

Review of Advanced Materials -Characterization and Qualification Guidelines

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JAMS 2017 Technical Review March 21, 2017

WSU Projects

- Advanced Fiber Reinforced Polymer Composite Materials
 Characterization and Qualification Guidelines for Aircraft Design and
 Certification
- Composite Repair Materials Characterization and Qualification Guidelines for Aircraft Design and Certification
- **Ceramic Matrix Composite (CMC)** Materials Characterization and Qualification Guidelines for Aircraft Design and Certification
- **Polymer-Based Additive Manufacturing** Characterization and Qualification Guidelines for Aircraft Design and Certification
- Bond Process Qualification Protocol
- Adhesive Characterization Guidelines for Aircraft Design and Certification







Overview

Shared Goals

- Develop the qualification framework for a unique material form.
- Generate shareable databases and guidelines to benefit industry and regulatory authorities.

• Timeline

- Projects in varying stages of development
- All projects will have initial qualification framework and test data in early 2018

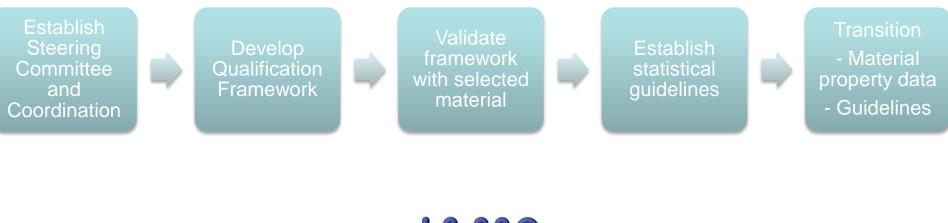






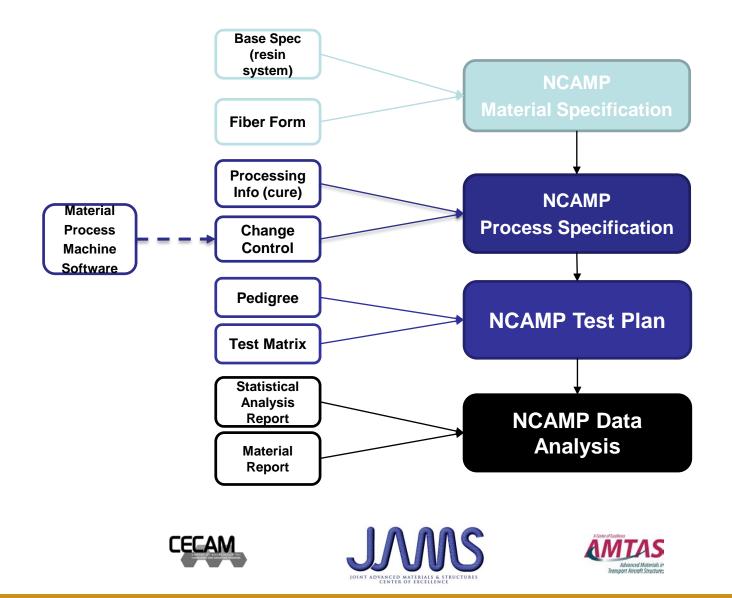
Technical Approach

- Develop a framework to advance selected material forms into the aerospace industry.
- Utilize the experience and framework of the NCAMP composite program as an example of process sensitive material characterization.
- Assess the validity of the qualification framework with equivalency testing.





Qualification Documentation



On-Line Portal

- All members of each Steering Committee have access to this site
- Meeting charts
- Documents for review
- Other relevant resources

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Wed 2017	nesday, March 1	5,			::	с <u>мс</u> ::				Rachael	1
	Title			Owner			Category	Modified Date	Size		
	CMC Qual Test Matrix - fo	r review		Rachael Andrulor	nis			2/28/2017	29.69 KB	Download	
	Feb meeting charts			Rachael Andrulor	nis			2/16/2017	781.23 KB	Download	
	Gonczy - CMC FAA Paper	r		Rachael Andrulor	nis			12/21/2016	455.95 KB	Download	
	Gonczy - CMC FAA Certifi	ication Presentation	I	Rachael Andrulor	nis			12/21/2016	707.92 KB	Download	
	Kick-Off Telecon Charts			Rachael Andrulor	nis			12/21/2016	1.73 MB	Download	

