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Impact Damage Formation on Composite Aircraft Structures

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JAMS 2019 Technical Review

May 22-23, 2019

Charlotte, NC



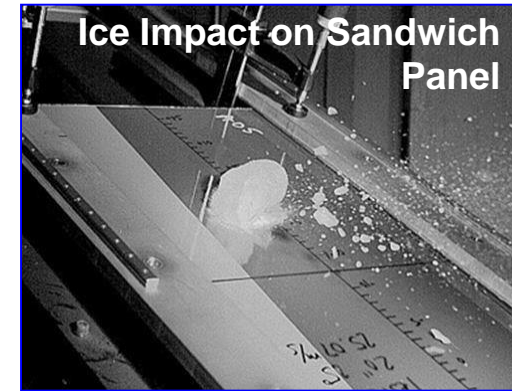
Impact Damage Formation on Composite Aircraft Structures

- **Principal Investigators & Researchers**
 - PI: Prof. Hyonny Kim, Professor, UC San Diego
 - Graduate Students
 - PhD:
 - HEWABI: Moonhee Nam, Chaiane Wiggers de Souza
 - Sandwich Core Crush: Konstantinos Anagnostopoulos
 - MS: none
- **FAA Technical Monitor**
 - Lynn Pham
- **Other FAA Personnel Involved**
 - Larry Ilcewicz , Ahmet Oztekin
- **Industry Participation**
 - Boeing, Bombardier, UAL, Delta, DuPont, JC Halpin Consulting

Impact Damage Formation on Composite Aircraft Structures

• Motivation and Key Issues

- impacts are ongoing and major source of composite damage
- High Energy Wide Area Blunt Impact (HEWABI) damage of main interest
 - involves large contact area
 - internal damage can exist with **low/no exterior visibility**



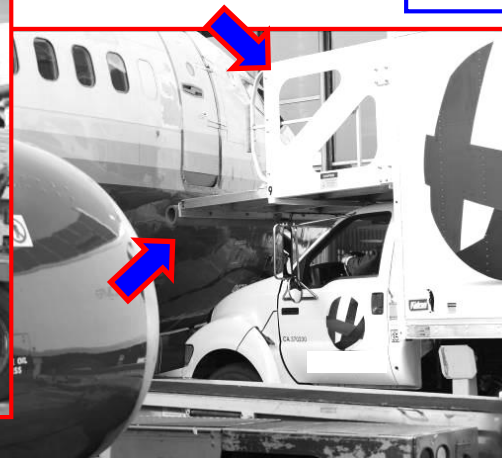
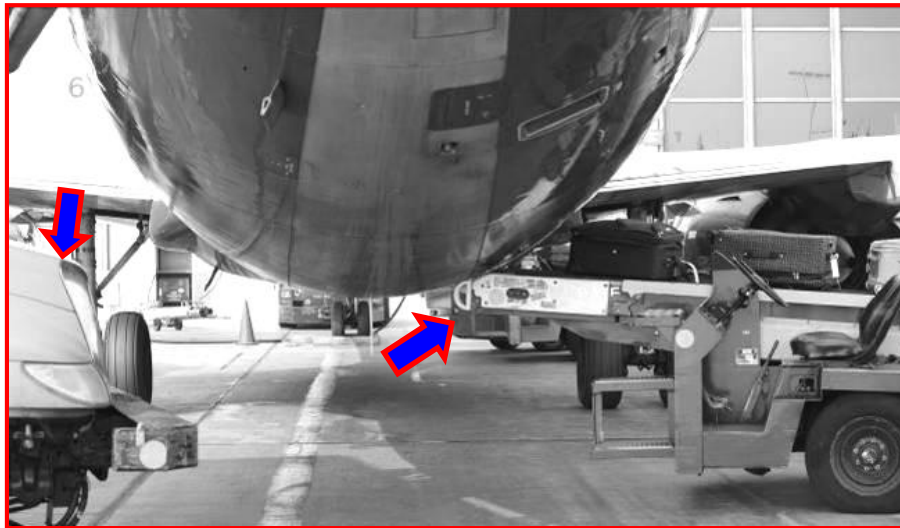
• Sources of Interest:

- ground service equipment (GSE) with rubber bumpers
- railings, blunt/round corners, FOD of unknown geometry
- hail ice, bird



Sandwich Blunt Impact

- core crush with low/non-visible dent
- low velocity: GSE, tools
- high velocity: ice, bird



Ground Vehicles & Service Equipment

- side & lower facing surfaces
- high mass, low velocity

Overall Project Objectives

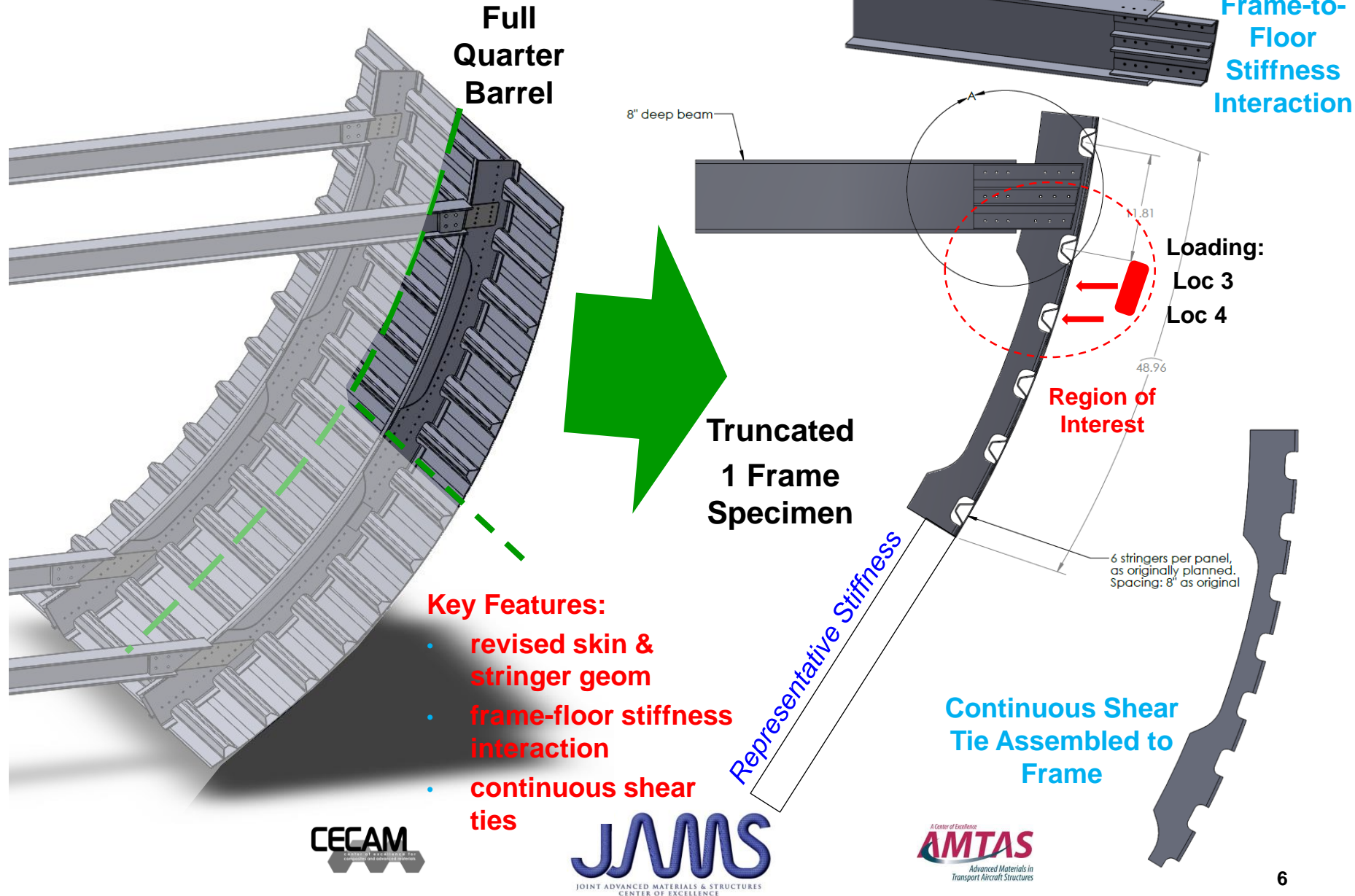
- **Understand impact damage formation; particularly for blunt sources and visual detectability**
 - Identify key phenomena
 - Understand controlling parameters
 - special attention to internal vs. external damage formation vs. bluntness/contact-area size
- **Develop testing methodology: full vs sub-structure and BC considerations**
- **Establish experimental database for analysis methods validation**
- **Develop progressive damage analysis methodologies predicting blunt impact**

Outline

- Ground Service Equipment (GSE)
High Energy Wide Area Blunt Impact
(HEWABI)
- Impact Damage to Sandwich Panels
& Core Crush Mechanics
- Summary, Benefits to Aviation, and
Future Work

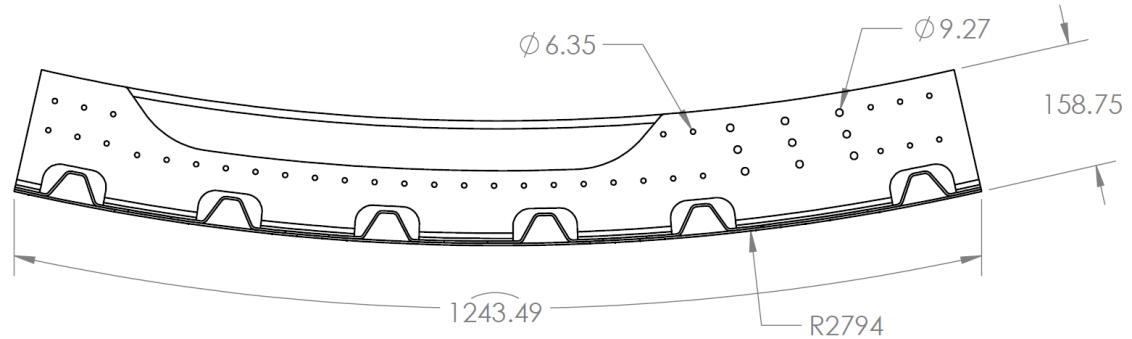
2nd Generation Specimen Blunt Impact Tests

Focus: Impact & Failure Near Floor Joint



Large Specimen Design

- Qty: 4 panels
- Each Panel:
 - 6 co-cured stringers
 - 1 frame with continuous shear tie
 - floor joint compliance BC



