Meeting The Needs of the Aerospace Industry: Accurate Simulation of Fabric Permeability

### **Advanced Composites Institute**

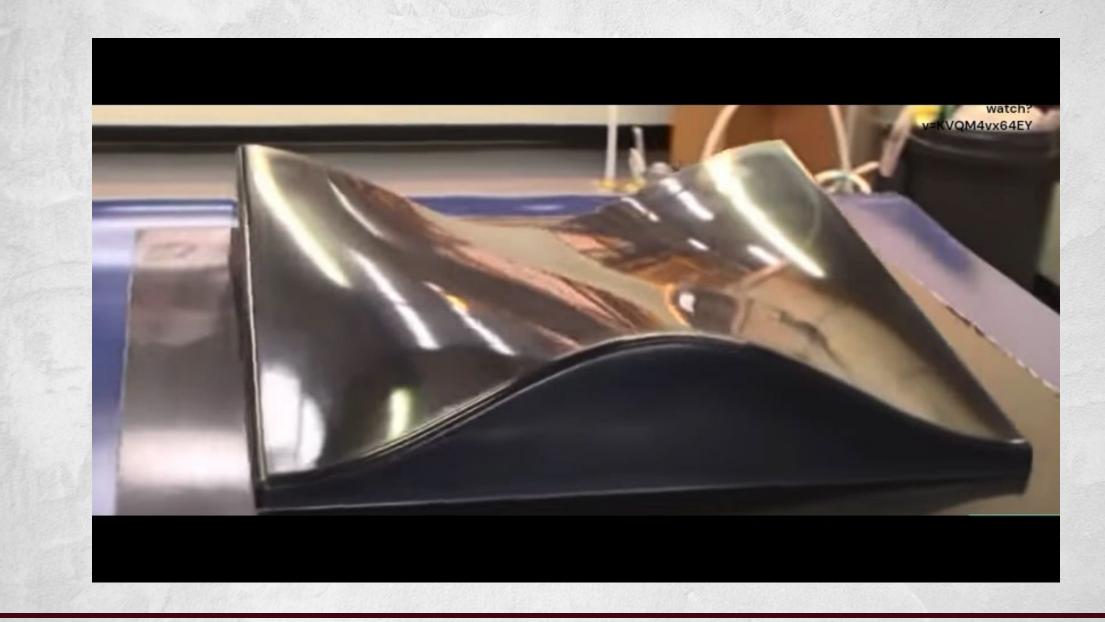
Home of the Marvin B. Dow Stitched Composites Development Center Mississippi Advanced Composites (MAC) Training Center

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FAA Technical Monitor: Dave Stanley / FAA Sponsors: Cindy Ashforth, Larry Ilcewicz









# How repeatable do you think these infusions would be?



What if we simulated the flow front? Would the simulation match these videos? What if these parts were larger? What if the part geometries were more complicated?



### The market identified simulation as a problem.



- Use of simulation for resin infusion process design is uncommon
  - Trial and Error
  - Operator experience
- Ultimate goals of infusion simulation
  - Reduce waste and cost
  - Reduce necessary operator knowledge



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How does one model an infusion process with commercially available software?

- 1. Resin flow
- 2. Thermal exchange between part and mold
- 3. Chemical reaction of resin



Draping and Thermoforming

Resin Transfer Molding (RTM), High-Pressure RTM and Compression RTM

Resin Infusion and its variants

Sheet Molding Compound (SMC)

Curing and Crystallization

Geometrical Distortions induced by the manufacturing process



#### Modeling an RTM process: Flow

Darcy's Law  
$$\vec{V} = -\frac{K}{\mu} \overrightarrow{\nabla P}$$

 $\vec{V}$  = Darcy's velocity K = permeability tensor  $\mu$  = viscosity of resin P = pressure

"simplistic"

Unified Darcy's Equation  $div\left(\frac{[K]}{\mu}\langle \nabla P \rangle\right) = \frac{d\varepsilon}{dt}$ 

 $\varepsilon$  is deformation of the fiber bed

General form of mass conservation for deformable media (i.e. fabric).