Example: http://www.niar.wichita.edu/ncampportal/CMC/tabid/177/Default.aspx







ADVANCED FIBER MATERIALS







Survey Overview

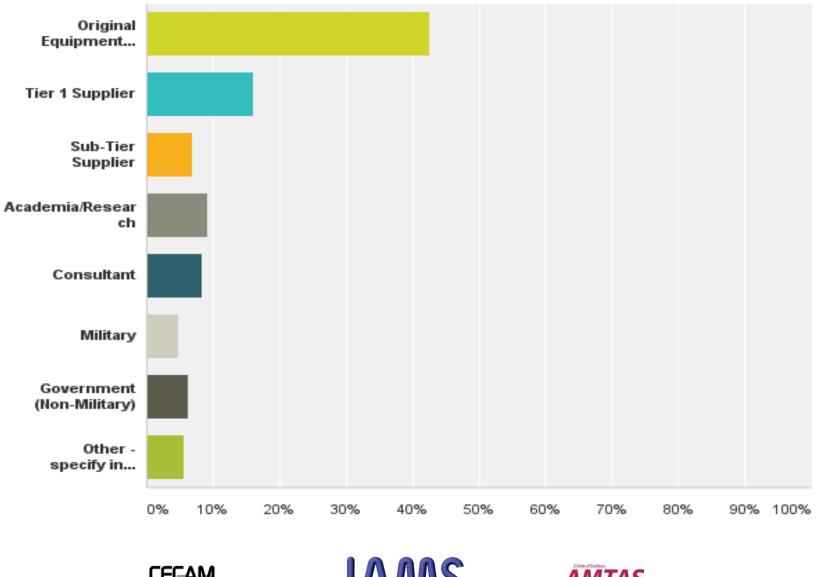
- **Objective**: To generate industry driven input on the development of a qualification framework for an advanced PMC material system.
- Administered to the composites community through Survey Monkey (Oct -Nov) to 143 responses received.
- The survey included multiple parts:
 - 1. Current PMC material forms and processes
 - 2. Future/planned material forms and processes
 - 3. Applications and parts
 - Factors affecting the decision making process when considering new PMC materials
 - 5. Individual and company interest in serving on steering committee or contributing to CMH-17