Dimensions in mm

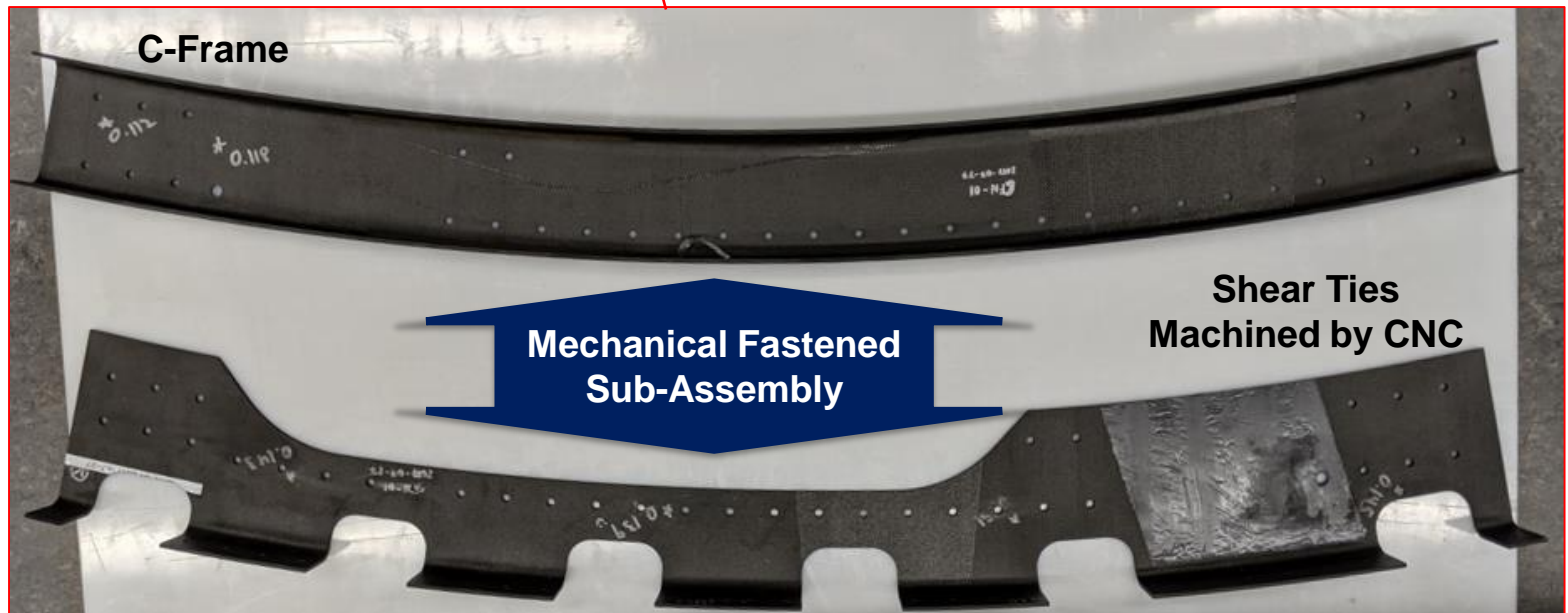
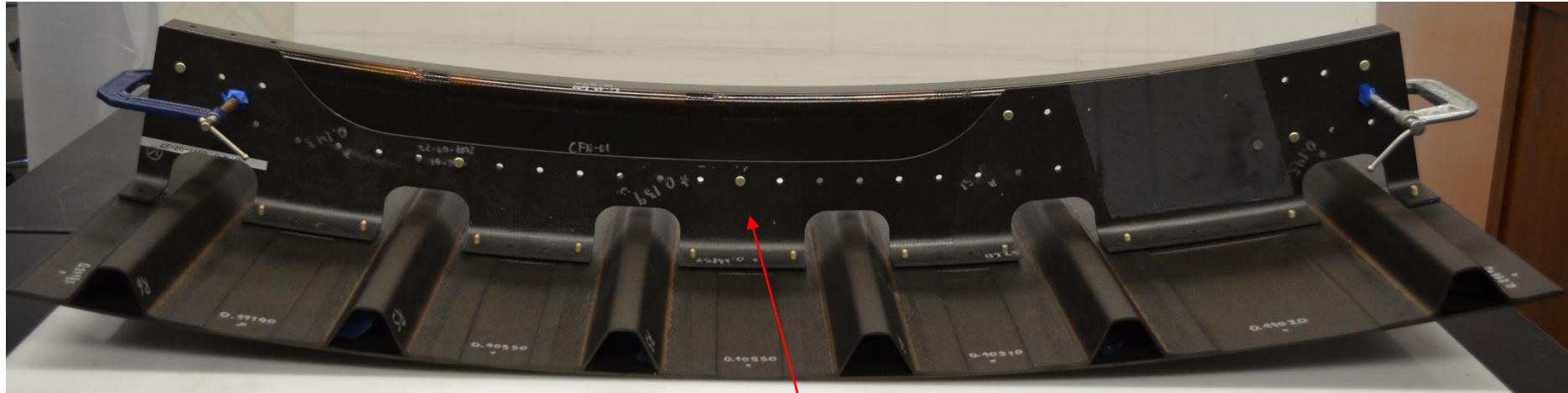
203 mm deep Alum I-beam represents passenger floor



Bracket representing compliance of floor-frame interaction

Part	Layup	THK (mm)
Skin	$[0w/0/45/90/-45/0/90]_s$	2.79
Stringer	$[0w/0/45/90/-45/0/90]_s$	2.79
C-Frame (all woven)	$[45/0/-45/45/0/-45]_s$ (web) $[45/0/0/-45/45/0/0/-45]_s$ (flange)	2.64 3.53
Shear tie (all woven)	$[45/0/-45/0/45/0/-45/0]_s$	3.53

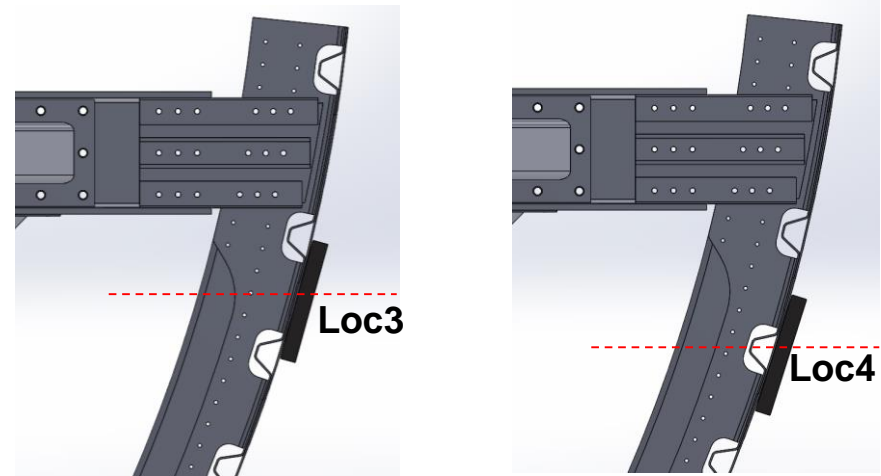
Fuselage Panel Assembly



Test Configuration

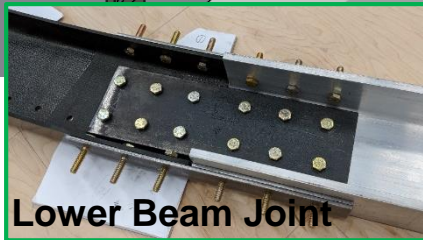
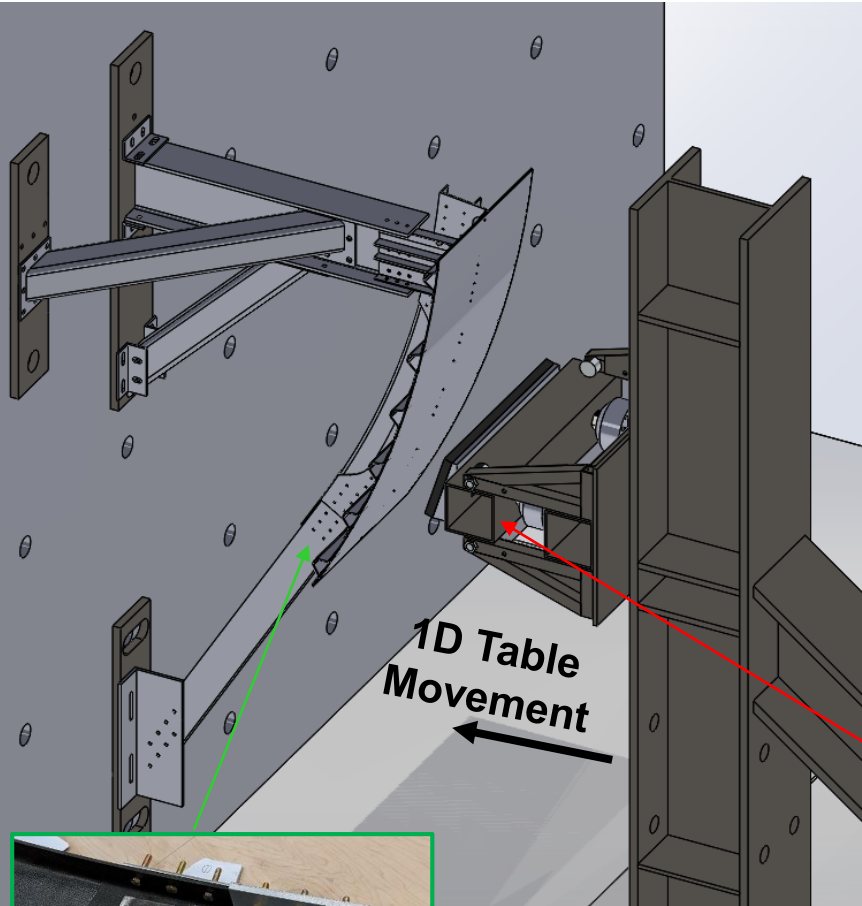
- Quasi-static loading only - table system tests found dynamic overshoot uncontrollable due to high inertia

Test Loading Locations: Loc3 & Loc4



Four Specimens: Quasi-static, Inspect & Reload

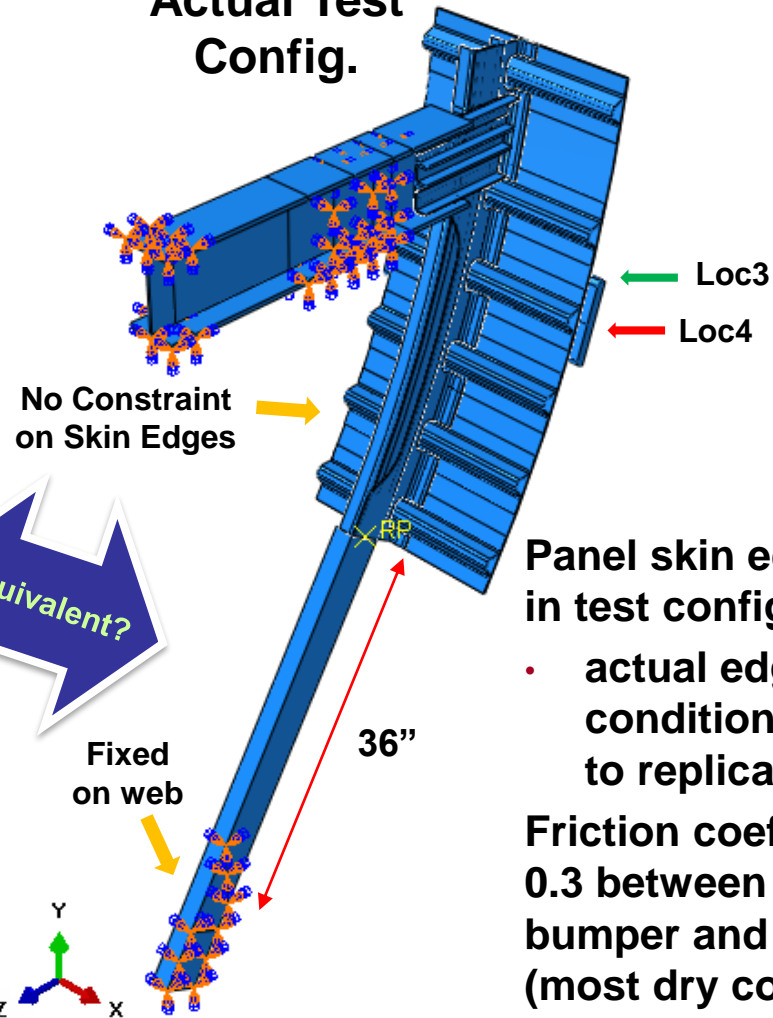
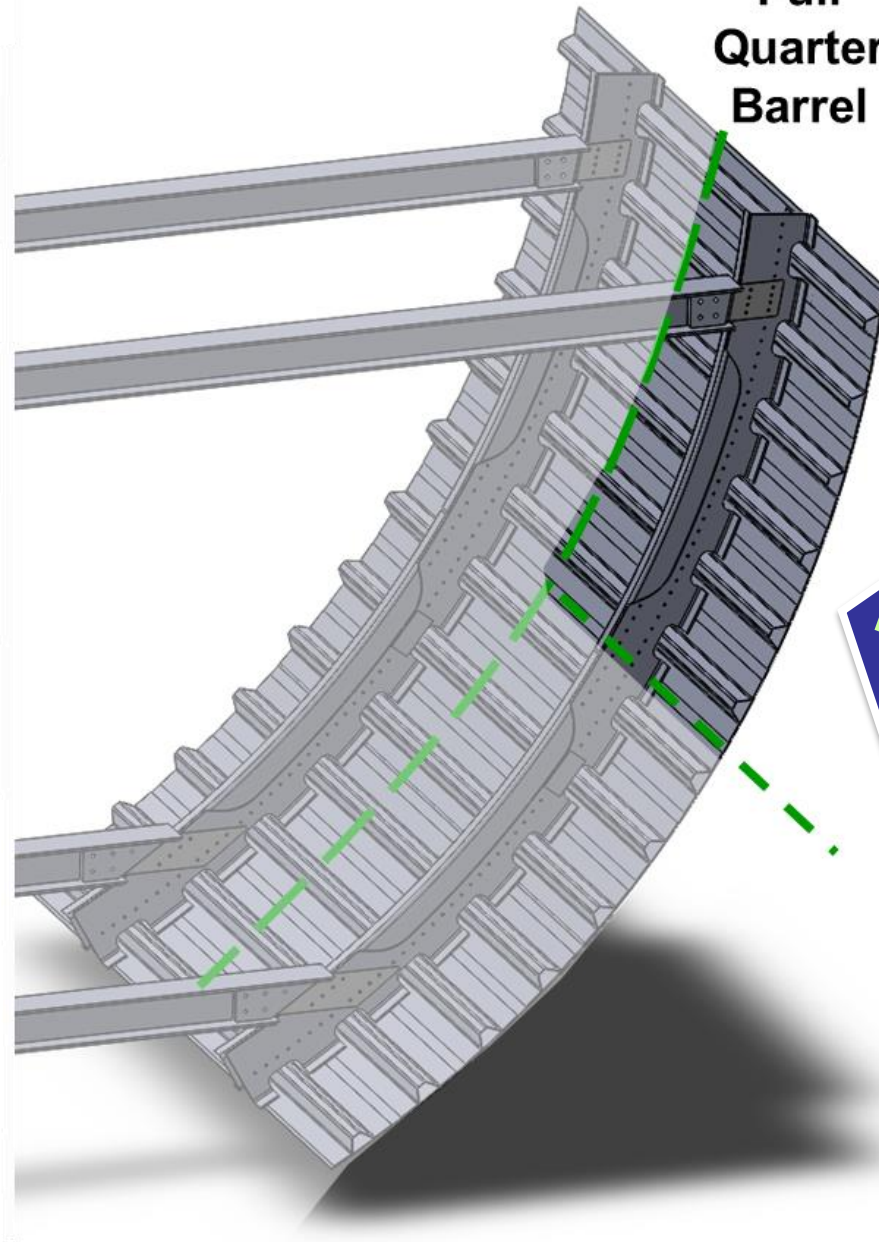
Specimen	Load	Test Level
1	Loc3	First significant damage mode
2	Loc3	Major damage - frame
3	Loc4	First significant damage mode
4	Loc4	Major damage - frame



