material Models for Structural Members
- **Joint Level R&D:**  
Updated Joint Types, Contacts, Friction and Material Type Definitions
- **Updated vATD**  
Occupant and Seat Models

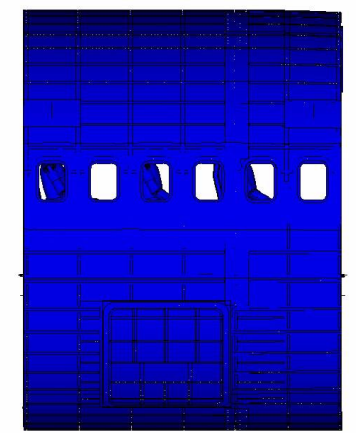
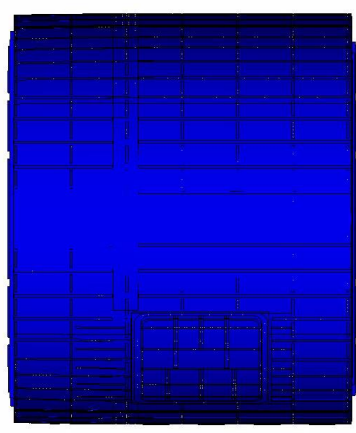
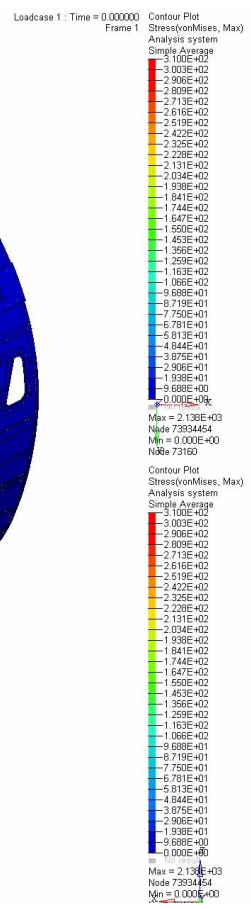
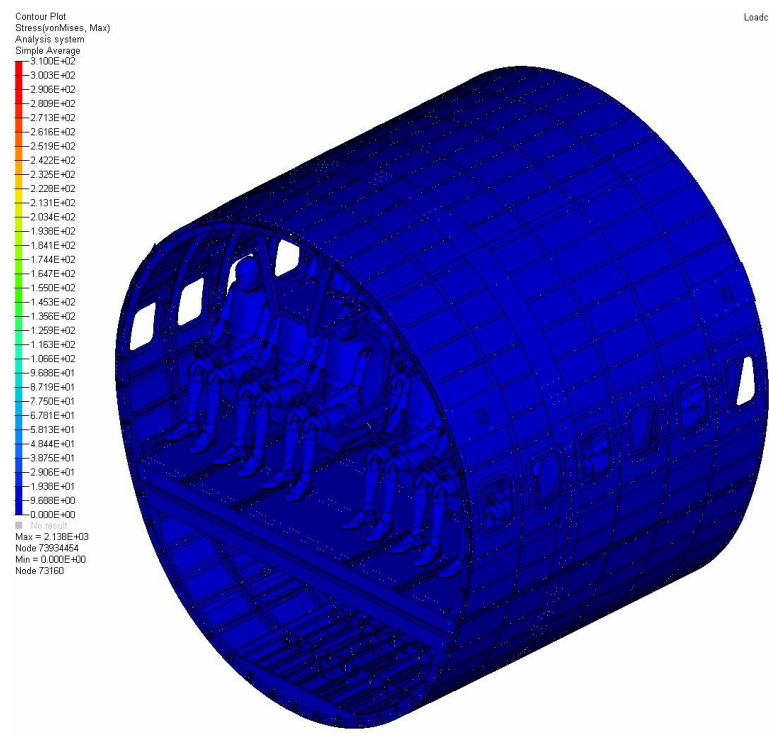


Cargo Door

Reinforced Beam



# Section Level – Kinematics and Stress Distribution



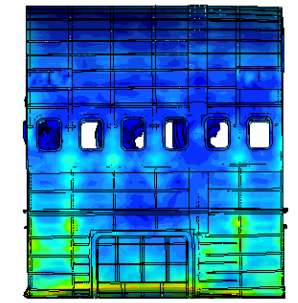
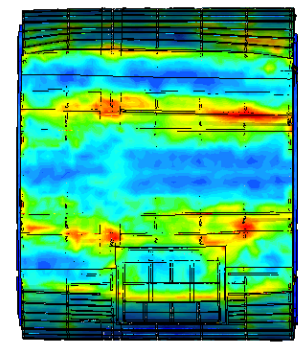
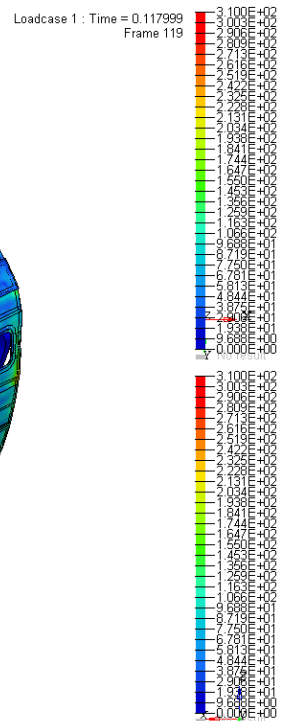
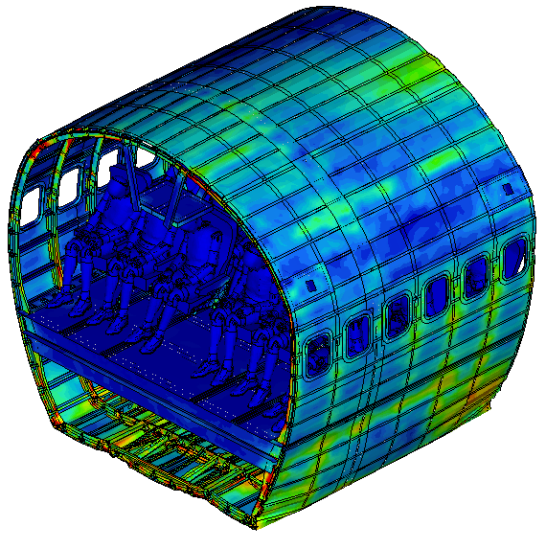
# Section Level –Stress Distribution (MPa)

- Time Max. Compression – 117 ms
- Yield Stress 310 Mpa

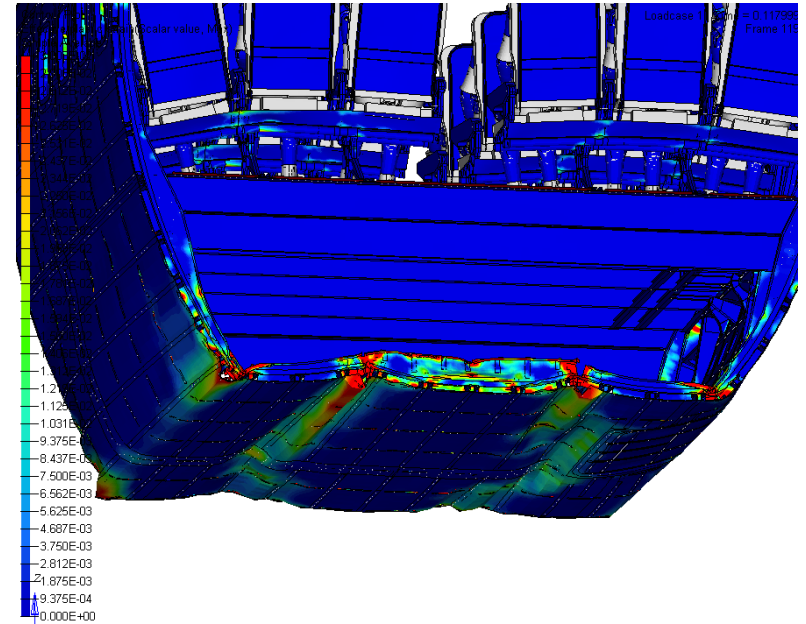
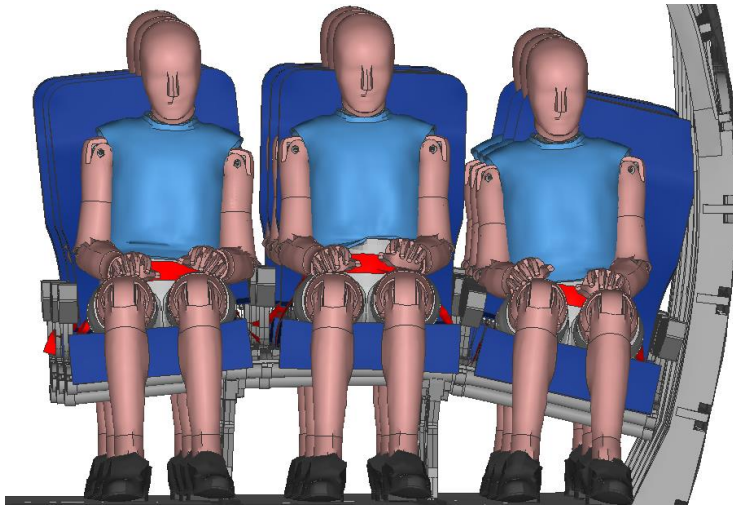
Contour Plot  
Stress(vonMises, Max)  
Analysis system  
Simple Average