Results: Organization Type

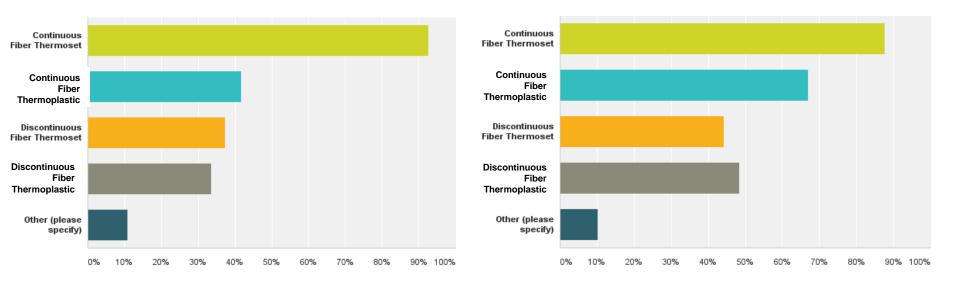








Results: PMC Material Forms



Currently In Use

5 – 10 years

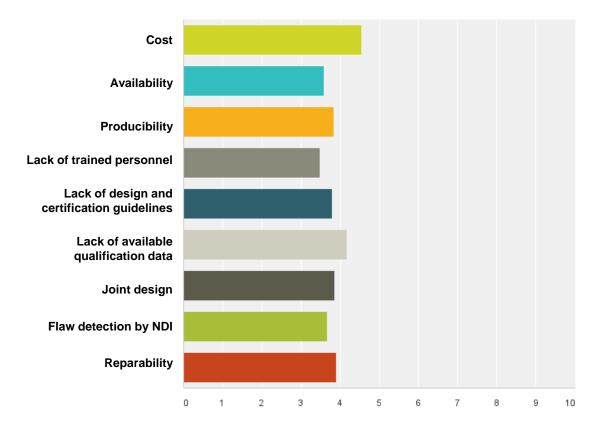
	NOW	5-10	
PMC Form	[%]	Years [%]	Change
Continuous Fiber Thermoset	93	88	-5%
Continuous Fiber Thermoplastic	42	67	60%
Discontinuous Fiber Thermoset	37	44	19%
Discontinuous Fiber Thermoplastic	34	48	44%
Other	11	10	-5%







Challenges









Advanced Fiber Current Status

Material Selection

- Thermoplastic composite based on survey results
- Initial phase: UD Tape Thermoplastic
- Secondary phase: Chopped Fiber Thermoplastic
- Material Partner: Tencate TC1225 (PAEK) UD Carbon
 - Polyarlyetherketone (PAEK) resin
 - Available commercially
 - Low melting point that makes for easier processing
 - Can be cured in an oven or autoclave
 - Can be used in melt overlay scenarios which make it more versatile for co-cure situations
 - Good smoke, toxicity, and flammability results.

Next Steps

- Steering Committee
- Draft of test matrix and test plan







REPAIR MATERIALS







Repair Survey Overview

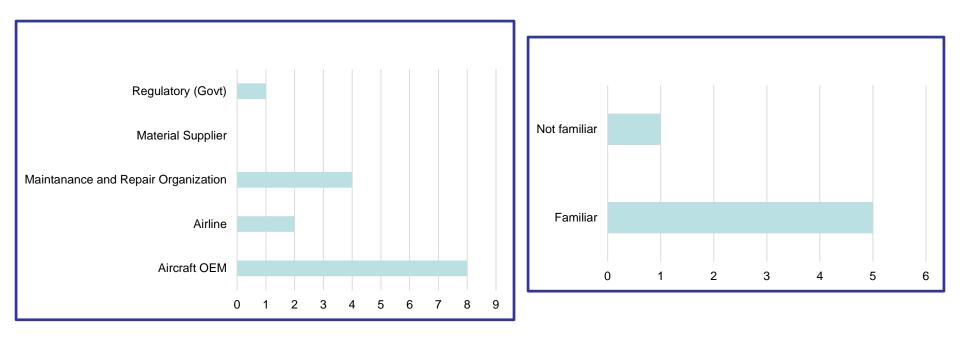
- **Objective**: To seek industry experts' guidance regarding
 - Repair material and technology development existing repair procedures and manuals, training curriculum and technology transfer, repair records keeping and new repair processing technologies
 - Identify a repair composite system(s) suitable for the initial qualification methodology framework.
- Administered to the repair community through Survey Monkey (Nov-Dec 2016).
- Results included information on:
 - Composite parts that are most commonly damaged
 - Most commonly used materials and processes for repair
 - Successes, challenges and lessons learned encountered during repair







Repair Survey Results



Organization

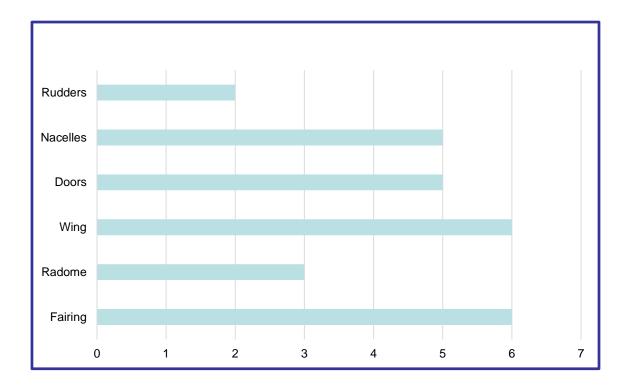
Familiar with CMH-17 and NCAMP







Parts Most Frequently Damaged









Most Commonly Used Systems for Repair

• Most commonly used systems used for repair: include the parent materials used for the base structure, wet lay-up systems or out-of autoclave prepreg systems.