Modeling: Verify BCs Represent Quarter Barrel

Full
Quarter
Barrel

Truncated:
Actual Test
Config.



Loc3

Loc4

No Constraint
on Skin Edges

Equivalent?

Fixed
on web

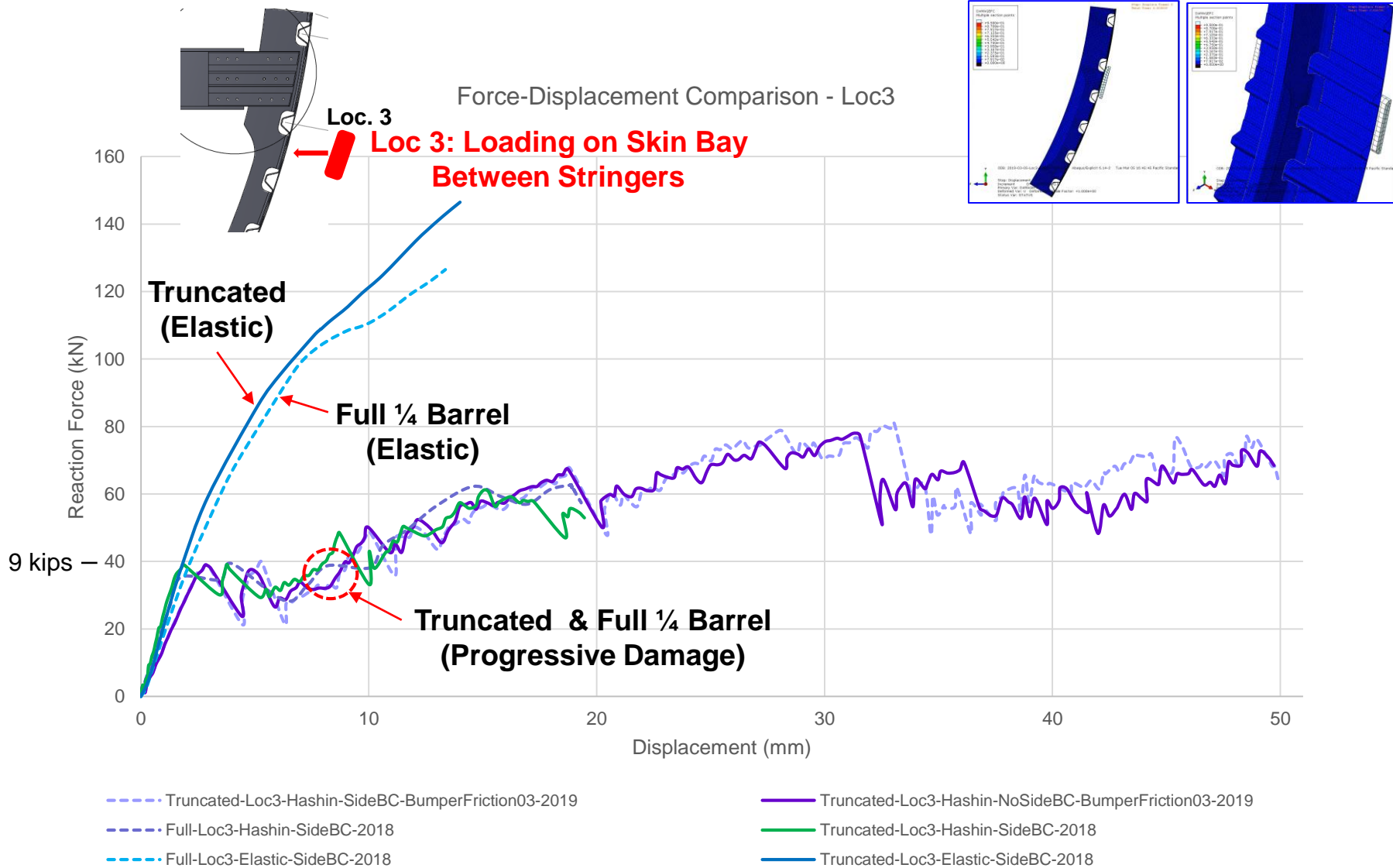
36"

Panel skin edges free
in test configuration

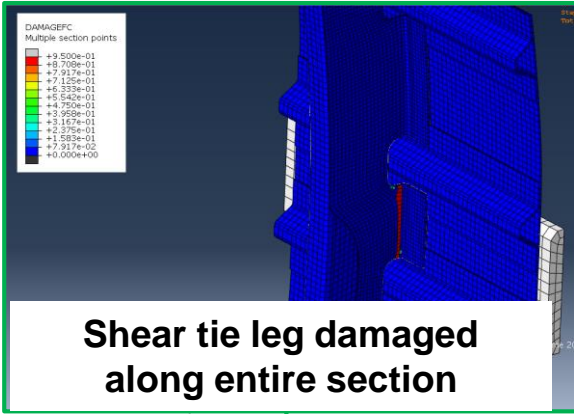
- actual edge condition difficult to replicate

Friction coefficient
0.3 between rubber
bumper and skin
(most dry contact
0.3-0.6)

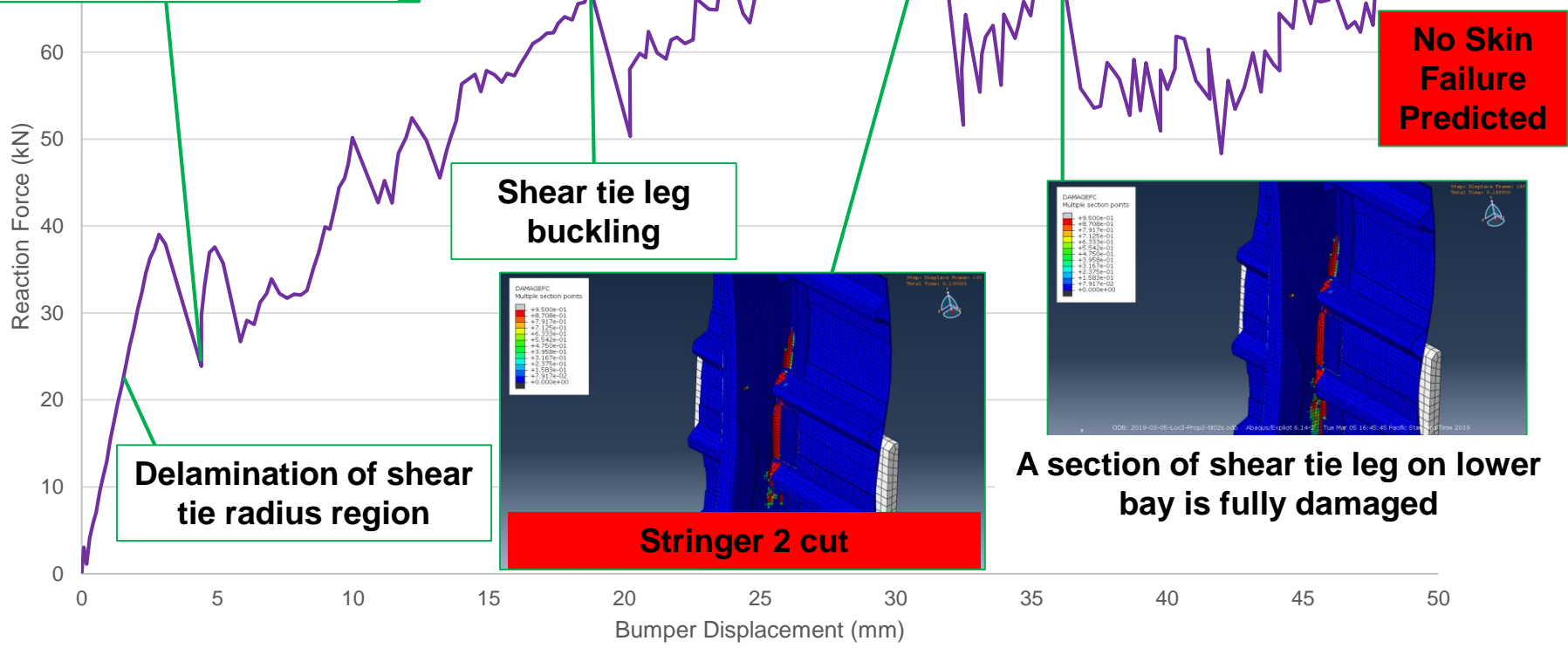
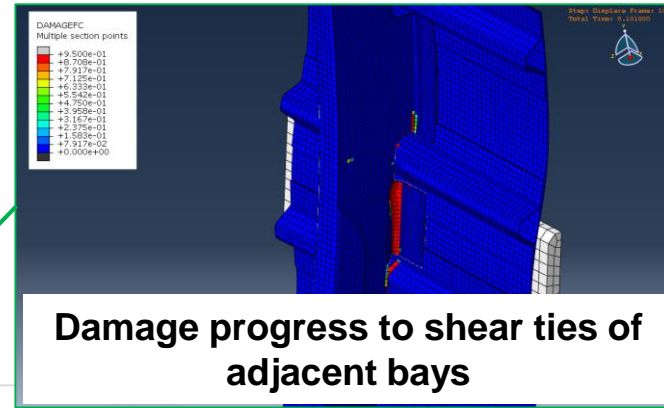
Loading Location 3 Response Comparison