3.100E+02  
3.003E+02  
2.906E+02  
2.809E+02  
2.713E+02  
2.616E+02  
2.519E+02  
2.422E+02  
2.325E+02  
2.228E+02  
2.131E+02  
2.034E+02  
1.938E+02  
1.841E+02  
1.744E+02  
1.647E+02  
1.550E+02  
1.453E+02  
1.356E+02  
1.259E+02  
1.163E+02  
1.066E+02  
9.688E+01  
8.719E+01  
7.750E+01  
6.781E+01  
5.813E+01  
4.844E+01  
3.875E+01  
2.906E+01  
1.938E+01  
9.688E+00  
0.000E+00

No Result



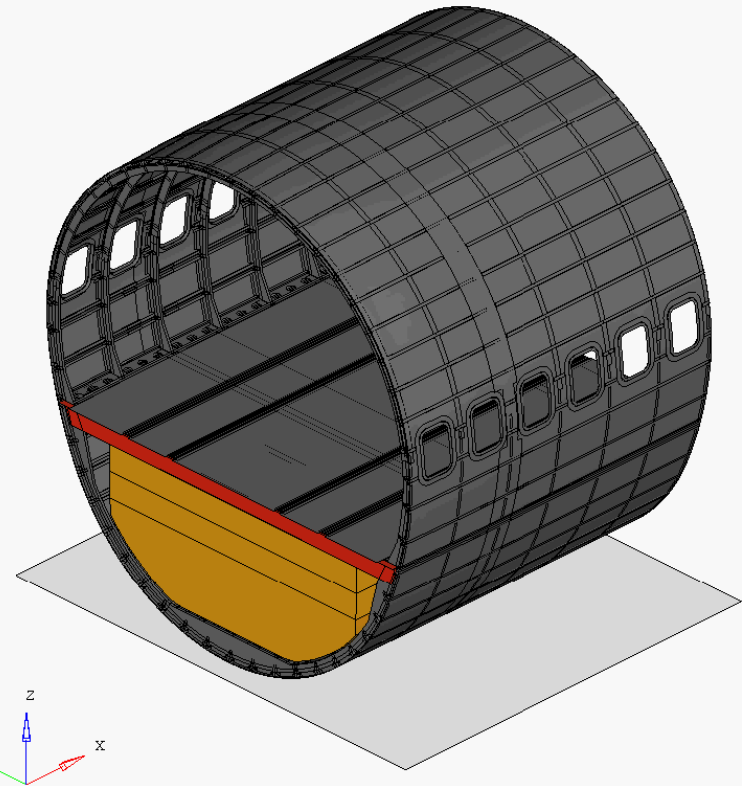
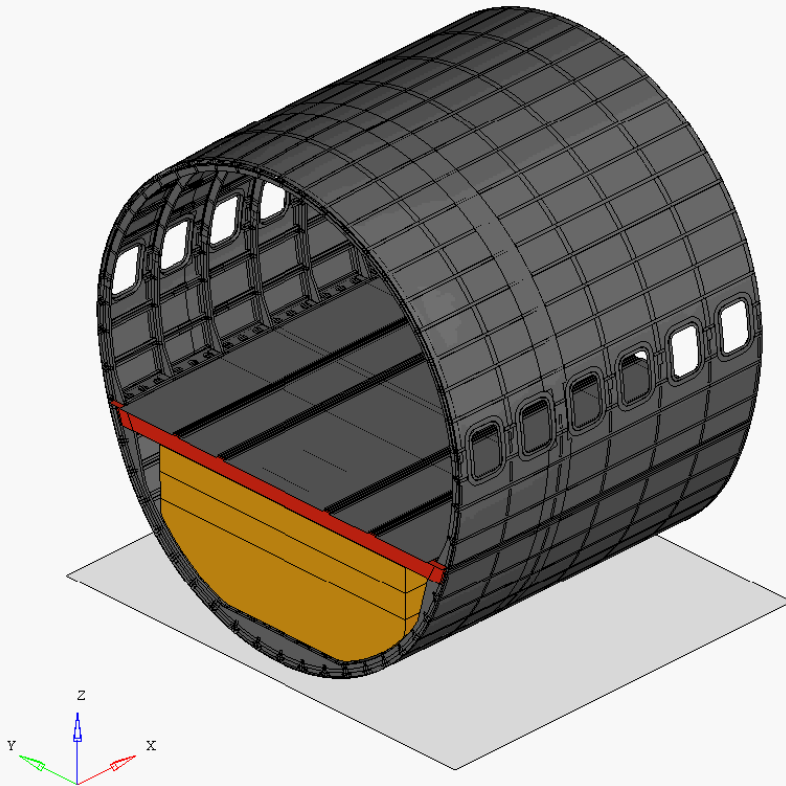
# Effective Plastic Strain – Post Damage Eval



# 30 ft/s - Full Cargo Symmetric Configuration

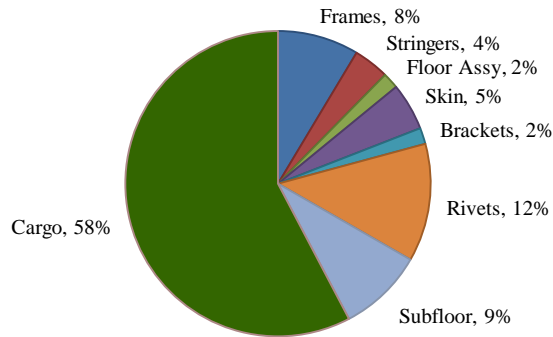
10FT Section - OLD  
Time = 0.000000

10FT Section - NEW  
Time = 0.000000



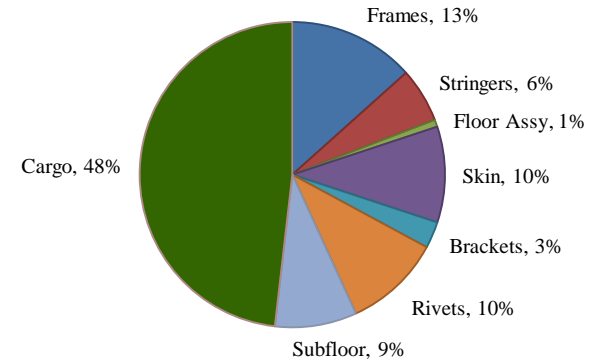
# Cargo Configuration – Energy Distribution