• Parent materials:

- Mostly 350°F carbon fiber/epoxy or fiberglass/epoxy prepreg,
- Mostly fabric with some unidirectional tape: AS4/8552, AS4/3501-5, T300/934, T300/970, T300/F593, G30/F593, etc.
- Fiberglass/epoxy prepregs are typically used for fairings, radomes and interior structures.

Repair Processes:

 Most of the repairs conducted are autoclave, oven or heat blanket cured.







Commonly Used Materials

Wet lay-up systems:

- Laminating resins LY5052, EA9396, Epocast 52 A/B, EA9390
- Dry carbon fabric Plain weave 193 gsm, 5HS, 8HS.
- Dry glass fabrics AMSC9084 grade III and grade VIII
- Specifically: Epocast 52 A/B + dry carbon fabric G0904 (plain weave 193 gsm) (AMS2980 CACRC qualified)

Prepregs and adhesive films:

- Cytec 5320-1 OOA
- Hexply M20/40%/G904 + EA9695 05NW (AMS 3970 CACRC qualified)
- Hexply M20/40%/G904 + FM300-2M
- Hexply M20/34%/134 or M20/34%/194 + FM300-2M (AMS6885 CACRC qualification in progress)
- Hexply F155/ 3K-70PW
- Hexply F263/3K-70PW
- Hexply F155/ 7781 Fiberglass Prepreg







Lessons Learned

- Preparation of bonding surface
- Removal of moisture
- Oil/contamination
- Insufficient drying of original parts
- Water tightness
- Control of thermal curing
- Repair inspectability after the repair application
- Importance of strict adherence to the SRM instructions and technician training to ensure quality repairs.
- Other challenges include repair material supply and storage, OEM approvals of repair materials for particular applications, and OEM proprietary test data







Industry Needs

- Results showed a strong need for the standardization of composite repair.
- The need for new materials, particularly lower temperature cure materials.
- Data
- Better documentation, training, and information to be included in the repair manuals.
- Several recommendations for improvements to existing repair procedures were suggested including:
 - More closely following current procedures, supplying build data, better NDT procedures and standards, better surface preparation and inspection procedures, more comprehensive process details, repair technology transfer, repairmen minimum training requirements and more extensive use of travelers.







Repair – Current Status

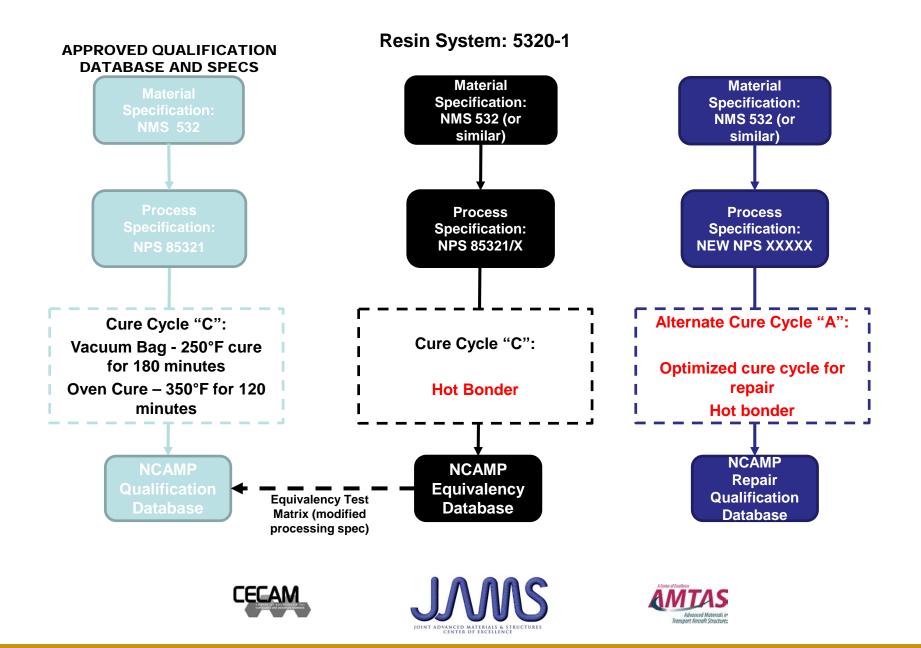
- <u>Steering Committee</u>
 - Established based on survey results
 - Monthly meetings began in January
- <u>Material Partner</u>
 - Solvay 5320-1 / T650 PW
- Qualification Framework
 - Process Spec initial draft complete
 - Material Spec already approved, possible modifications
 - Test Plan in development