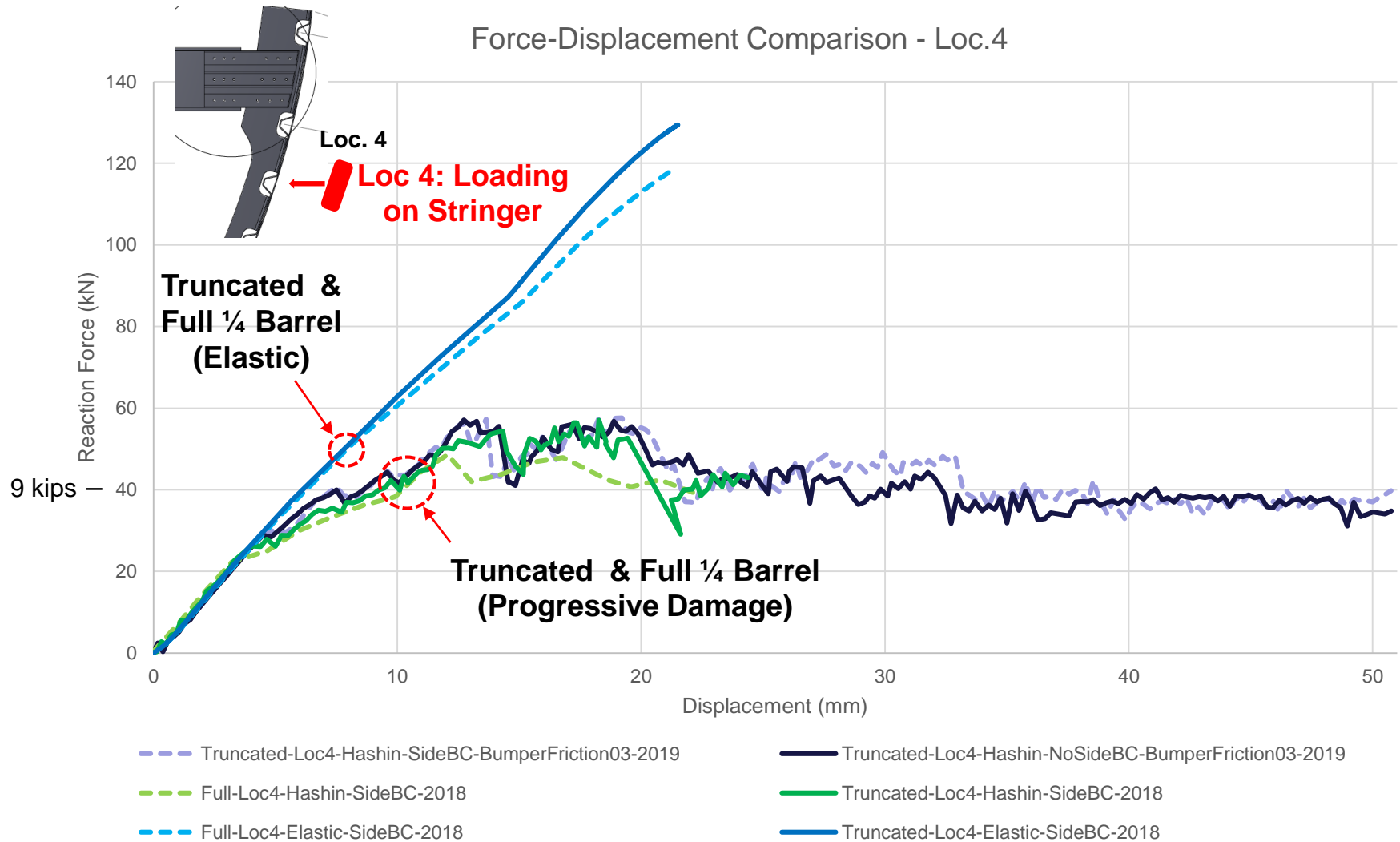
Failure Sequence: Location 3



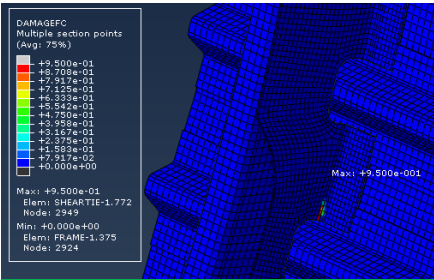
Force-Displacement - Loc3



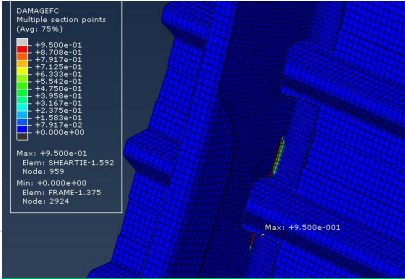
Loading Location 4 Response Comparison



Failure Sequence: Location 4

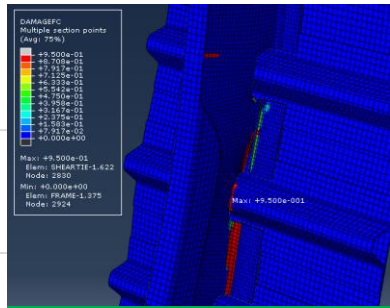


Shear Tie radius damage starts near mouse hole upper side at Loc4.

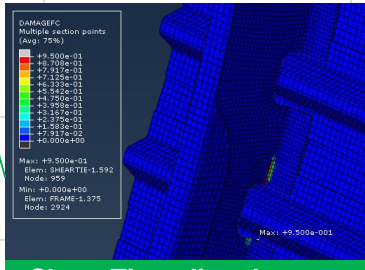
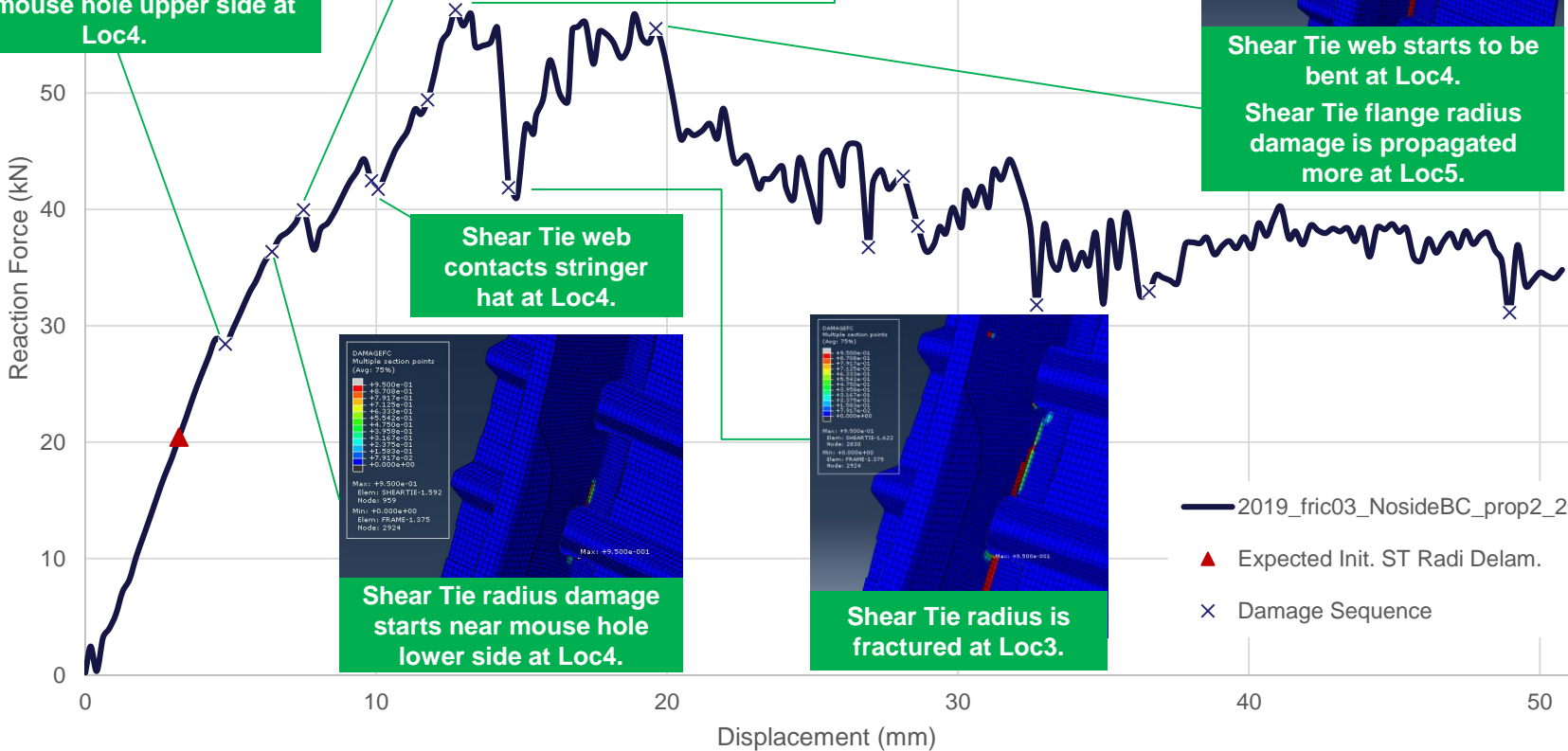


Shear Tie radius damage is propagating from mouse hole at Loc4.

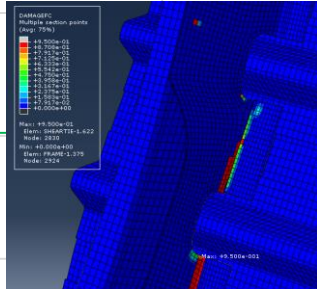
Stringer hat damage starts at Loc4.



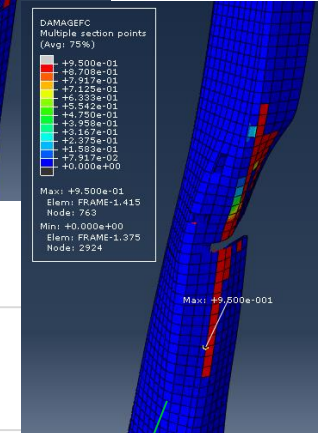
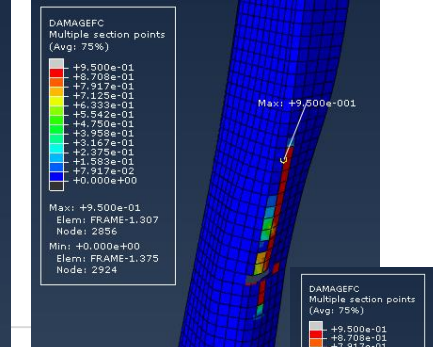
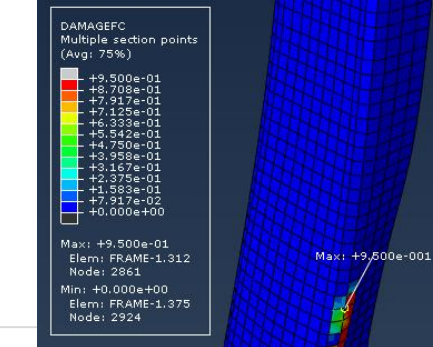
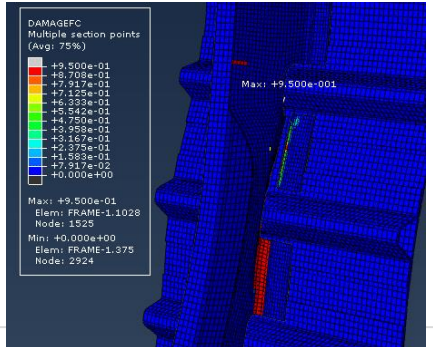
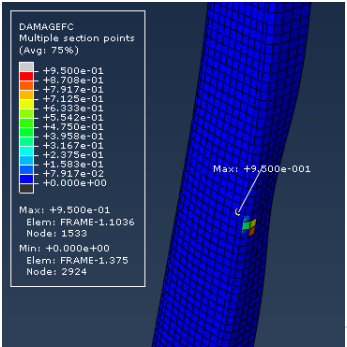
Shear Tie web starts to be bent at Loc4.
Shear Tie flange radius damage is propagated more at Loc5.



Shear Tie radius damage starts near mouse hole lower side at Loc4.



Shear Tie radius is fractured at Loc3.