Old Model



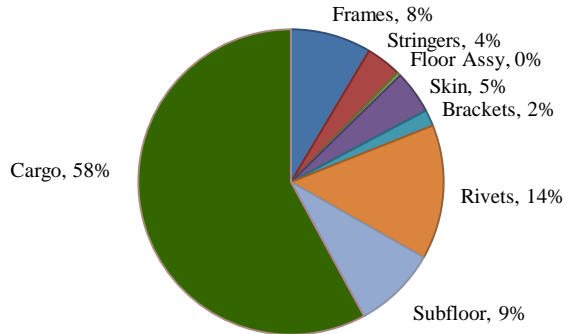
Time = 110ms

Updated Model



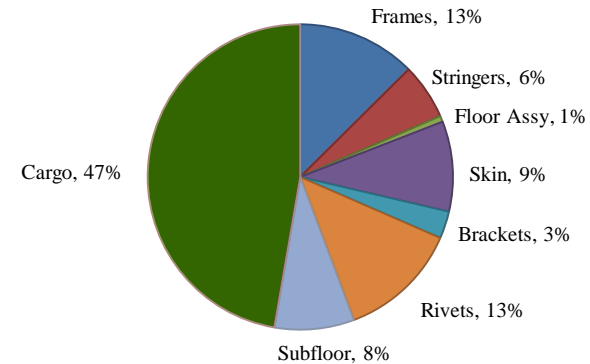
Time = 118ms

Old Model



Time = 300ms

Updated Model

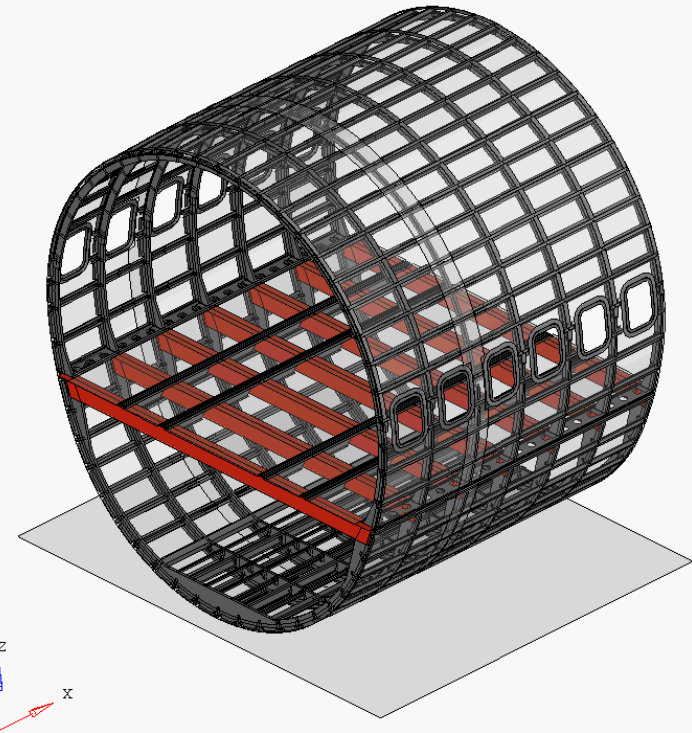
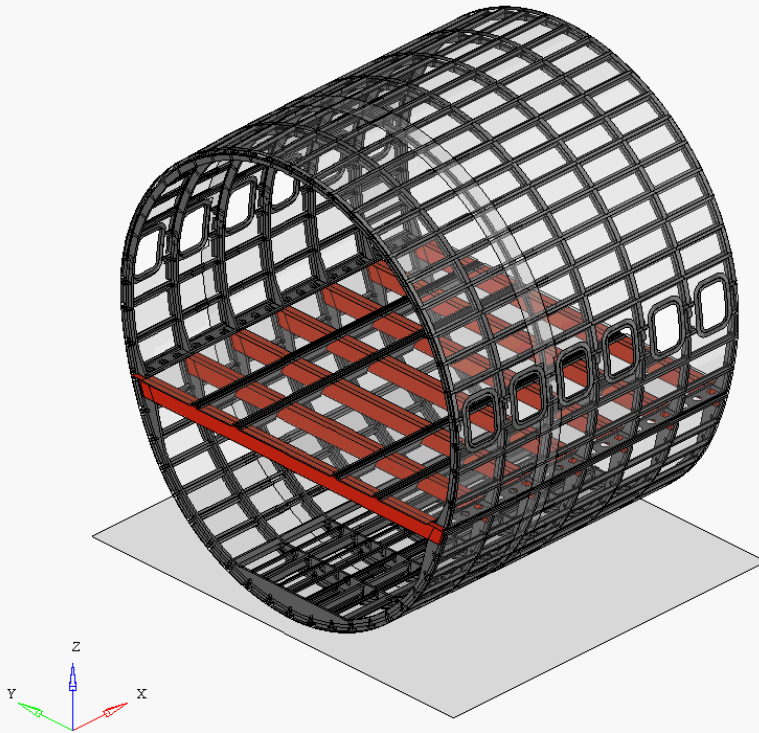


Time = 300ms

# 30 ft/s - no Cargo Symmetric Configuration

10FT Section - OLD  
Time = 0.000000

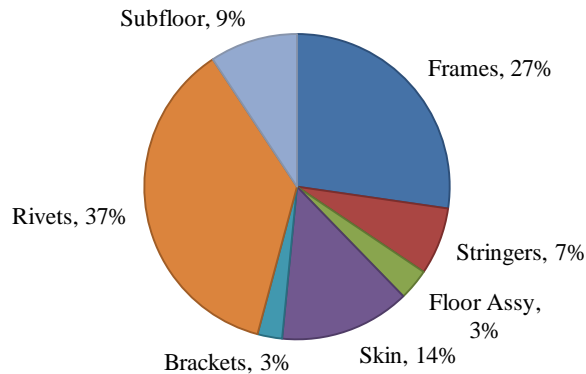
10FT Section - NEW  
Time = 0.000000





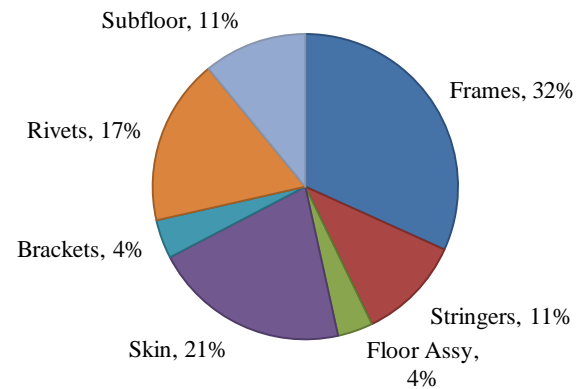
# 30 ft/s - no Cargo Configuration

Old Model



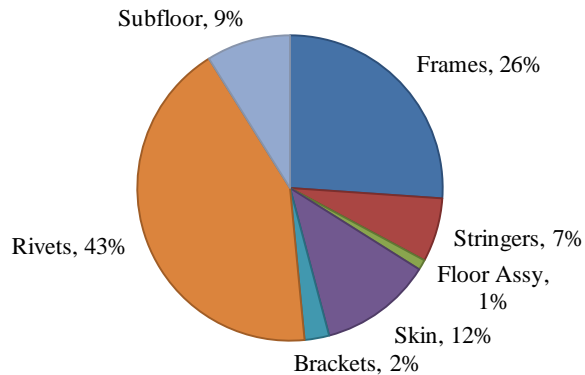
Time = 157m s

Updated Model



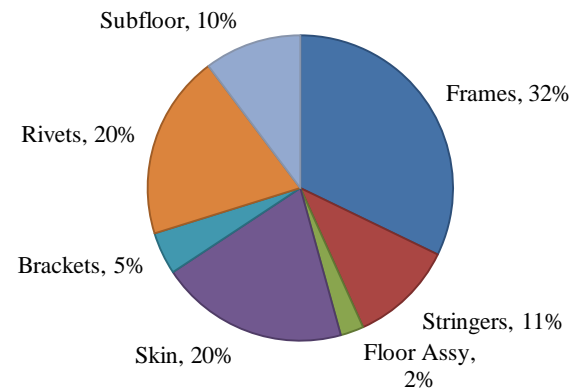
Time = 157m s

Old Model



Time = 300m s

Updated Model



Time = 300m s

# Modeling Fastener Joints – Observations

- Solid Model
  - Shows good correlation to Test Data
- Simplified Techniques
  - Rigid Body Element (RBE) – Load Transfer shows good correlation to Solid Model
  - Mesh Independent Spotweld Beam – Some configurations show good correlation of Load transfer to Solid Model while others deviate. The location of the beam model with respect to element is difficult to control in large models where parts are meshed independently
  - Mesh Independent Spotweld Beam with Patch - Some configurations show good correlation of Load transfer to Solid Model while others deviate
  - Note that although the load transfer may agree with the solid model, for some of the simplified techniques the absence of fastener hole means that Stress Concentrations around hole are not present. This alters the stress distribution and profile of the joint and will also affect the failure mode
  - It was also noted that Simplified techniques failed at different locations (not necessarily in the vicinity of the hole) and at a later time (since no hole allows more load to be transferred)
- Preload
  - Solid Model – Shows 2.5% Drop in load transfer with no preload
  - Beam Model – Shows no drop in load transfer