Current Approach



CERAMIC MATRIX COMPOSITE MATERIALS

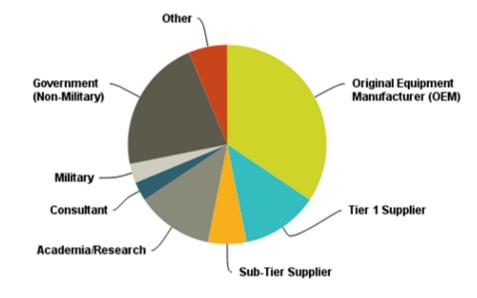






Survey Results

- **Objective**: Generate industry input on issues for qualification and material selection
- Administered by Survey Monkey (Oct Nov 2016)
- **Responses**: 32 responses received (21%)

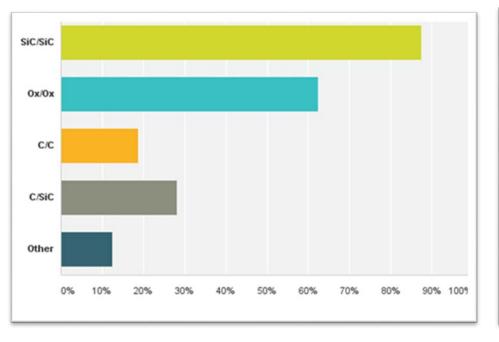




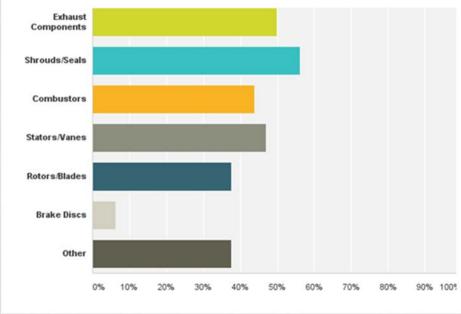




CMC Survey Results



CMC Materials Currently Used



Parts Made With CMC Materials







Survey Responses

- Challenges related to CMC Materials
 - Highest rated: <u>cost</u> (4.38) and <u>lack of design and certification</u> <u>guidelines</u> (4.03)
 - Other noted challenges:
 - Reproducibility of parts with consistent properties
 - Stability of materials and processes over time and the cost to evaluate stability
 - Current state of CMC materials is such that only limited applications exist
 - Limited design database and lack of lifetime testing presents challenges to trustworthiness and safety of the design







CMC Materials – Current Status

- Steering Committee
 - Monthly meetings
 - Input on test matrix
- Coordination
 - CMH-17 CMC Coordination Group
 - USACA, ASME, AFRL, NASA inputs
 - ASTM C28







CMC Materials – Current Status

- Material Partner: Axiom
 - CMC Oxide/Oxide Prepreg specific form TBD
 - Ox/Ox composites becoming mainstream material option for high temp composites
 - Cost reductions are required to keep market competitive with Ti and other high temp alloys
 - 3M Nextel Ceramic Fibers
 - Axiom prepreg developer
 - Composite Horizons Inc parts designer



CMC Materials – Current Status

- Qualification Framework Documents
 - Test Matrix
 - Initial draft reviewed
 - Input and comments
 - Test Plan being drafted
 - Test Matrix includes:
 - Composite Physical and Thermal Properties
 - Lamina Mechanical Fabric
 - Laminate and Design Guidance
 - Advanced Design Guidance