"more advanced"

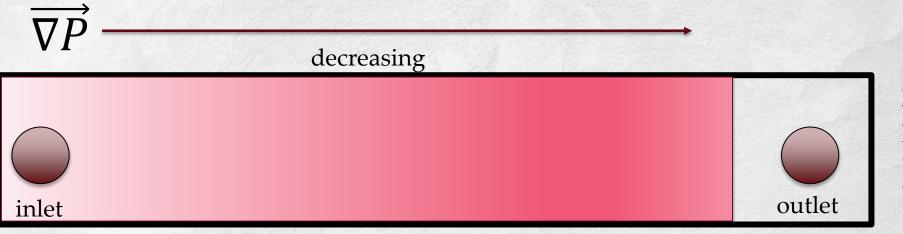


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#### Modeling an RTM process: Compaction forces

• Vacuum bagging (VARTM)



Rapid pressure drop can cause voids

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- Vacuum (LP-RTM)
- Press (RTM, HP-RTM)



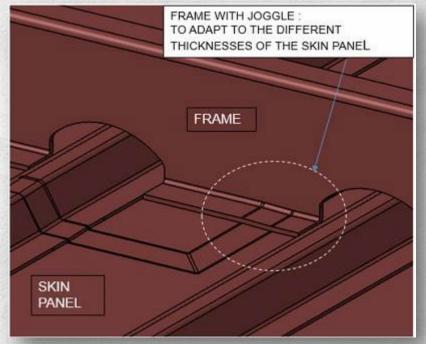
#### Key Factors Affecting Permeability: FVF and nesting

### Various infusion processes may have different FVF and gradients thereof

Table 7 Measured fiber volume fractions for each manuf. method.75

Process	Fiber Volume Percentage		
VARTM	-		
FVF Inlet	47%		
FVF Outlet	49%		
SCRIMP	-		
FVF Inlet	47.7%		
FVF Outlet	47.9%		
DBVI	-		
FVF Inlet	45.4%		
FVF Outlet	47.5%		
VAP	-		
FVF Inlet	50.2%		
FVF Outlet	50.5%		
CAPRI	-		
FVF Inlet	51.8%		
FVF Outlet	52.2%		
PI	-		
FVF Inlet	39.5%		
FVF Outlet	48.7%		

Complex shapes may perform differently for various infusion processes



#### 32 layers pad up; 24 layers skin; $\Omega$ stiffener 16 layers

Design and manufacture of a reinforced fuselage structure through automatic laying-up and in-situ consolidation with co-consolidation of skin and stringers using thermoplastic composite materials, Heliyon, Volume 9, Issue 1, 2023,

#### Advanced Composites Institute

An objective comparison of common vacuum assisted resin infusion processes. *Compos. Part A Appl. Sci. Manuf.* **125**, 105528 (2019).



#### Key Factors Affecting Permeability: Laminate Thickness

#### Laminate Thickness

- Introduces complexity when in-plane flow is considered
  - Alternate flow pathways into lowpermeability layers
- Accurate modeling of laminates required for simulation
  - Laminates with flow media, release fabric, etc.

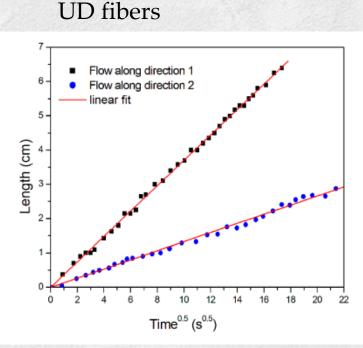




#### Key Factors Affecting Permeability: The fabric itself

#### Anisotropy

- UD fibers High anisotropy
  - NCF, tape, etc.
  - Can cause bubbles
- Woven Lower anisotropy



Direction	Permeability
K1 (um <sup>2</sup> )	2.81
K2 (um <sup>2</sup> )	0.38
K3 (um <sup>2</sup> )	0.043