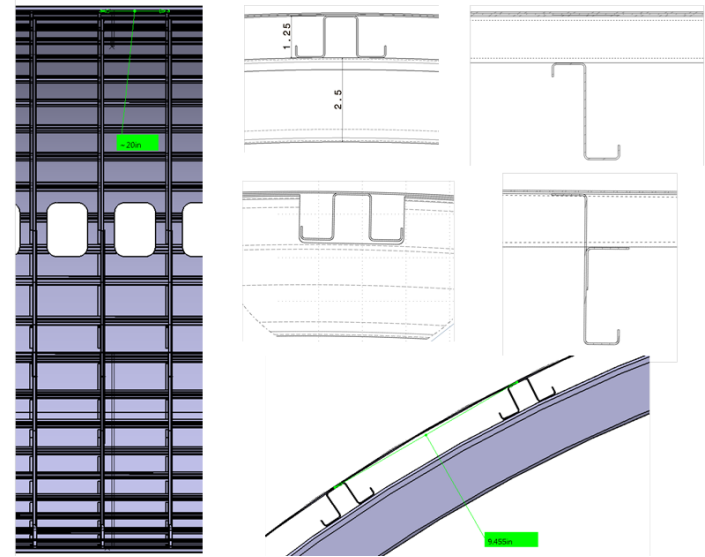
# **Accident Reconstruction 737 Flight TK 1951**

Full Scale Structural Evaluation

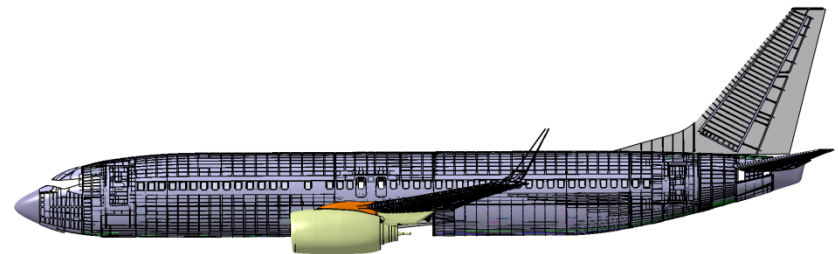
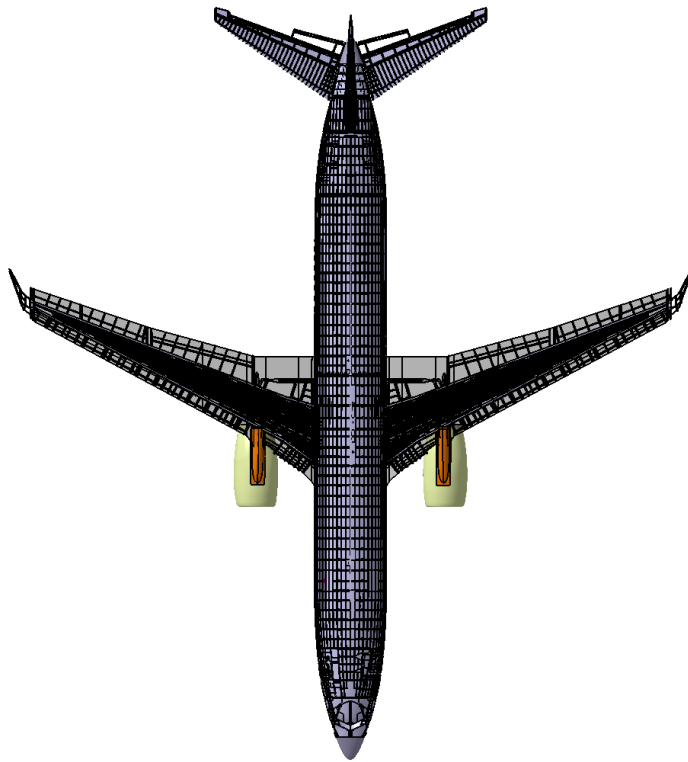
JAMS 2015 Technical Review  
April 1, 2015

# Accident Reconstruction 737 Flight TK 1951

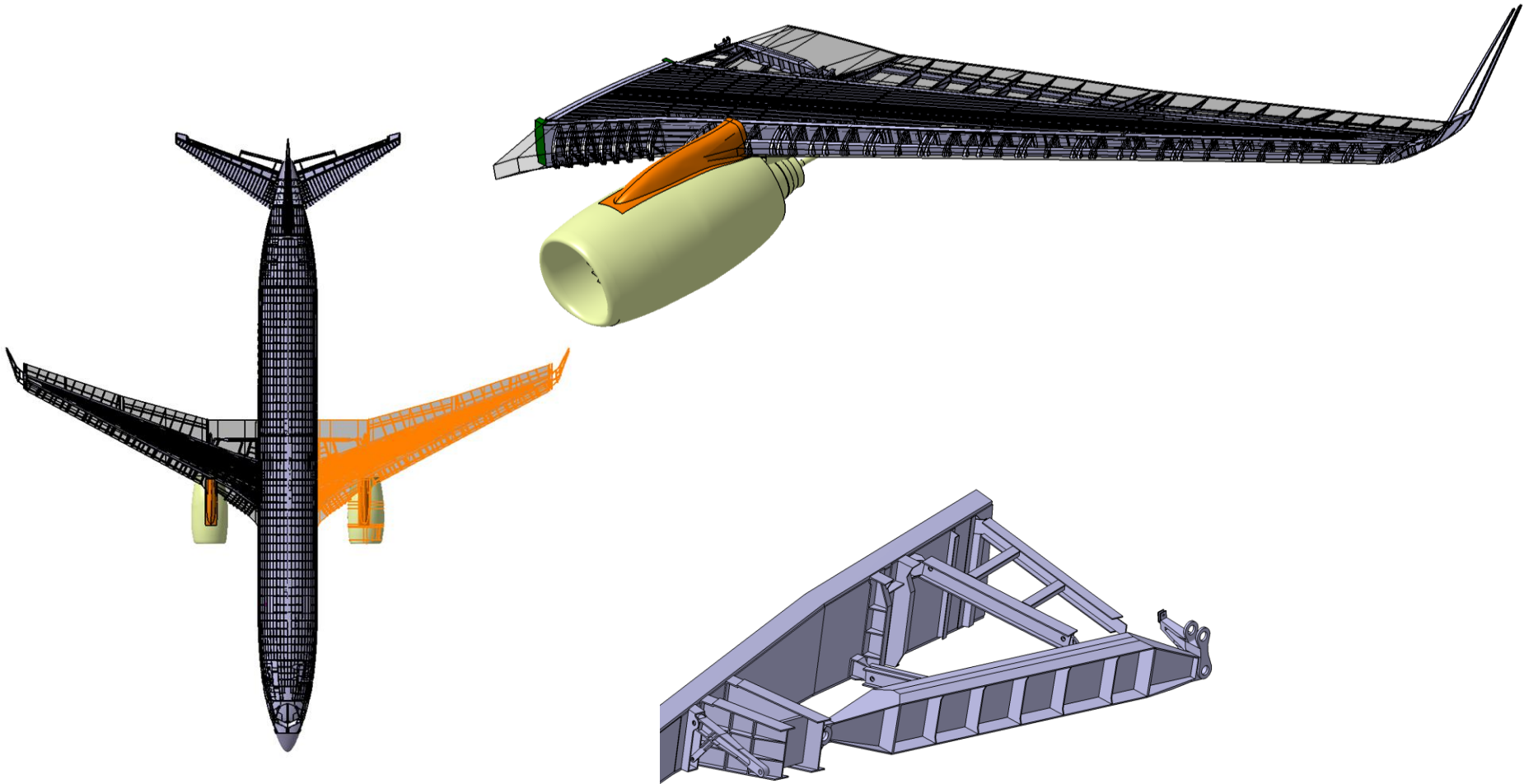
- Full Scale Structural Evaluation
  - Accident Reconstruction
    - Validate the full aircraft model response with the data available from the Turkish Airlines Flight that crashed during landing to Amsterdam Schiphol Airport, Netherlands, on February 25<sup>th</sup>, 2009
  - Structural Evaluation
    - Define a new CAD Model of Narrow Body - 800 configuration to represent as close as possible the actual geometry
    - Pending Work
      - Interface between the engine
      - Wing structure
      - Exit doors structure
      - Supporting structure for the landing gear system
    - Soil Model Validation and Evaluation - complete
  - V&V Accident Dataset:
    - Pending meeting with FAA, EASA, and Dutch Authorities after legal issues are clear