Composite Physical and Thermal Test Matrix

Test Method MIL-HDBK-787	per Panel	Comments
-	4	
	1	NDT on flat cured/consolidated composite test panels. Chosen
MIL-HDBK-731		methodology should consider the CMC constituents being evaluated.
MIL-HDBK-733 CMH		
17 V5 Sec. 3.7		
ASTM D3171	Determined for	To be used for determining normalized mechanical properties.
(Method II)	all mechanical	
	test specimens	
ASTM D3171	3	Requires knowledge of the fiber and cured/consolidated composite
(Method II)		density and weight of the fiber in a single unconsolidated ply (fiber areal weight).
ASTM D3171	3	Assumes zero void content, which will lead to gross error due to the
(Method II)		highly porous nature of CMCs; however, the equations can be modified
		using the actual void content found by optical microscopy. Requires
		knowledge of the fiber, matrix, and cured/consolidated composite
		density along with the void content and weight of the fiber in a single
		unconsolidated ply (fiber areal weight).
ASTM C373	3 (total per batch)	Density of monolithic ceramic processed with composite test panels.
ASTM C373	3	Density of composite taken from composite test panels.
Optical Microscopy	3	Determined by optical microscopy of polished cross-section.
CMH-17 V5 Sec. 3.6		
ASTM E1269	3 (total per batch)	The temperature range of interest must be defined.
ASTM E1461	3 (total per batch)	Test temperatures must be defined. Directions need to be determined
	, , ,	based on the thermo-physical differences/likeness between the fiber
		and the matrix as well as the fiber form (i.e. 1-D, 2-D weave, or 3-D
		weave). Directions to consider: in-plane (fiber direction) and out-of-
		plane (non-fiber direction).
ASTM E228	3 (total per batch)	The temperature range of interest must be defined. Directions need to
	, , ,	be determined based on the thermo-physical differences/likeness
		between the fiber and the matrix as well as the fiber form (i.e. 1-D, 2-D
		weave, or 3-D weave). Directions to consider: in-plane (fiber direction)
		and out-of-plane (non-fiber direction).
CMH-17 V5 Sec. 3.6	3 (total per batch)	
		A A A A
	JA	Advanced Materials in Transmission
	17 V5 Sec. 3.7 ASTM D3171 (Method II) ASTM D3171 (Method II) ASTM D3171 (Method II) ASTM C373 ASTM C373 Optical Microscopy CMH-17 V5 Sec. 3.6 ASTM E1269 ASTM E1269 ASTM E1269	17 V5 Sec. 3.7ASTM D3171 (Method II)Determined for all mechanical test specimensASTM D3171 (Method II)3ASTM D3171 (Method II)3ASTM D3171 (Method II)3ASTM C3733 (total per batch)ASTM C3733 (total per batch)ASTM C3733 (total per batch)ASTM C3733 (total per batch)ASTM E12693 (total per batch)ASTM E14613 (total per batch)