Materials 2020,13, 4800

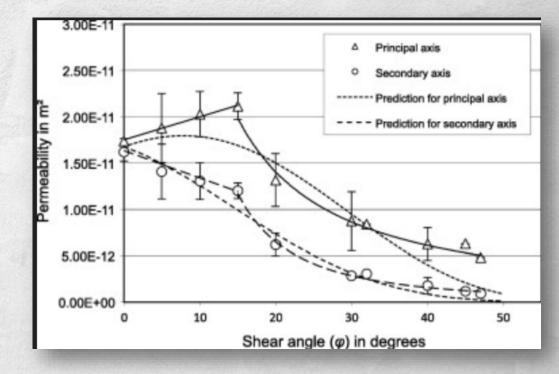


#### Key Factors Affecting Permeability: Fabric Shear

#### **Fabric Shear**

- Fiber tows are not perpendicular
- can be sheared over the entirety of the ply, or locally around changes in geometry
- Permeability change
  - Volume fraction changes with shear angle
  - Fiber tow reorientation can align flow directional components

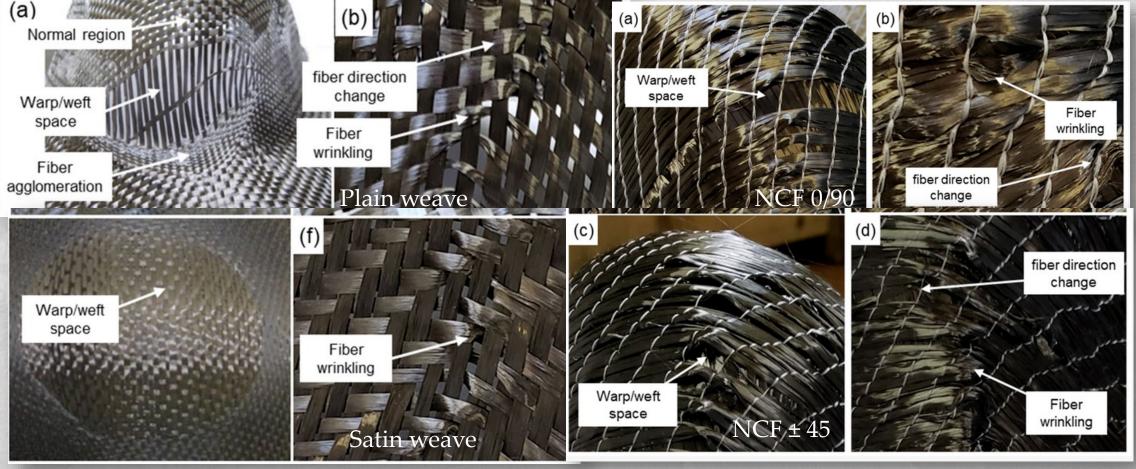
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Composites Part B: Engineering, Volume 65, 2014, Pages 158-163,

#### Key Factors Affecting Permeability: Fabric Shear



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#### Key Factors Affecting Permeability: Capillary Forces

#### **Capillary Action**

- <u>Controversial</u>
- Senoguz Surface tension measurements<sup>1</sup>
  - Capillary pressure too small compared to inlet pressure and can be ignored
- Amico and Lekakou Experimental studies<sup>2</sup>
  - Capillary forces cannot be ignored at low infusion pressures (i.e. VARTM)
    - Can be as high as 5.4 PSI<sup>3</sup>

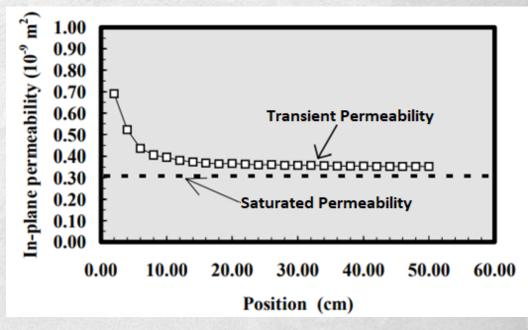
Journal of Composite Materials, vol. 35, no. 14/2001
 Composites Science and Technology, vol.61(13), pp.1945-1959
 Polymer Composites, June 1997, vol. 12, no. 3

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#### Key Factors Affecting Permeability: Transient vs Saturated Flow

#### Saturated vs. Transient Flow

- Saturated flow steady-state, occurs once the fabric has been fully wetted by the permeating fluid
- Transient flow occurs between wet and dry regions of the fabric