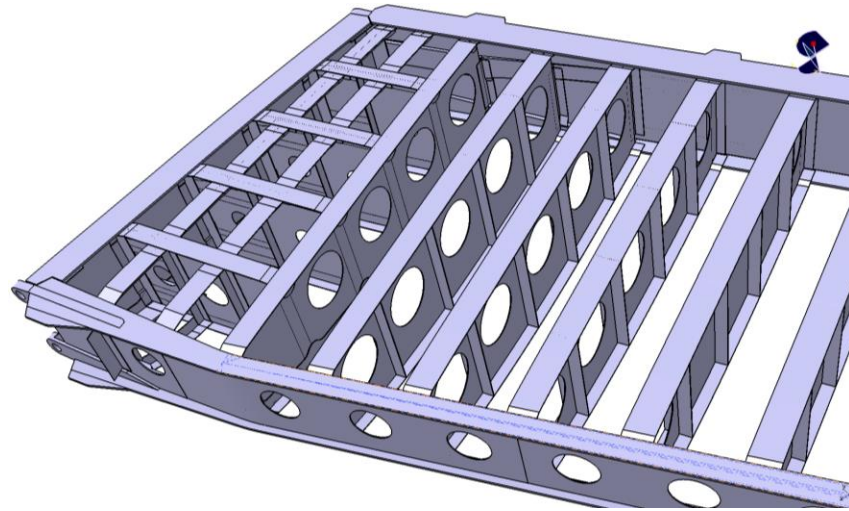
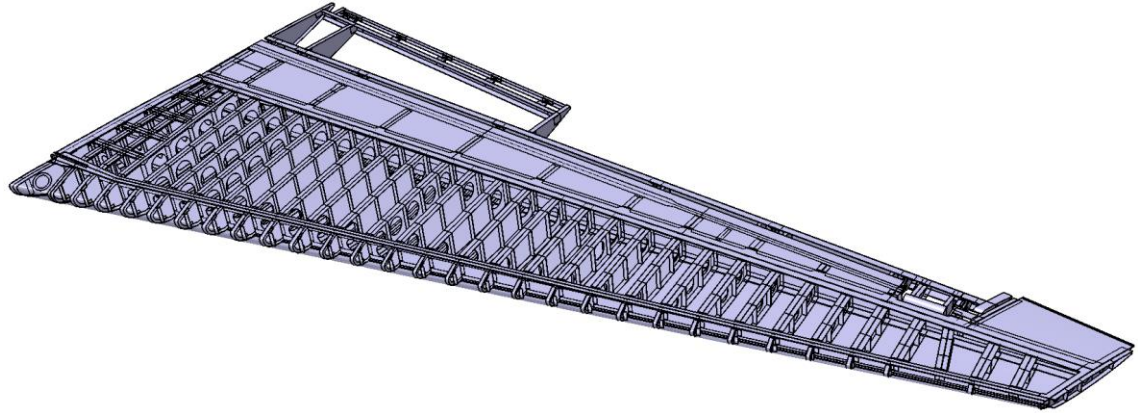
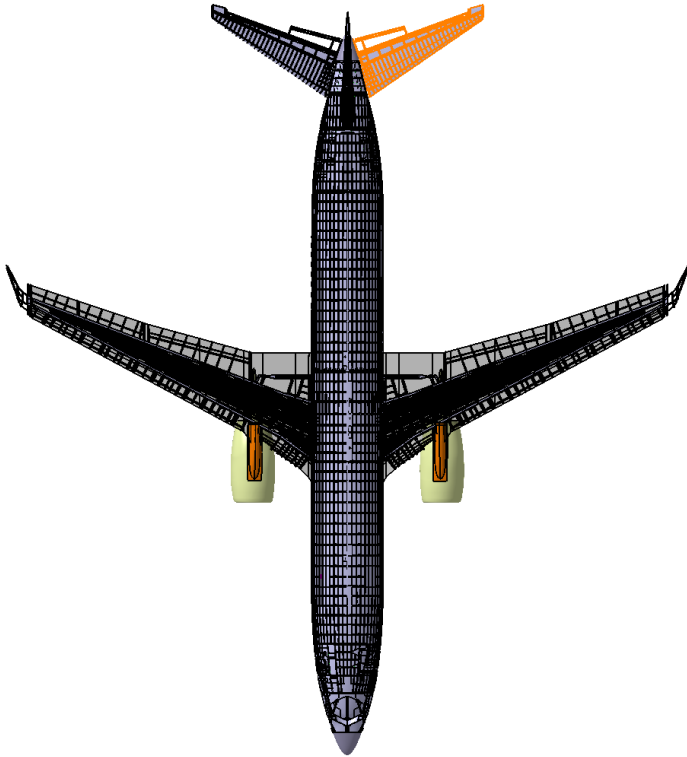
# CAD Model Definition



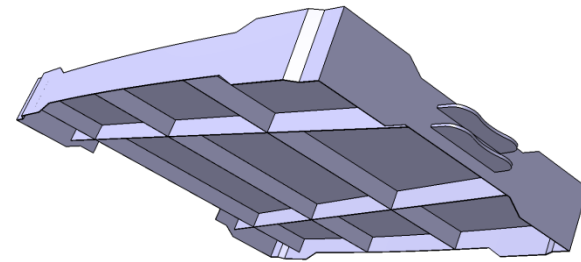
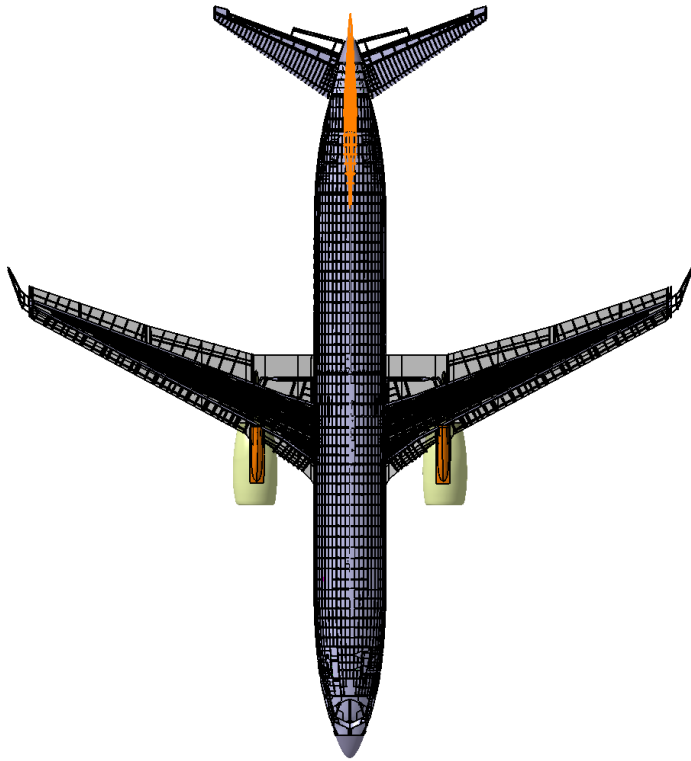
# Wing- Trailing Edge Fittings