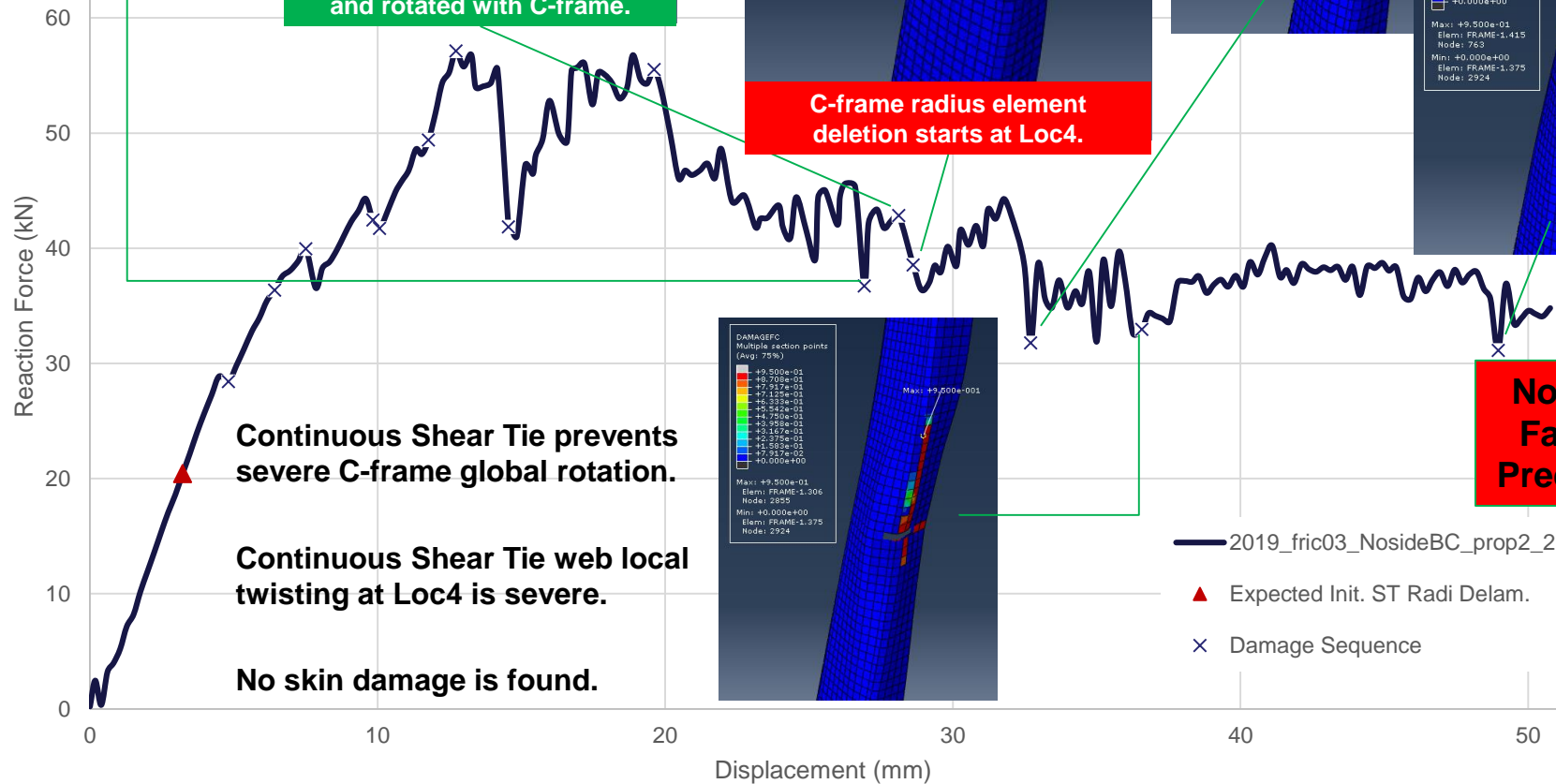
C-frame damage starts with buckling at Loc4.

Shear Tie web is bent more and rotated with C-frame.

C-frame radius element deletion starts at Loc4.

C-frame damage starts with buckling at Loc4.

No Skin Failure Predicted



Continuous Shear Tie prevents severe C-frame global rotation.

Continuous Shear Tie web local twisting at Loc4 is severe.

No skin damage is found.

- 2019_fric03_NosideBC_prop2_2
- ▲ Expected Init. ST Radi Delam.
- × Damage Sequence

Test Schedule

- May 2019
 - Complete assembly (1st specimen)
 - Install strain gauges
 - Test site prep; fixtures install
- June 2019
 - Mount the first specimen in UCSD Powell Lab
 - Perform tests on first specimen
 - Assembly of all specimens (3 remaining specimens)
 - Install strain gauges
- July 2019
 - Perform testing on final 3 specimens

Outline

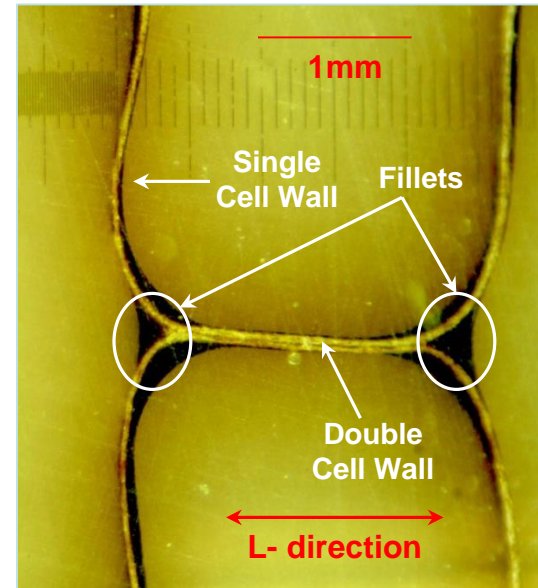
- Ground Service Equipment (GSE)
High Energy Wide Area Blunt Impact
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& Core Crush Mechanics
- Conclusions, Benefits to Aviation, and
Future Work

Introduction – Sandwich Core Crush

- Sandwich panel core crush/wall fracture affects residual strength
- Complex Nomex® core mesostructure ($\rho = 64 \text{ kg/m}^3$) affects core crush response



W-direction side view



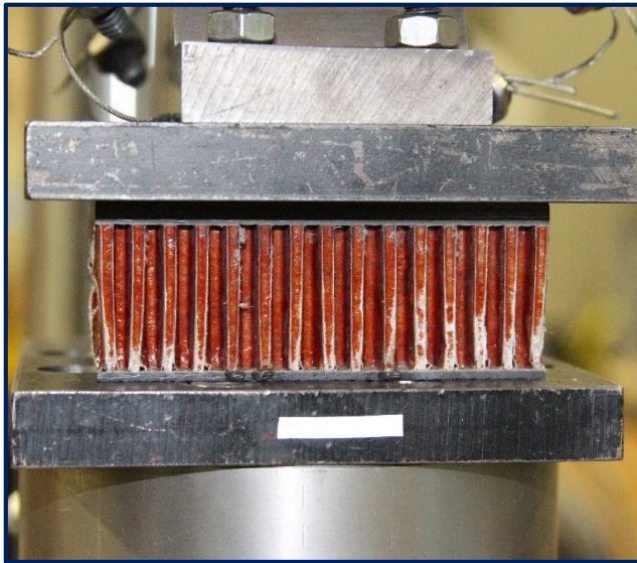
Objectives:

- Determination of core damage extent under impact loads
 - focus on cellular core fracture mechanisms
- Employ image processing techniques to quantify core geometry imperfections
- Modeling core crush tests to include key features and manufacturing defects

Approach

1) Core Crush Experiments

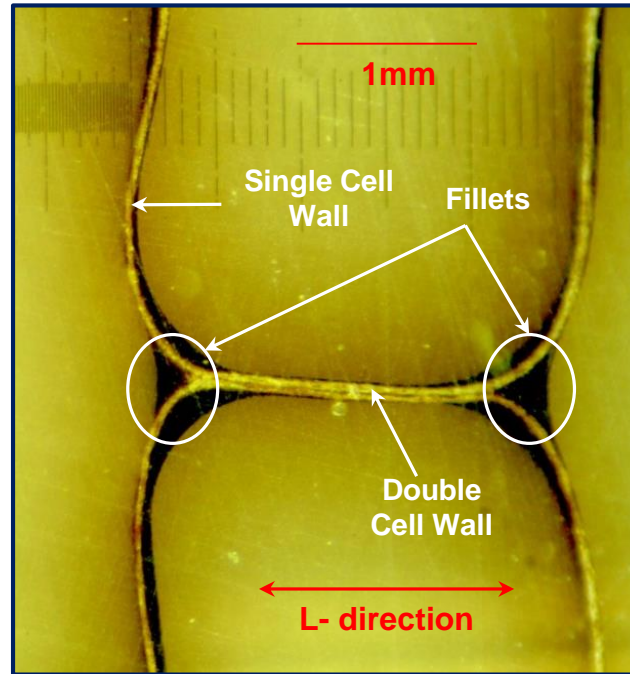
- Observe key mechanisms leading to cell collapse



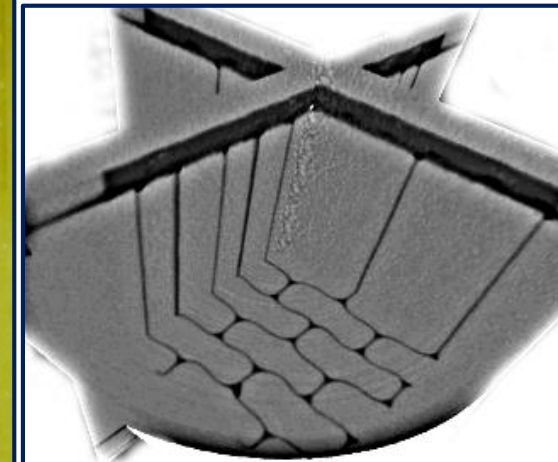
Flatwise compression test apparatus on Nomex® cores

2) Actual Geometry Quantification

- Metrics of geometry, including imperfections
- damage onset and evolution



Morphology of pre-impregnated Nomex® walls

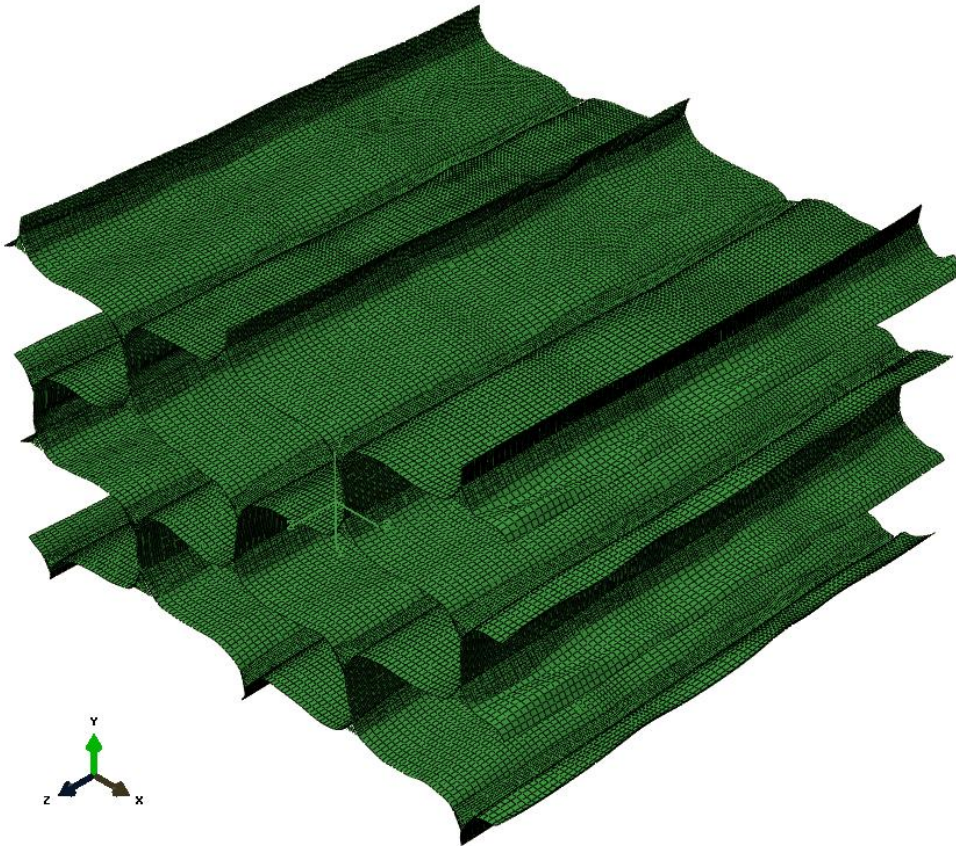


X-Ray Computed Tomography (CT) scans on honeycomb core samples (Univ. Utah)