JOINT ADVANCED MATERIALS & STRUCTURES CENTER OF EXCELLENCE

Lamina Mechanical Test Matrix for 2-D and 3-D Fabrics

				Number	f Batches	
				x No. of	Panels x	
				No. of Sp	ecimens	
				Test Tem	perature	
Layup	Test Type and Direction	Property	Test Method	RTD	ETD	Comments
[0]	Warp In-Plane Tension	Strength, Modulus,	ASTM C1275 (RTD)	3x2x3	3x2x3	A number of differently shaped specimens are discussed for various fiber
		and Poisson's Ratio	ASTM C1359 (ETD)			forms and constituents. A contoured specimen is generally preferred,
		(RTD Only)				but the stress concentration at the radii and can be problematic for 1-D
						CMCs. A straight sided specimen may be more desirable for 1-D CMCs.
						Poisson's Ratio may be difficult to determine at high temperatures due
						to limitations of strain instrumentation.
[90]	Fill In-Plane Tension	Strength and	ASTM C1275 (RTD)	3x2x3	3x2x3	A number of differently shaped specimens are discussed for various fiber
		Modulus	ASTM C1359 (ETD)			forms and constituents. A contoured specimen is generally preferred,
						but the stress concentration at the radii and can be problematic for 1-D
						CMCs. A straight sided specimen may be more desirable for 1-D CMCs.
[0]	Warp In-Plane	Strength and	ASTM C1358	3x2x3	3x2x3	A straight sided specimen is generally preferred, but a contoured
	Compression	Modulus				specimen has been used successfully. For a straight sided specimen,
						consider using specimen detailed in SACMA SRM 1 with face supported
						fixture detailed in SACMA SRM1 or ASTM D695. For a contoured
						specimen, consider using specimen detailed in ASTM C1358 or ASTM
						D695 with face supported fixture detailed in SACMA SRM1 or ASTM D695.
						Back-to-back strain gages should be used on first two specimens from the
						RTD condition to assess bending (see note 2).
[90]	Fill In-Plane	Strength and	ASTM C1358	3x2x3	3x2x3	A straight sided specimen is generally preferred, but a contoured
	Compression	Modulus				specimen has been used successfully. For a straight sided specimen,
						consider using specimen detailed in SACMA SRM 1 with face supported
						fixture detailed in SACMA SRM1 or ASTM D695. For a contoured
						specimen, consider using specimen detailed in ASTM C1358 or ASTM D695 with face supported fixture detailed in SACMA SRM1 or ASTM D695.
						Back-to-back strain gages should be used on first two specimens from the
						RTD condition to assess bending (see note 2).
[+45/-45]	In-Plane Shear	Strength and	ASTM D3518	3x2x3	3x2x3	A simple test method but poor for measuring ultimate shear strength
[,]	(+45/-45 Tension)	Modulus				because fibers align with length/tensile axis as the specimen is loaded.
	(,					Offset strength, strength at defined strains, and modulus may be difficult
						to determine at high temperatures due to limitations of strain
						instrumentation.
[0]	In-Plane Shear	Strength and	ASTM D5379	3x2x3		Provides the best shear response of the standardized methods but not
	(Iosipescu Shear)	Modulus				suitable for high temperatures because fixture moves on greased
						rod/bearing. Can be used to supplement data obtained from ASTM D3518
						since this data is obtained from a mixed stress state.
[0]	Interlaminar Shear	Strength	ASTM C1292 (RTD)	3x2x3	3x2x3	The face supported fixture detailed in ASTM D695 is utilized to stabilize
	(Double Notch Shear)		ASTM C1425 (ETD)			the specimen. Notched specimens are more difficult to machine and
						failures are sensitive to notch quality.
[0]	Interlaminar Shear	Strength	ASTM D2344	3x2x3		ASTM D2234 is very simple and inexpensive, great quality control test,
	(Short-Beam Strength)					but the stress state is mixed. Can be used to supplement data obtained
						from ASTM C1292 since notched specimens are more difficult to machine
						and failures are sensitive to notch quality.