# Horizontal Tail- Front Spar w/ Ribs

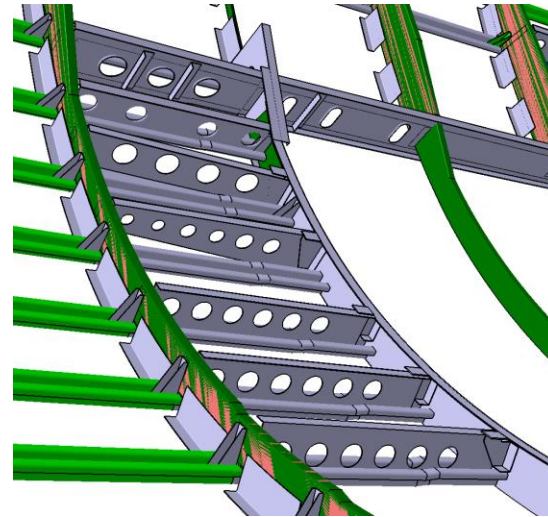
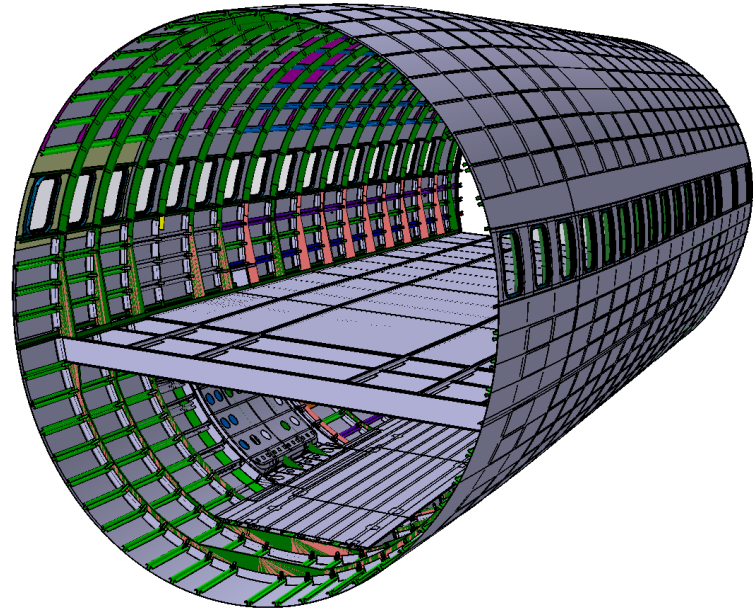
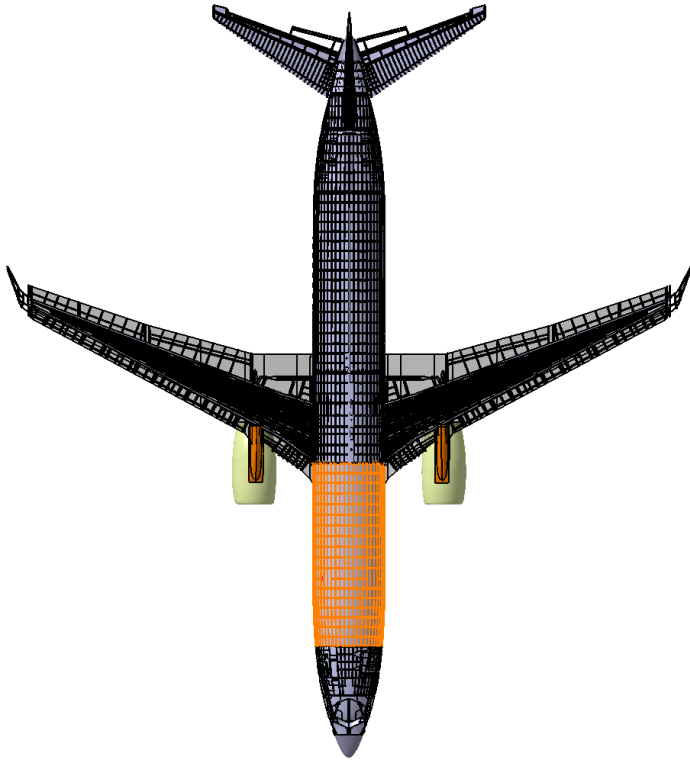


# Vertical Tail- Rudder Hinge Fitting

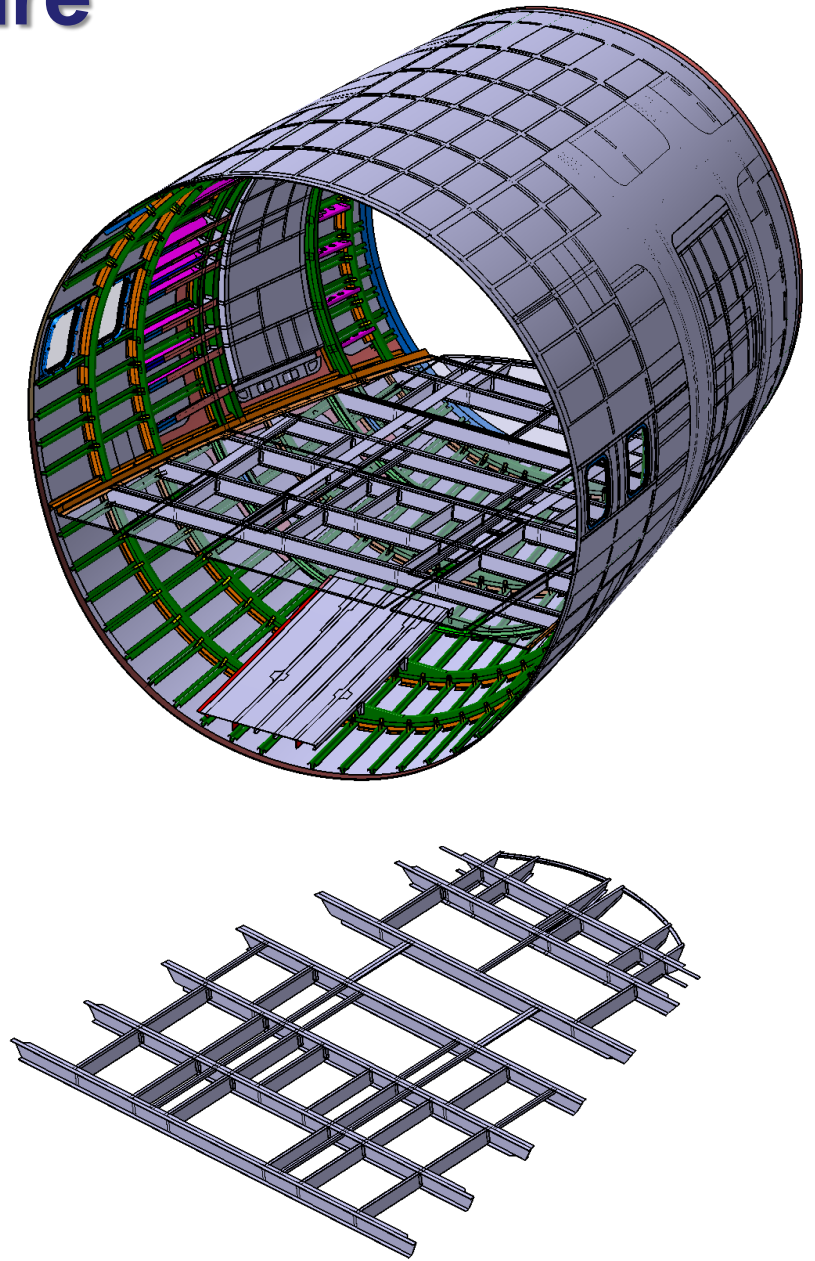
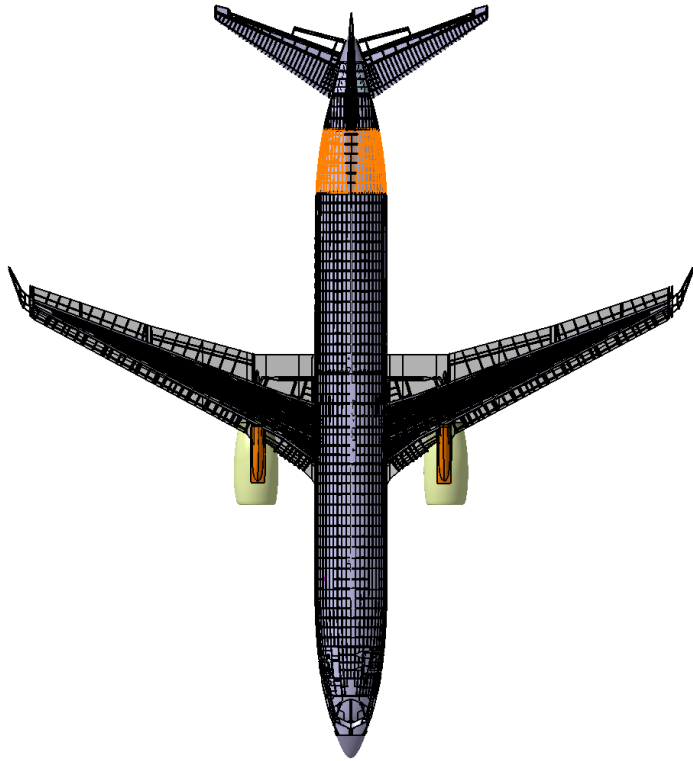