Approach

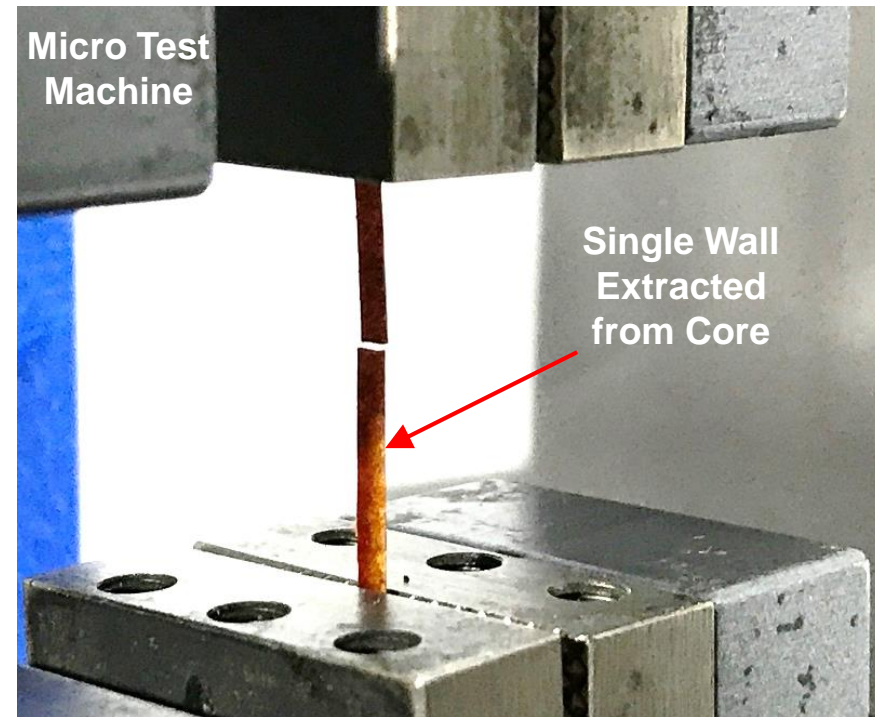
3) Finite Element Modeling

- Incorporate geometric defects



4) Basic Constituent Properties Determination

- Constitutive modeling & data gathering via single wall tests



1) Core Crush: Ice Impact Tests

- 10° glancing angle, 80 - 160 m/s velocity; 275 - 590 J kinetic energy, 4-ply PW

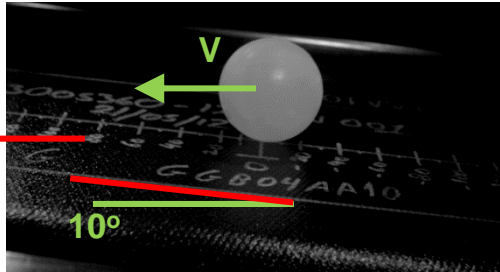


50.8 mm ice bal in sabot



t = 1.665 ms from trigger

Impact direction

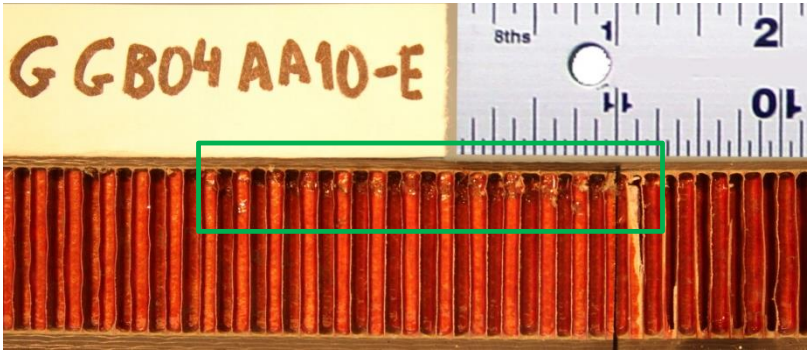


t = 1.332 ms from trigger

- High Speed videos from 590J impact (Velocity: 360 mph)

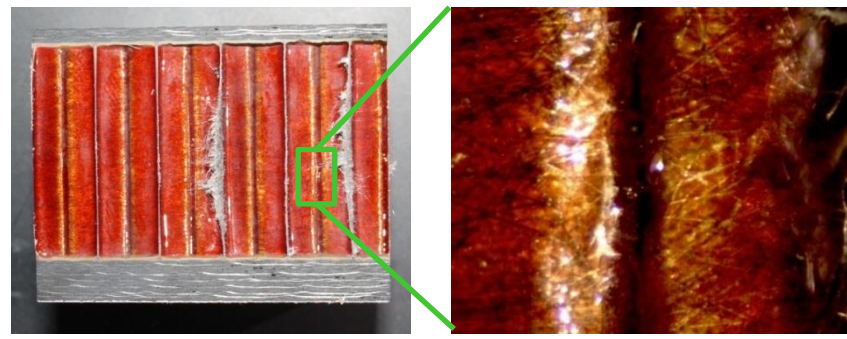
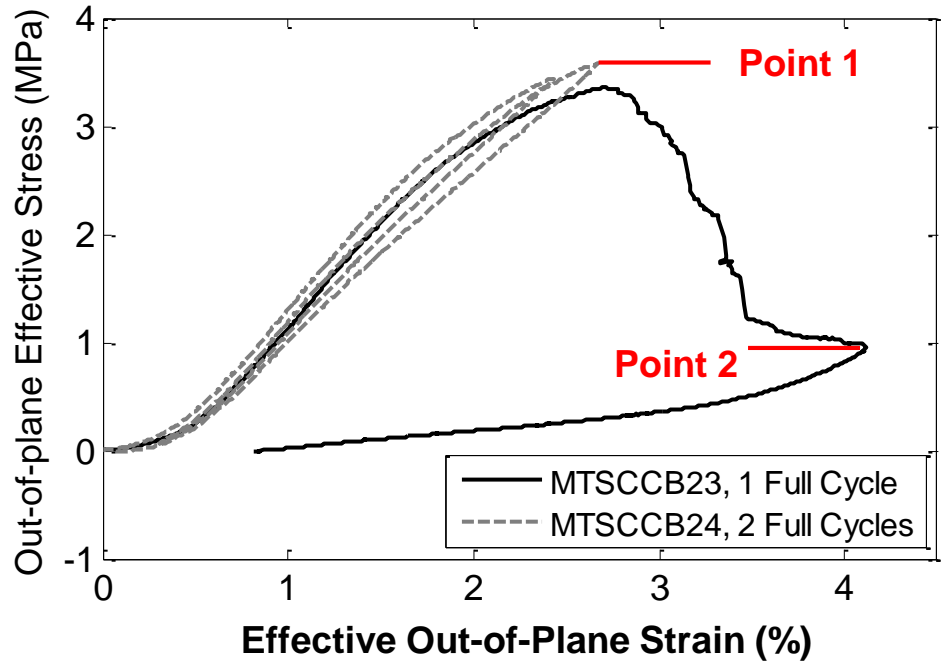


Hightspeed camera #1: GGB04AA10 test



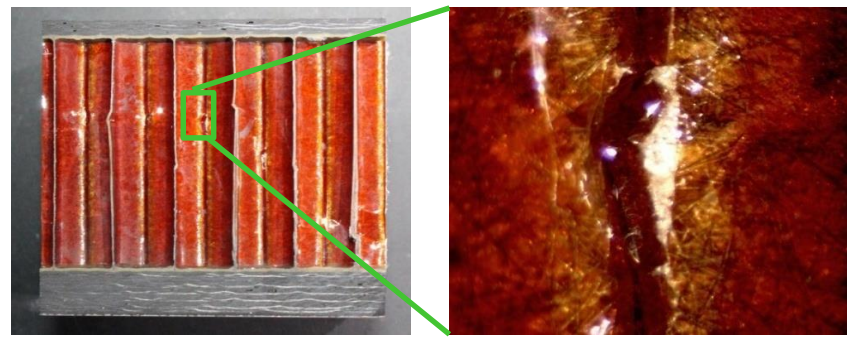
Core crushing span for 590 J energy: ~76 mm

1) Core Crush: Flatwise Compression



Unloading at peak stress (Point 1):

- Onset of resin fillet disbonding from cell wall
- Strength is recoverable upon re-loading



Unloading at crushing region (Point 2):

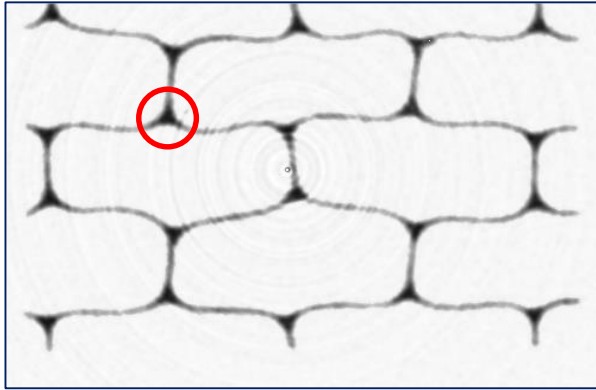
- Fractured fillet leading to local cell collapse
- Strength and stiffness not recoverable

Sequence of crushing phenomena

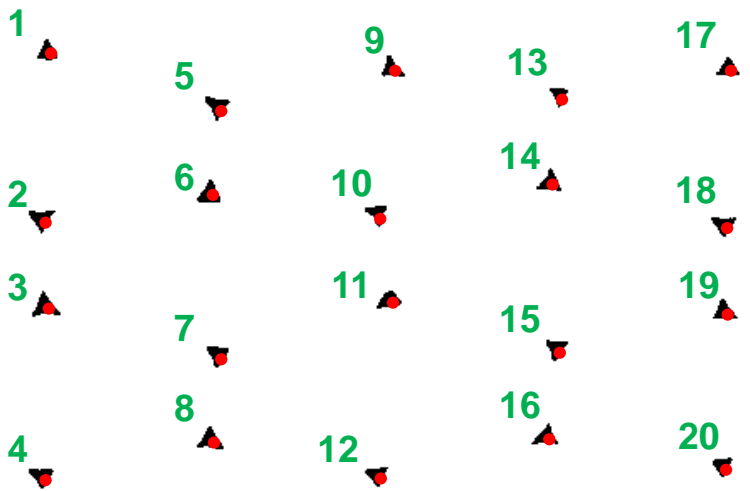
1. Visual buckling of outer core corners
2. Visual post-buckling of single cell walls
3. Local disbond of fillet column
4. Kinking of single cell walls and fillet columns

2) Actual Geometry: 3D Reconstruction From Imaging

1. Isolate critical pixels describing cell wall and fillet zone geometries



Through-thickness CT-scan slice



Resin-rich (Fillet) zones

2. B-spline surfaces and volumes to interpolate data points

$$C(u) = \sum_{i=0}^n N_{i,p}(u)P_i, \quad u \in U, \quad U = \{0, \dots, 0, u_{p+1}, \dots, u_{m-p-1}, 1, \dots, 1\}$$