Proceedings of ICCM-11, Gold Coast, Australia, 14th-18th July 1997



### Methodology for Permeability Measurement

- Various methods for measuring permeability
  - 1-dimensional flow tests
    - Simple calculation and experimental design, saturated/unsaturated measurement
    - Race tracking along fabric edges, multiple tests needed for full characterization
  - Radial injection
    - No race tracking effects, simultaneous warp/weft measurements
    - More difficult setup, only unsaturated measurement
- Flow front tracking
  - Optical Well-defined procedures, cheap equipment
  - Capacitive sensors Test apparatus does not need to be optically clear, more expensive



### Permeability Measurement – Test Setup

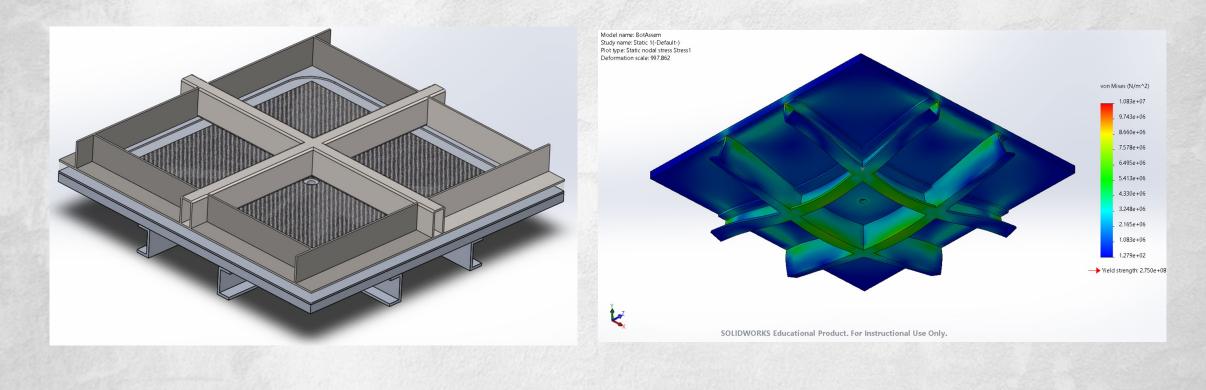
#### **In-Plane Test**

- Biaxial non-crimp fabric is cut to 10" squares on CNC ply cutter table
- 1/4" diameter hole punched in the center of each ply