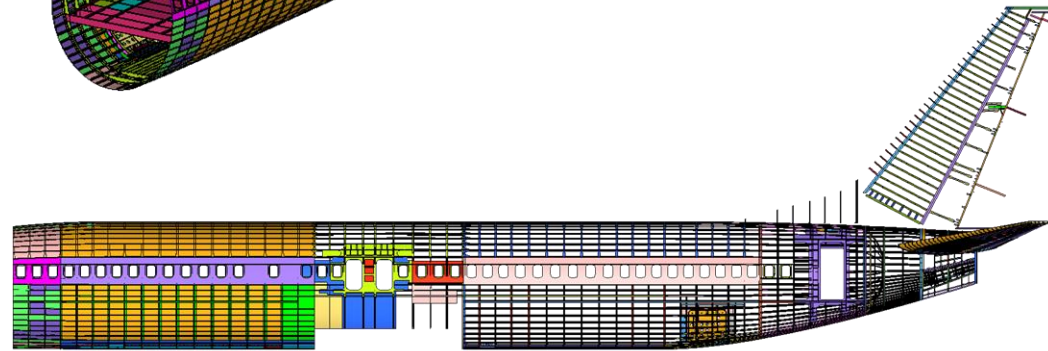
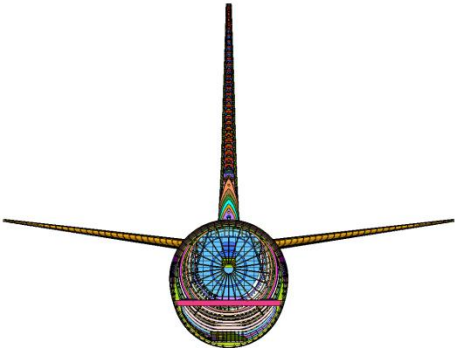
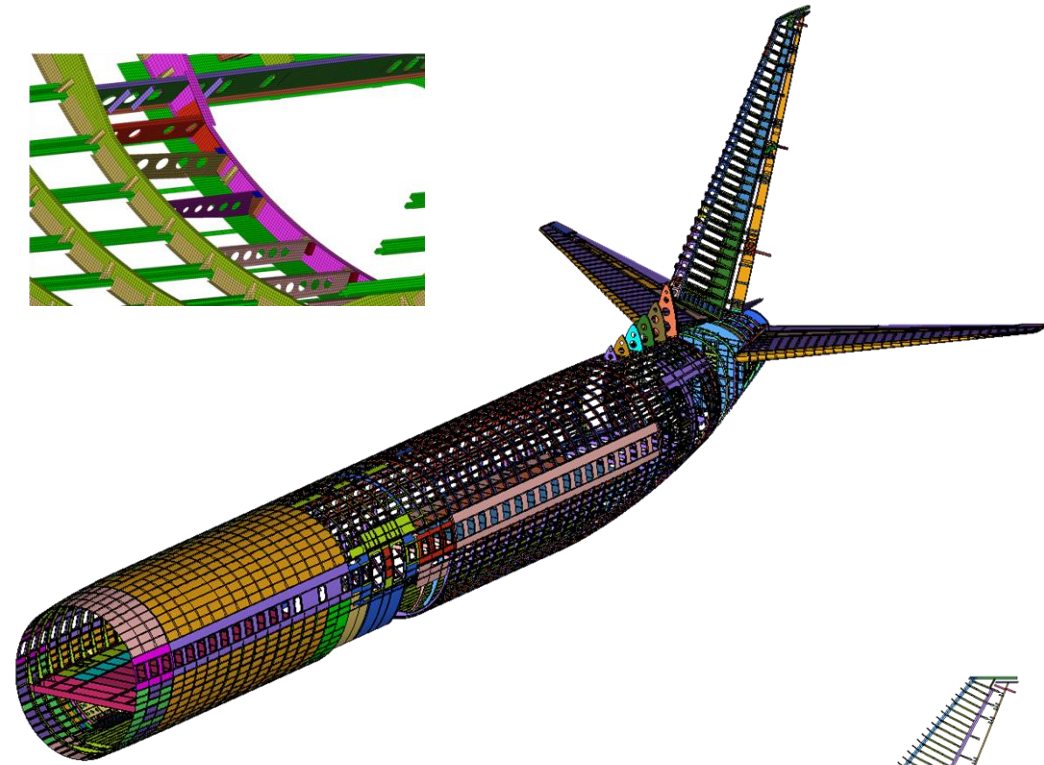
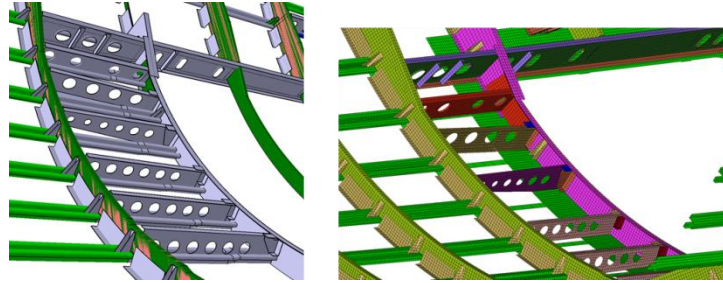
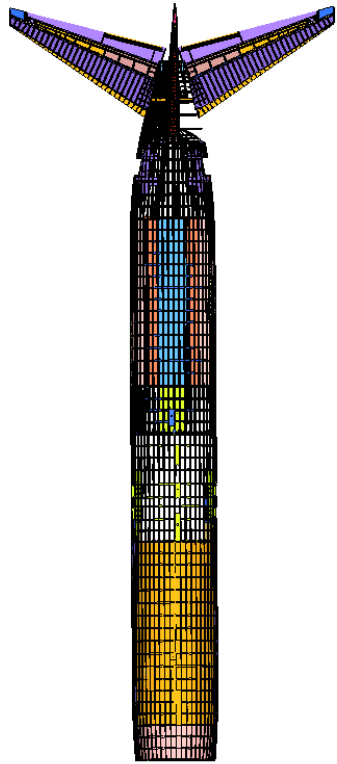
# SEC 43- Door Surround Structure



# SEC 47- Floor Structure



# Meshing Process Status

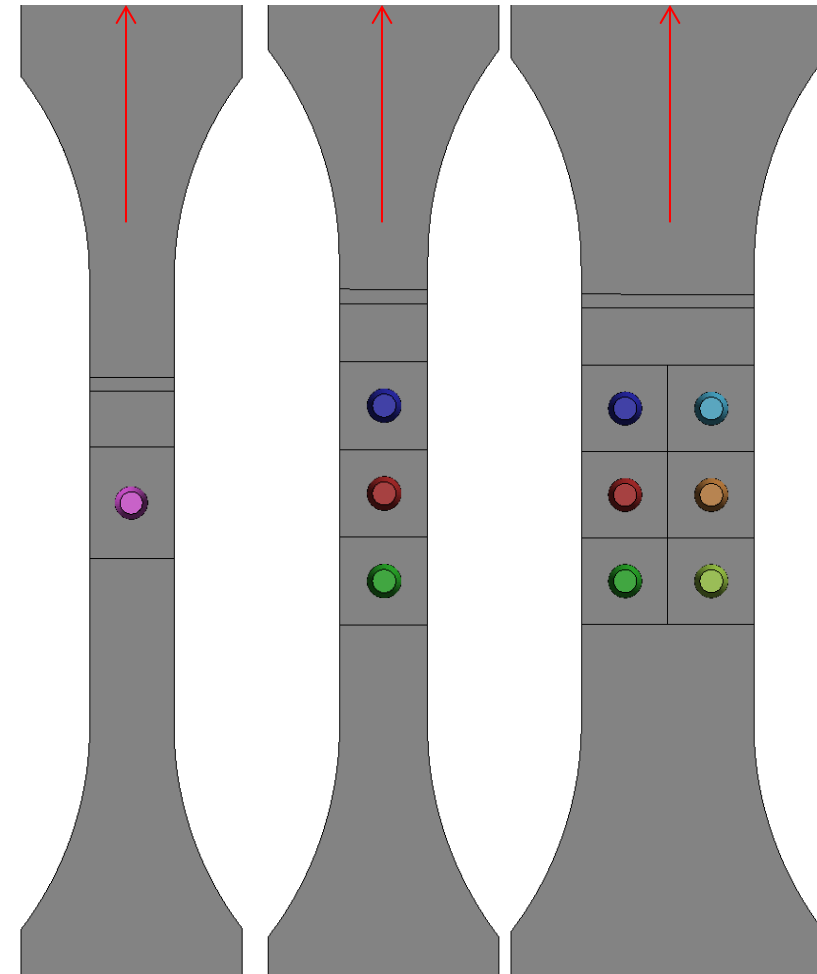


# High End Visualization Accident Data Methods



# Ongoing and Future Work

- Coupon Level WP 2.1: Complete. Report under FAA Review
- Round Robin WP2.2: Complete for Tension, data has been presented (ASC Paper 2014)
  - Future funding required for compression and shear
  - ASTM or SAE Standard should be developed
  - Report Ongoing – October 1st
- Joint WP4: Pending High Strain Rate Tests
  - Future Funding required for multiple joints
  - Future Funding required for composite joints
- Accident Reconstruction Phase IV: Ongoing
  - Present Preliminary results ASIDIC Conference 2015 November
  - Pending Accident Data Approval
- Future Work:
  - **Phase II WP 5. Section Level Experimental and Computational Best Practices:** The objective of this working package will be to summarize the numerical and experimental best practices developed in WP0 through WF in order to define a certification by analysis methodology that can be used the future by the aerospace industry.
  - **Phase V:** Design and evaluate an equivalent composite structure (Narrow Body Section)