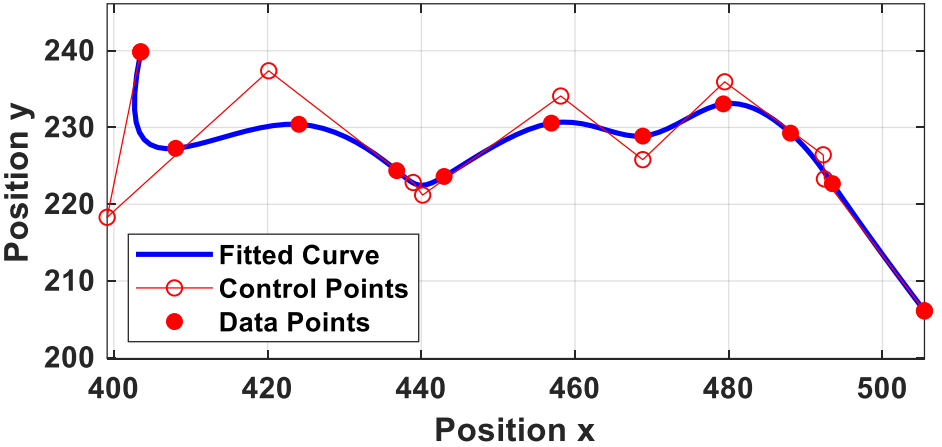
$$N_{i,p}(u) = \frac{u - u_i}{u_{i+p} - u_i} N_{i,p-1}(u) + \frac{u_{i+p+1} - u}{u_{i+p+1} - u_{i+1}} N_{i+1,p-1}$$

P_i : Control points, U = Knot vector

Inverse Problem

$$Q_k = C(\bar{u}_k) = \sum_{i=0}^n N_{i,p}(\bar{u}_k)P_i,$$

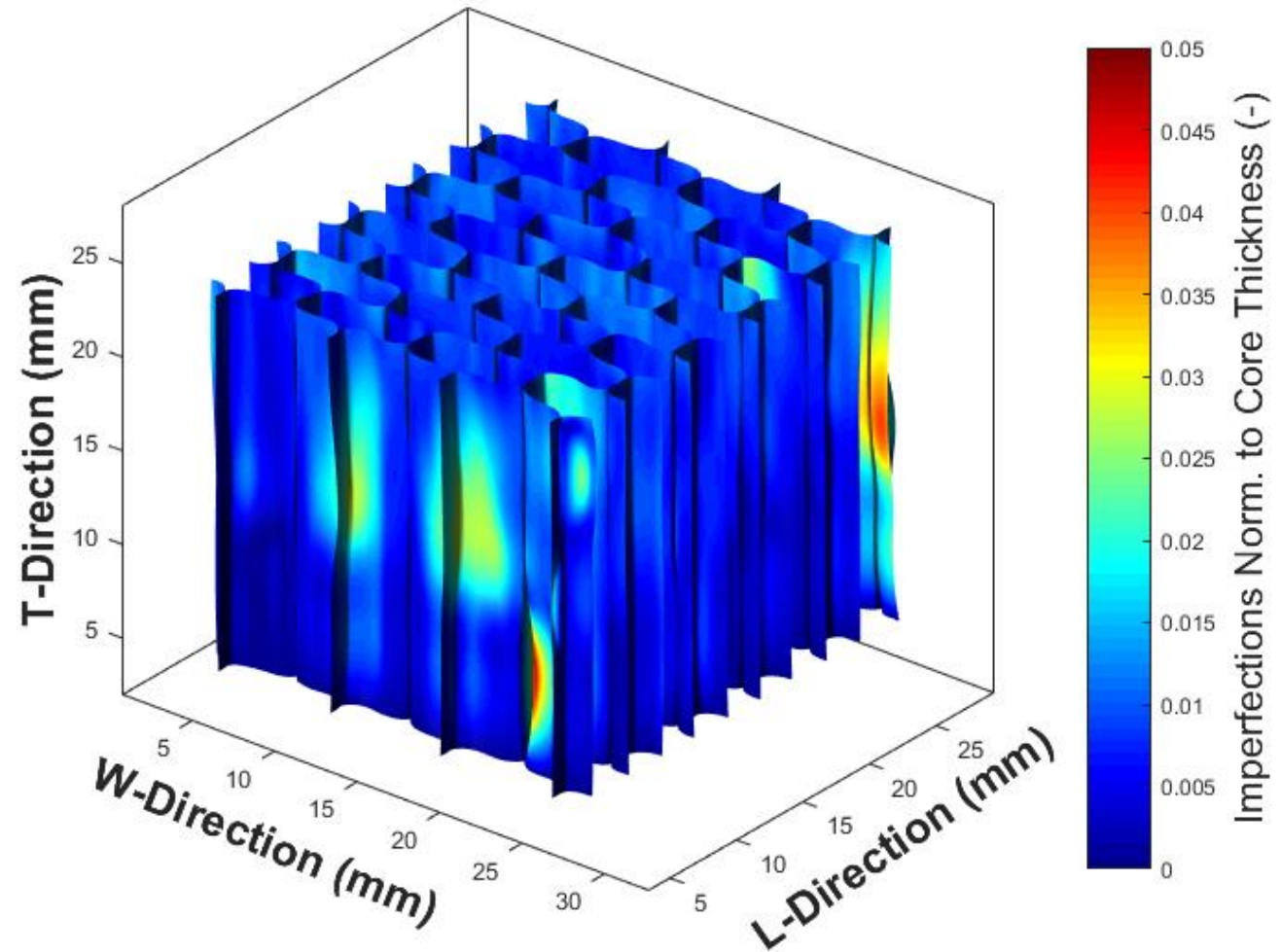
Find P_i and U by solving $(n + 1) \times (n + 1)$ system



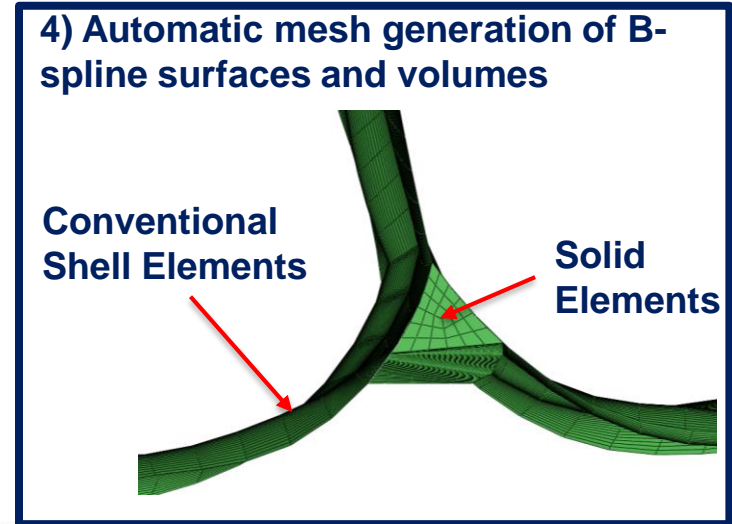
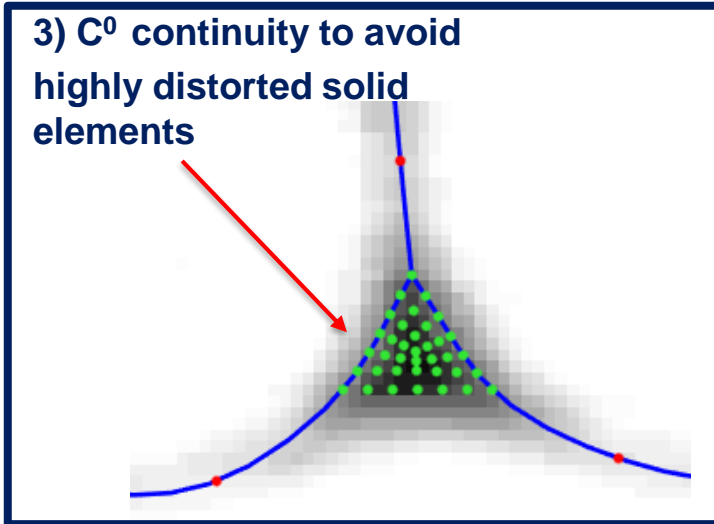
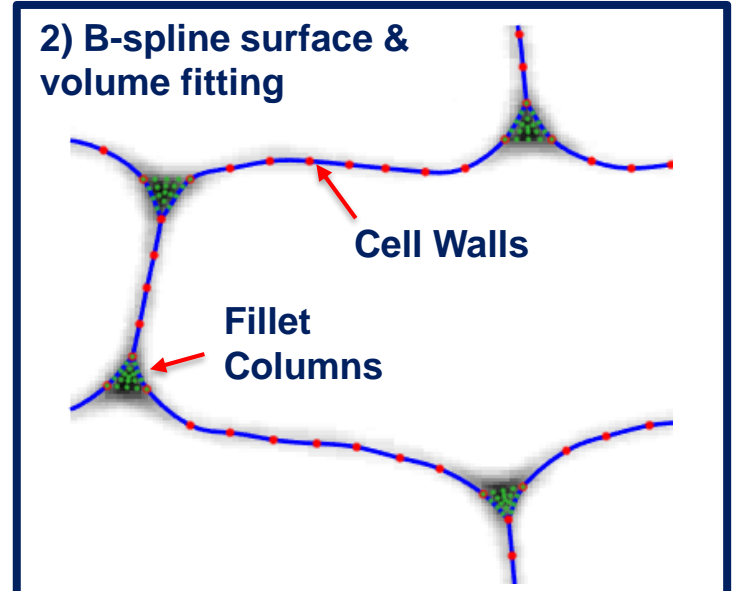
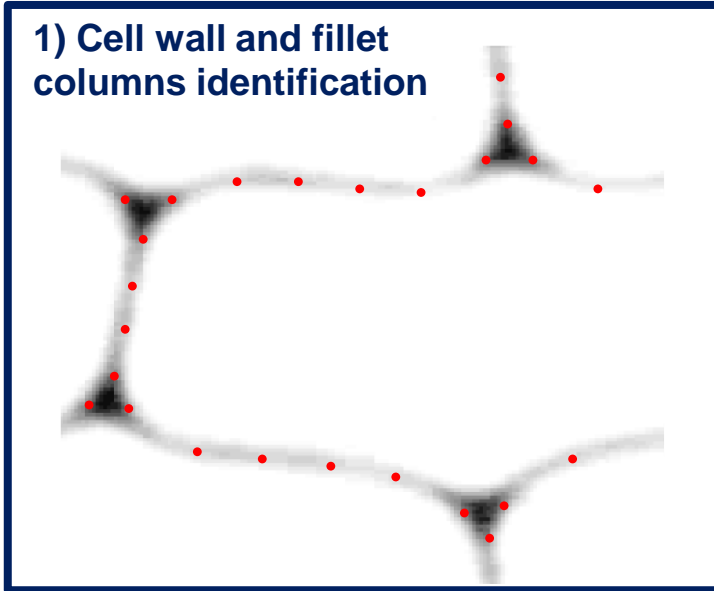
2) Actual Geometry: 3D Reconstruction From Imaging

- 7 CT-scan slices at different core thickness locations
- Interpolated to create 3D geometry model (for FEM)