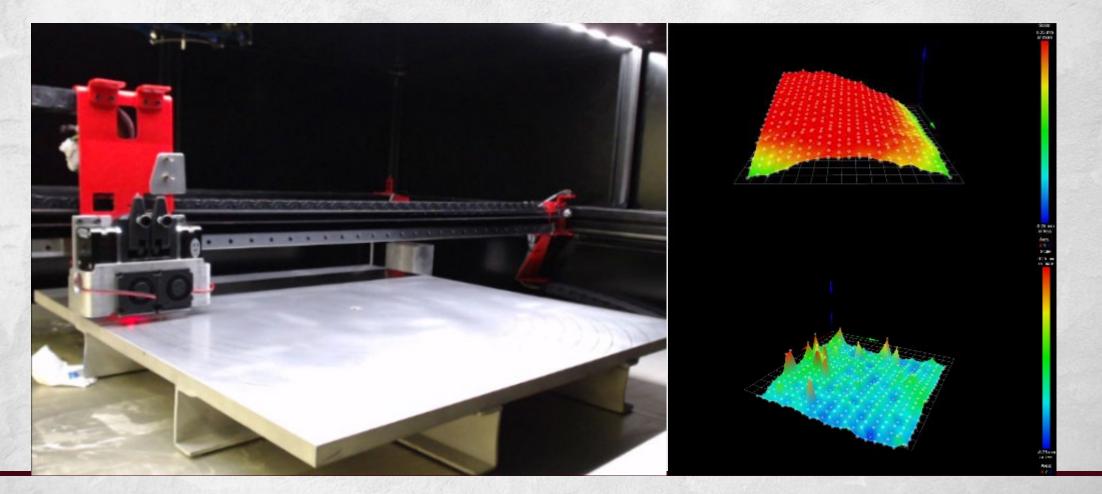


#### Permeability Measurement Test Apparatus Design V1



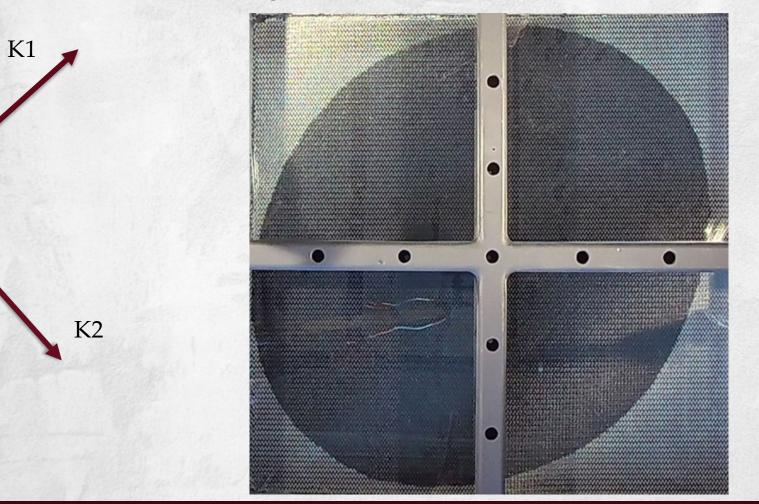


### Bed leveling to measure flatness





### Permeability Measurement – Test Results





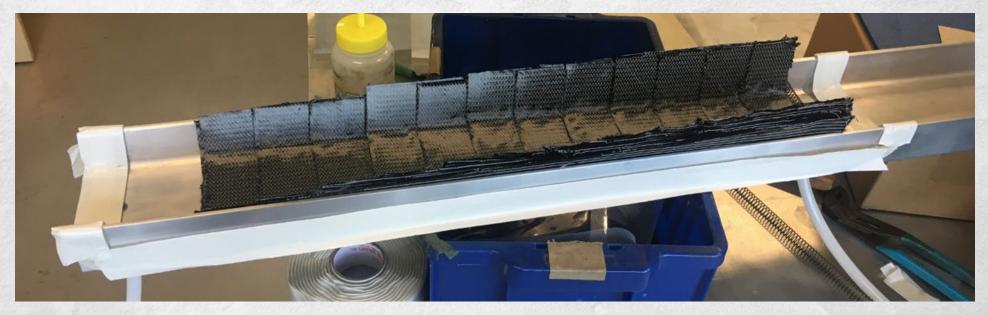
### PAM-RTM Simulation Permeability Values at 52% FVF

	Fiber Permeability (m <sup>2</sup> )	EasyPerm Fiber Permeability (m <sup>2</sup> )	Flow Media Permeability (m <sup>2</sup> )	Release Ply Permeability (m <sup>2</sup> )	
In-Plane (Warp)	2.76E-11	1.3E-11	2.50E-10	2.50E-12	
In-Plane (Weft)	3.42E-11	1.2E-11	2.50E-10	2.50E-12	
Through-Thickness	1.85E-12	1.8E-12	1.00E-09	2.00E-11	
	Measured		Assumed valu		
		Assumed values are unfavorable, but realis			



### PAM-RTM Simulation – Comparison Case

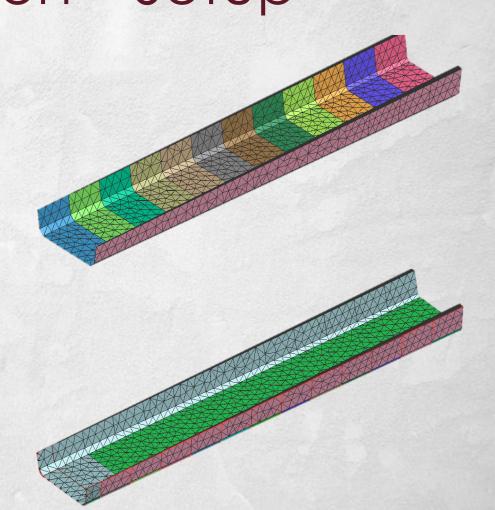
- A test case infusion was set up for comparison to the simulation result
- Infusion performed with 14.5psi vacuum at outlet, with 3psi vacuum at inlet