Single

1 Col - 3 Row

2 Col - 3 Row

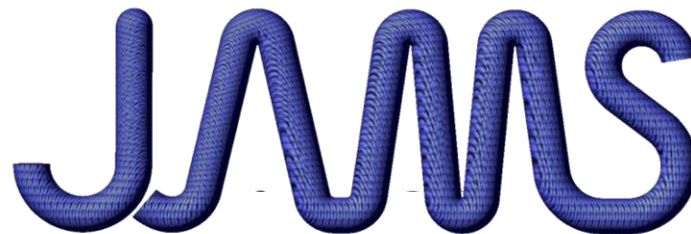


**2<sup>nd</sup> Aerospace Structural Impact Dynamics International Conference – Aeropolis, Seville, Spain, November 17-19<sup>th</sup> 2015**



End of Presentation.

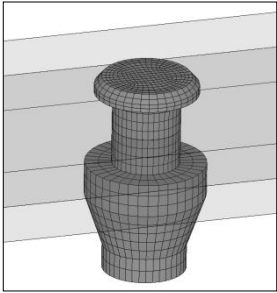
Thank you.



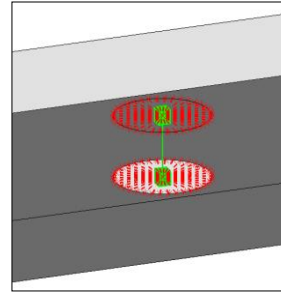
JOINT ADVANCED MATERIALS & STRUCTURES  
CENTER OF EXCELLENCE



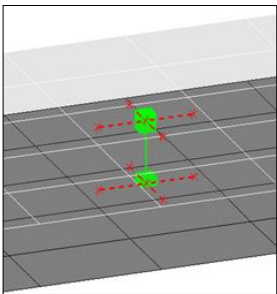
# Appendix - Bolt Modeling Techniques



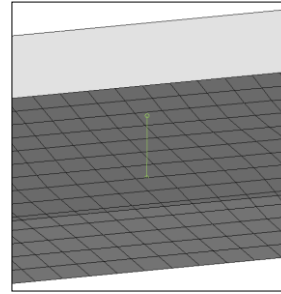
- 3D Solid Elements
- Most accurate FE representation
- Accurately captures bearing stresses and stress around fastener hole



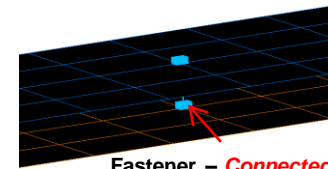
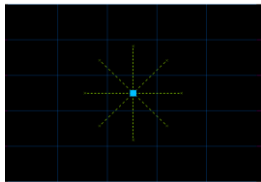
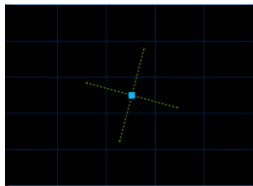
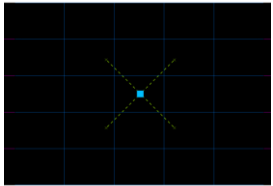
- Bolt shank modeled with beam element and connected to hole using rigid links
- Fastener hole is modeled, therefore meshing of large assemblies will be complicated
- Cannot capture bearing stress since forces are distributed circumferentially around the hole



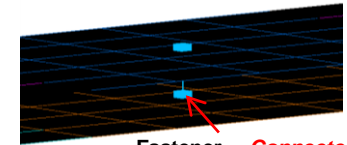
- Bolt shank modeled with beam element and rigid links used to distribute the forces
- Fastener hole not modeled
- Several variations as shown below are possible with this technique



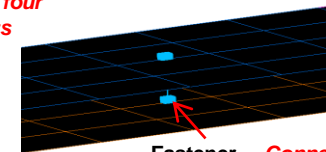
- Type 9 spotweld beam connection to represent the bolt
- Fastener hole not modeled
- Results vary due to both mesh size and location of weld relative to center of contact segment (LS DYNA Keyword Manual). Some variations shown below



Fastener – **Connected on edge of four elements**



Fastener – **Connected at Element Center**

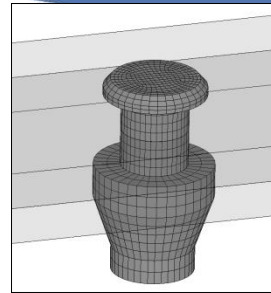
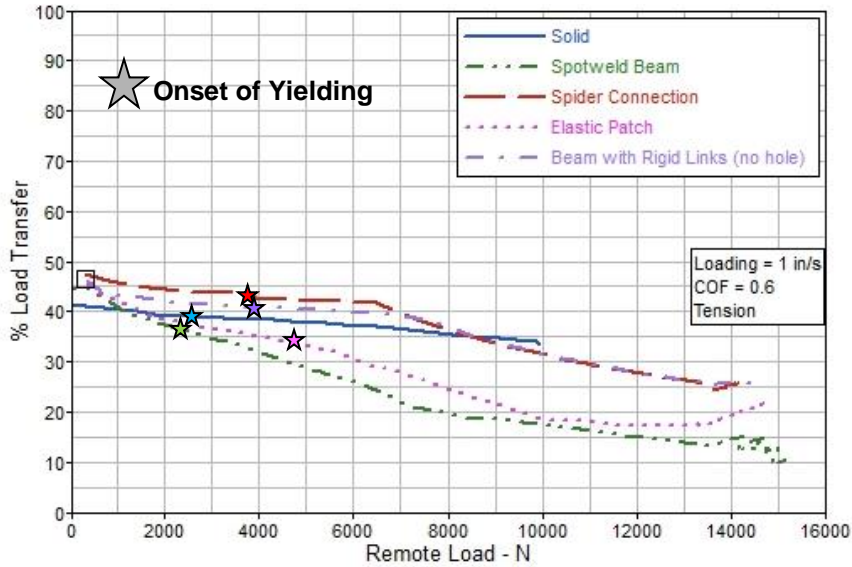


Fastener – **Connected between 2 elements on center of edge**

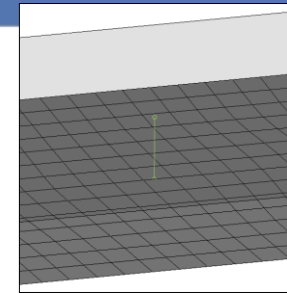


# Bolt Modeling Techniques

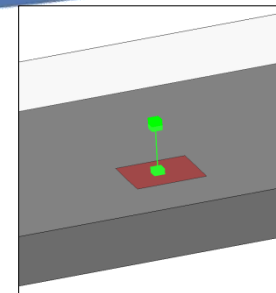
## % LOAD TRANSFER EVALUATION



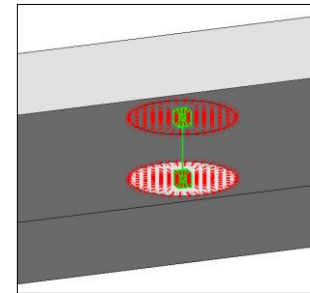
Solid



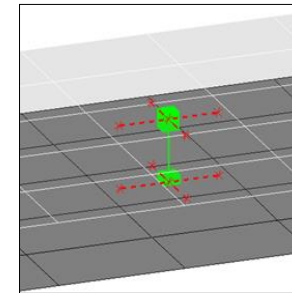
Spotweld Beam



Elastic Patch



Spider Connection



Beam with Rigid Links (no hole)