Reconstruction of Pristine Core Sample Using CT-Data

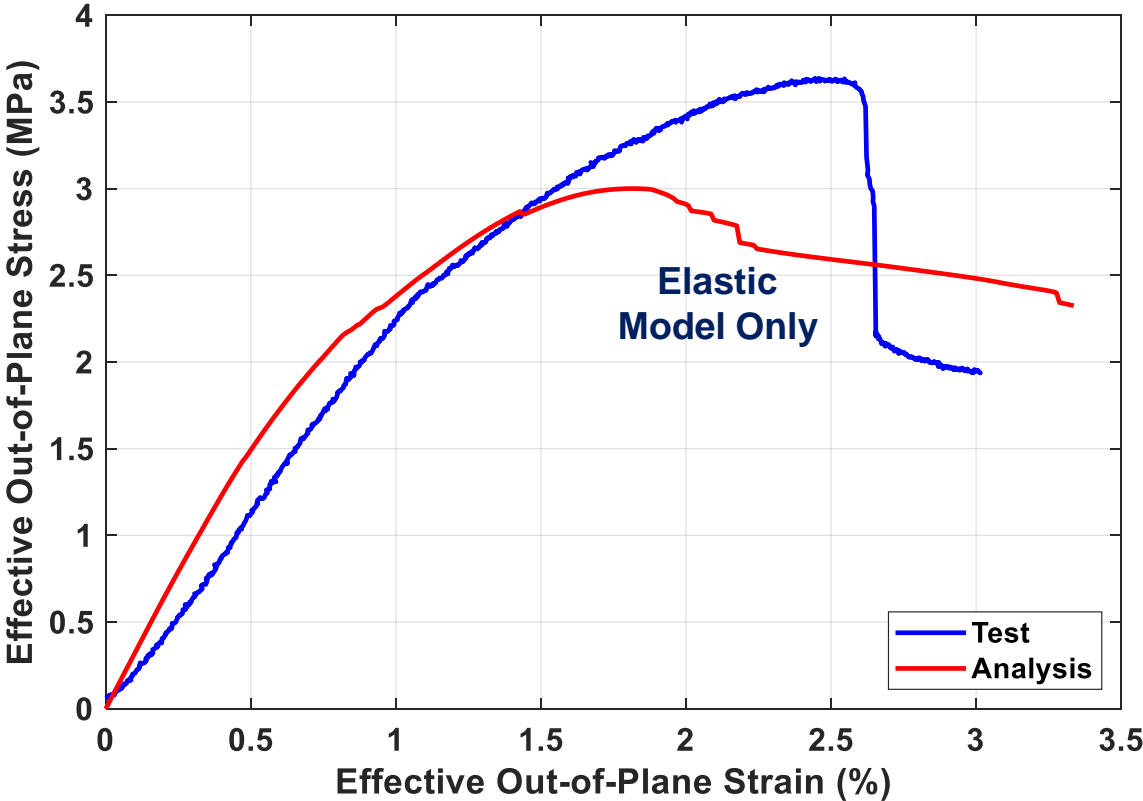


3) FEM: Automated FE Mesh Generation

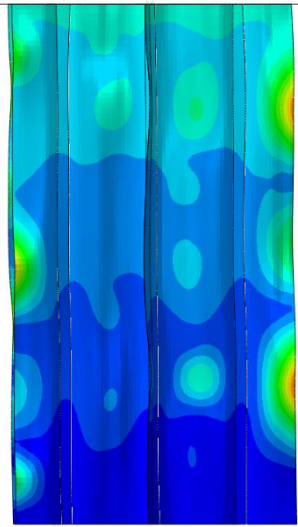


3) FEM: Simulation Results – Single Cell Geometry

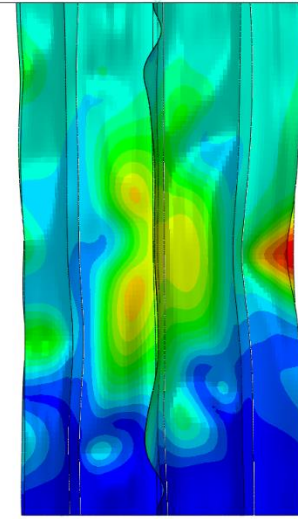
- Elastic properties from literature (limited available data)
- Cellular geometry extracted from CT-scans
- Underestimation of collapse strength (~80% of tests)
 - need improved material properties



Effective Strain = 0.6%

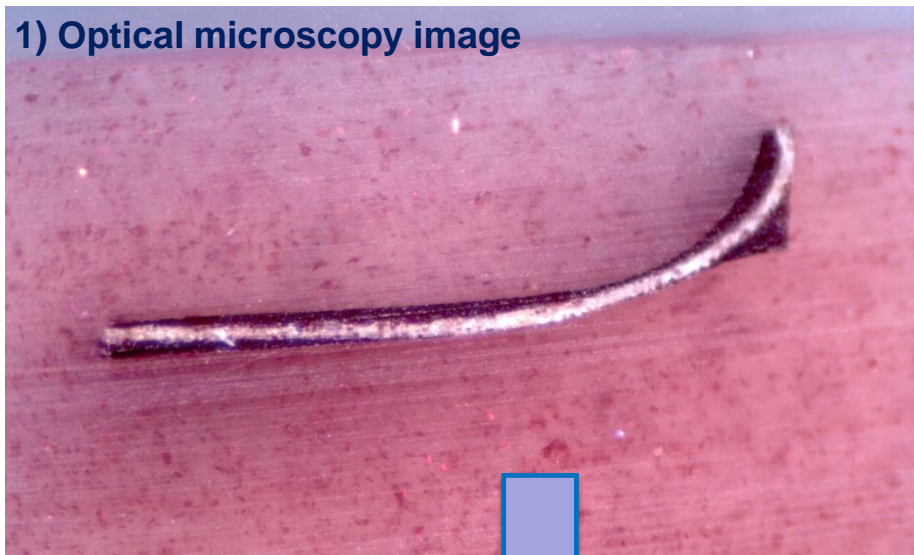


Effective Strain = 1.6%

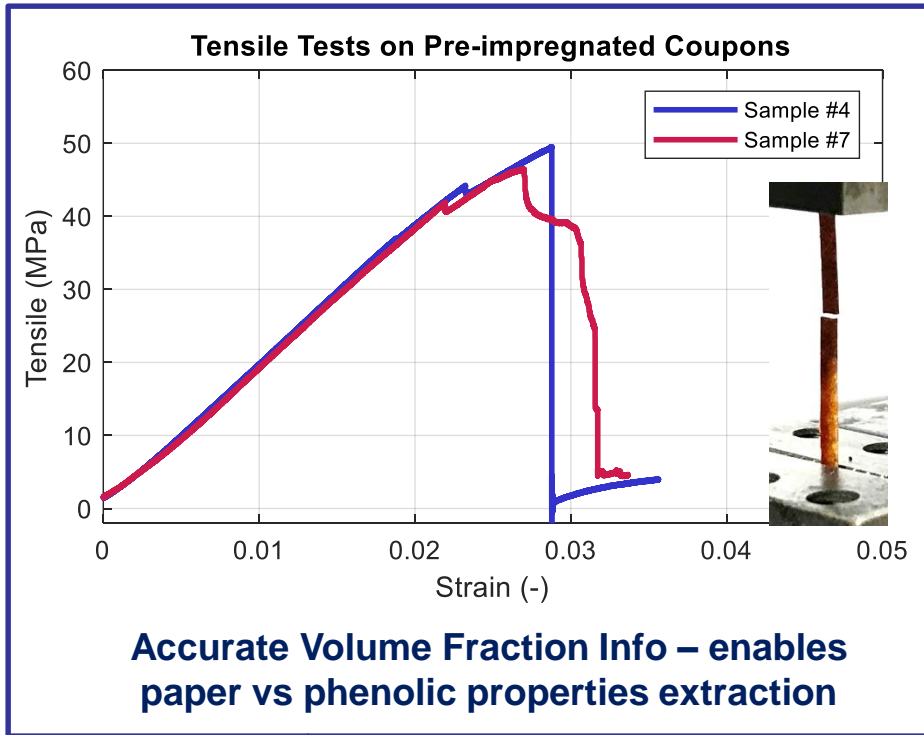
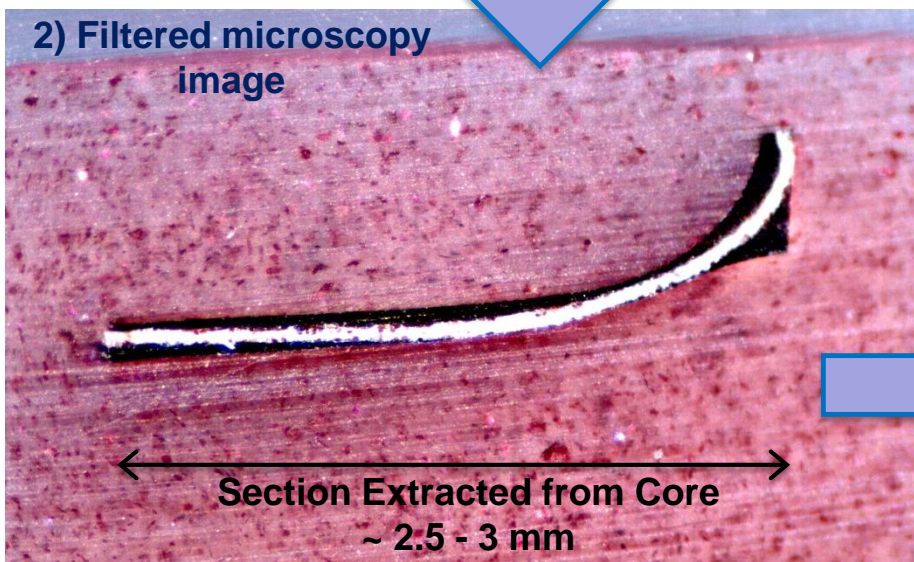


4) Basic Constituent Properties: Nomex Cell Walls

1) Optical microscopy image

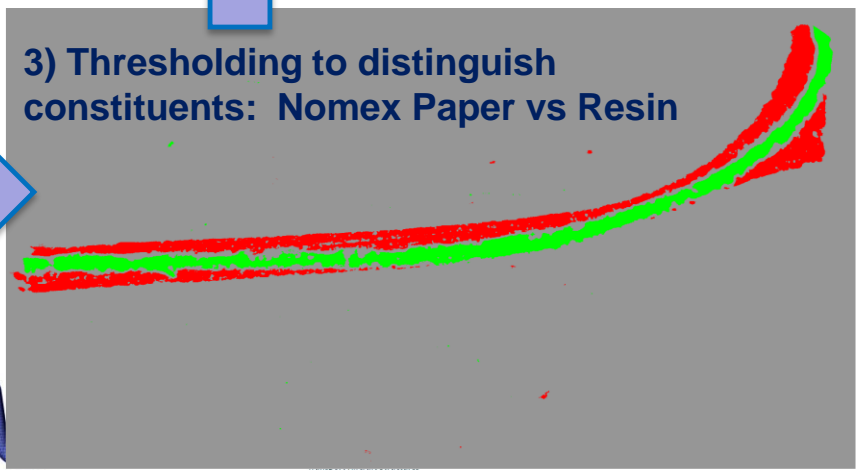


2) Filtered microscopy image



Improved Test Understanding

3) Thresholding to distinguish constituents: Nomex Paper vs Resin



Outline

- Ground Service Equipment (GSE)
High Energy Wide Area Blunt Impact
(HEWABI)
- Impact Damage to Sandwich Panels &
Core Crush Mechanics
- **Summary, Benefits to Aviation, and
Future Work**

Summary

Ground Service Equipment (GSE) High Energy Blunt Impact

- 2nd Generation HEWABI specimen design & fabrication + assembly nearly completed, test fixtures ready
- FE simulations of blunt impacts near floor beam completed
 - predict sequence of failure modes; major internal damage w/ no skin failure
 - truncated specimen geometry shows equivalence to full quarter barrel
- Prediction & sub-structure test methodology established for HEWABI testing

Impact Damage to Sandwich Panels

- Nomex[®] based core cells exhibit mesoscale structural complexity
 - Phenolic resin-rich zones around wall intersection boundaries (fillet columns) strongly affect core crush stability
- Image analysis used for 3D reconstruction of actual geometry using CT-scan data
- Numerical models are underestimating collapse strength of cores
 - non-uniform phenolic resin coating & fillet columns
 - effects of actual imperfect geometry

Benefits to Aviation

- Understanding damage resulting from HEWABI
 - key phenomena awareness and possible internal damage modes can be predicted
 - guides inspection strategies and location definition
 - permits more accurate model representation, could influence design
- Improved FE modeling methodology and validation for blunt impact damage
- Demonstrate techniques for effective boundary conditions definition for smaller sub-structure specimens to represent larger full structure.
- Establish relationship between core features vs crushing and fracture
 - resin fillet columns
 - non-uniform resin thickness coating cell walls
 - geometric imperfection of walls
- Understand effects of manufacturing defects/imperfection on core mechanics

Looking Forward

HEWABI:

- Complete HEWABI specimens assembly and testing
- Continued development of high fidelity FEA modeling capability for HEWABI
 - validated at element and full scale structure levels
 - define effective representation of fasteners and its influence in damage initiation and progression

Sandwich Core Crush:

- Simulation of core crush response with actual geometry & complexity (from microscopy, CT scans)
- Run parametric computational studies on the effect of the resin-rich zones on the out-of-plane crushing response of Nomex® based cores

Write Final Reports – Both Topics