# PAM-RTM Simulation – Setup

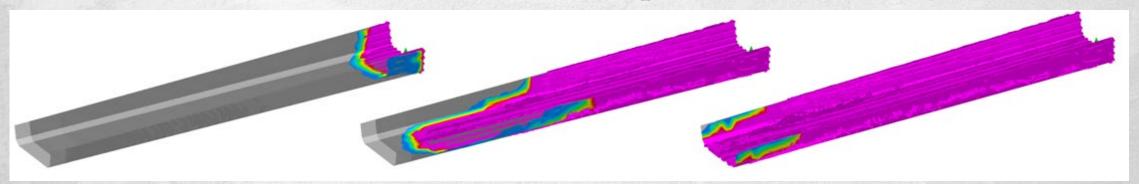
- A modified C-Channel
  - Tapered thickness (16→5 plies)
    Tapered depth
- 3D tetrahedral elements
- Flow media and a Teflon release ply on top of the laminate





# PAM-RTM Simulation – Results

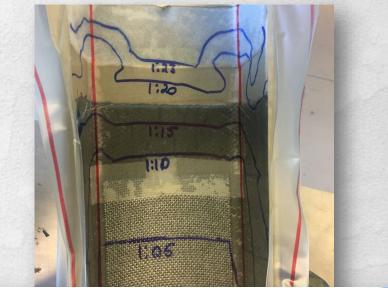
- The simulation ran for ~3 hours and proceeded through 3,394 calculation steps
- Simulated filling time: 28.9 min
- Flow media was fully filled: 20.7 min
- Resin reached the end of the fiber preform: 22.1 min





### PAM-RTM Simulation – Comparison Case

- The test case stopped after 23 minutes
  - Complete filling of the carbon preform
  - Only small wet spots on 'resin brake' release ply area
  - Simulation: 28.9 min
- Flow media filled: 5-10 min
  - Simulation: 20.7 min
- Resin spread up the sides of the channel after flow media is filled, higher at end with inlet

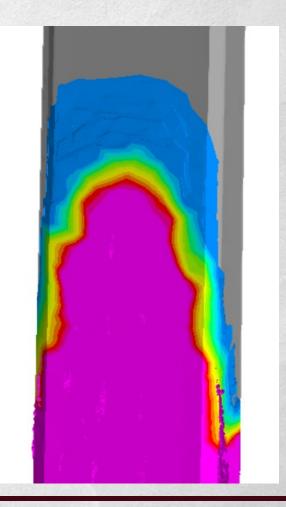






# PAM-RTM Simulation – Results

- Using 3D elements allows flow front visualization that isn't normally seen
- Total filling time 25.7% error
- Simulation did not predict the flow front interaction between areas with and without flow media
- It is likely that the assumptions made about non-carbon laminate material permeability significantly affected the result





# Permeability Measurement: Requirements

- Should conform to ISO draft: Experimental Characterization of In-Plane Permeability of Fibrous Reinforcements for Liquid Composite Moulding
  - Test fluid injected above atmospheric pressure (Maximum 0.3MPa)
  - Specimen thickness control
    - Test apparatus stiffness (maximum 2% cavity height deflection under pressure)
    - Repeatable spacing between two halves of test apparatus
    - Measurement procedures to verify cavity uniformity
  - Fluid pressure transducer (0.5% FS accuracy, FS < 2MPa)
  - Specimen edge length 30 times the injection port radius



# Permeability rig V2

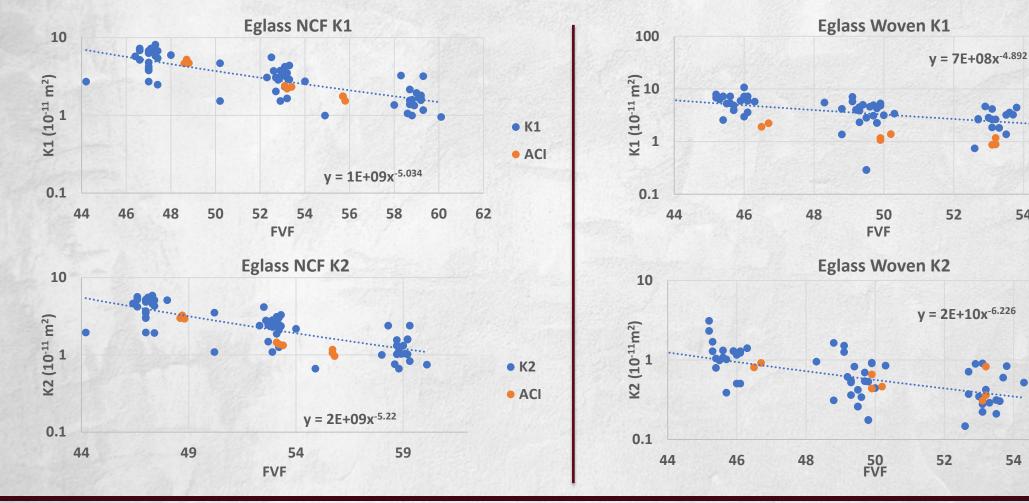








### How do we compare to benchmark?



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• K1

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• K2

ACI

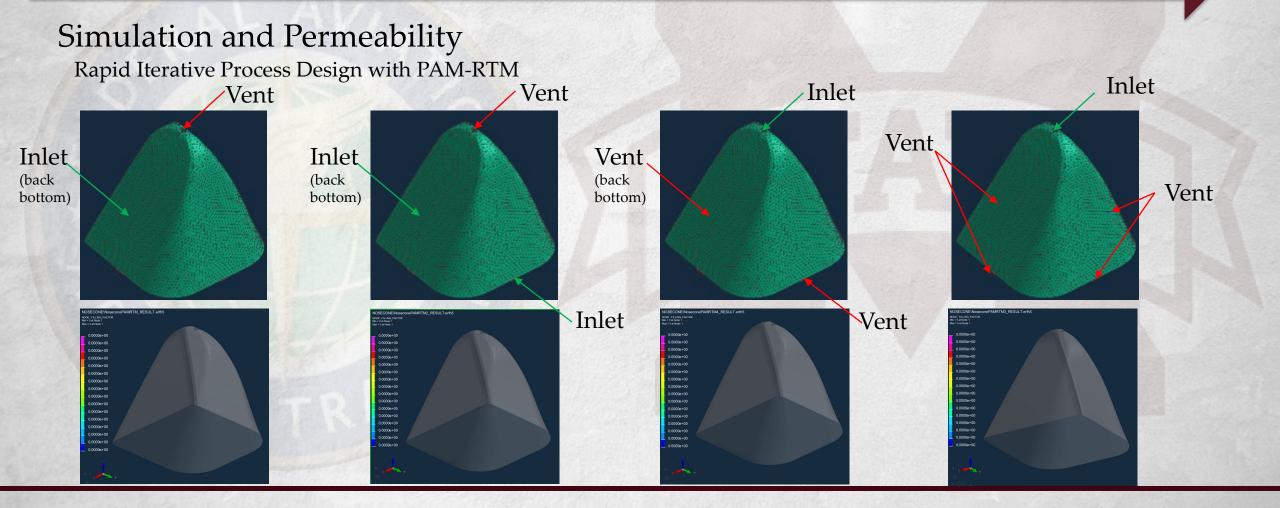
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### Technology Readiness for Stitched Resin Infusion

Phase II: Microcracking, NCAMP equiv., simulation, & preliminary testing for demonstrator





# Hill Helicopters





https://www.hillhelicopters.com/

https://www.linkedin.com/feed/update/urn:li:activity:7043914894076772352/



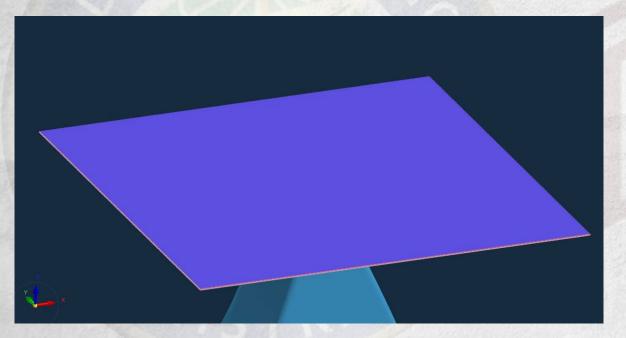
# Questions



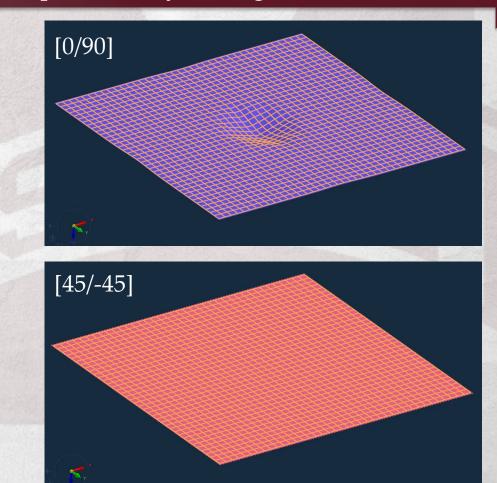
### Technology Readiness for Stitched Resin Infusion

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<u>Simulation and Permeability</u> Multi-Layer Draping Simulation with PAM-FORM



Simulation is more complex for a single-sided hard tool



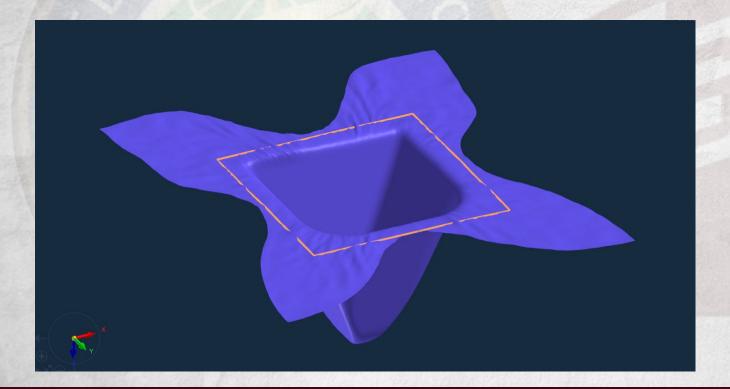


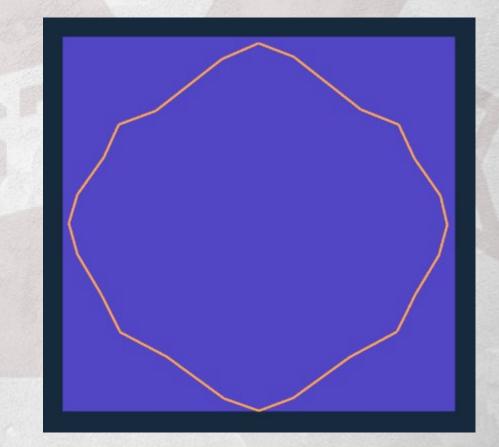
### Technology Readiness for Stitched Resin Infusion

Phase II: Microcacking, NCAMP equiv., simulation, & preliminary testing for demonstrator

#### Simulation and Permeability

Efficient Ply Design for Reduced Waste







# Questions?



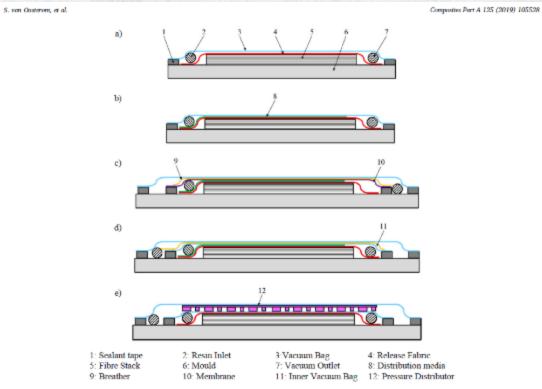


Fig. 1. Schematic description of the process variants; (a) VARTM, (b) SCRIMP and CAPRI, (c) VAP, (d) DBVI, and (e) PL (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