Laminate and Design Guidance

				Number	of Batches	
				x No. of		
				No. of Sp		
				Test Tem		
Layup	Test Type and Direction	Property	Test Method	RTD	ETD	Comments
	Flexure	Strength and	ASTM C1341	3x2x3		A good test for material development, quality control, and material
[-]		Modulus				flexural specifications. A number of factors lead to ambiguity in using
						flexure results for CMC material design data. Uni-axial tensile and
						compressive tests are recommended for material design data based on
						uniformly stressed test condition. Flexural stress is calculated using
						elastic beam theory with the assumption that the material is
						homogeneous and linearly elastic. This only holds true when the
						principal fiber direction is transverse to the length of the beam. Four-
						point loading geometries are preferred. Modulus may be difficult to
						determine at high temperatures due to limitations of
						strain/displacement instrumentation.
[0]	Trans-Thickness	Strength	C1468	3x2x3		May be difficult to obtain valid failure modes for 3-D woven fabrics. More
[0]	(Flatwise) Tension	Strength	01100	SALAS		test development is necessary for testing at high temperatures.
[+45/0/-45/90]	Unnotched In-Plane	Strength and	ASTM C1275 (RTD)	3x2x3		A number of differently shaped specimens are discussed for various fiber
[+3/0/ +3/30]	Tension	Modulus	ASTM C1275 (RTD)	37273		forms and constituents. A contoured specimen is generally preferred,
		Woddids	ASTIMICISSS (ETD)			but the stress concentration at the radii and can be problematic for 1-D
						CMCs. A straight sided specimen may be more desirable for 1-D CMCs.
[+45/0/-45/90]	Unnotched In-Plane	Strength and	ASTM C1358	3x2x3		A straight sided specimen is generally preferred, but a contoured
[+3/0/ +3/30]	Compression	Modulus	A31101 C1330	37273		specimen has been used successfully. For a straight sided specimen,
	compression	modulus				consider using specimen detailed in SACMA SRM 1 with face supported
						fixture detailed in SACMA SRM1 or ASTM D695. For a contoured
						specimen, consider using specimen detailed in ASTM C1358 or ASTM
						D695 with face supported fixture detailed in SACMA SRM1 or ASTM D695.
						Back-to-back strain gages should be used on first two specimens from the
						RTD condition to assess bending (see note 2).
[+45/0/-45/90]	Notched / Open-Hole	Strength	ASTM D6484	3x2x3		Assumption is made that an open hole is critical for CMC notched
[* 10/ 0/ 10/ 50]	Compression	otrongen		GALAG	0//L/IO	compression testing.
[+45/0/-45/90]	Notched / Filled-Hole	Strength	ASTM D6742	3x2x3	3x2x3	Assumption is made that a filled hole is critical for CMC notched tension
[* 10/ 0/ 10/ 50]	Tension	otrongen	//01/12/07/12	GALAG		testing, as opposed to a open hole due to fastener torque/preload.
[+45/0/-45/90]	Single Shear Bearing	Strength	ASTM D5961	3x2x3		Procedure C is for a single-piece configuration, fastened to a robust
[* 10/ 0/ 10/ 50]	ongle oneur beuring	otrongen	(Procedure C)	GALAG		fixture.
[+45/0/-45/90]	Tension or Compression	Strength	ASTM D7136 &	3x2x3		Tension after impact strength may be more appropriate for CMCs than
, .,,,	After Impact		ASTM D5766 or			compression after impact due to the tension sensitive nature of CMCs
			ASTM D7137			and their specific applications. Consider using ASTM D5766 (open-hole
						tension) for guidance for performing the tension test. Modifications to
						ASTM D7136 may have to be made for CMCs (e.g. specimen geometry,







Advanced Design Guidance for 2-D and 3-D Fabrics

				Number o	of Batches	
				x No. of	Panels x	
				No. of Sp	ecimens	
				Test Tem	perature	
Layup	Test Type and Direction	Property	Test Method	RTD	ETD	Comments
Any	Fracture Toughness		ASTM D5528	1x2x3		Considerations may need to be made by the end user for specific
			ASTM D6671			applications. There may not be a consensus for a standard approach.
			ASTM E1922			Probably outside of the scope of the effort.
Any	Creep		ASTM C1291		1x2x3	Considerations may need to be made by the end user for specific
			ASTM C1337			applications. There may not be a consensus for a standard approach.
						Probably outside of the scope of the effort.
Any	Fatigue, In-Plane		ASTM C1360	1x2x9		Considerations may need to be made by the end user for specific
	Tension					applications. There may not be a consensus for a standard approach.
						Probably outside of the scope of the effort. If performed, would
						recommend 6 replicates at 3 stress levels.
Any	Fatigue, Thermal &		-	1x2x3		Thermal fatigue of specimens followed by determination of static in-
	Static, In-Plane Tension					plane tensile strength. Considerations may need to be made by the end
						user for specific applications. There may not be a consensus for a
						standard approach. Probably outside of the scope of the effort.







POLYMER BASED ADDITIVE MANUFACTURED MATERIALS







Project Overview

- Initial meeting/workshop: St. Paul August 2016
 - Material for initial qualification was selected: ULTEM 9085
 - Discussion on specifications and overall plan
- **Collaboration** with America Makes/AFRL/rp+m program
 - Shared resources
 - Deliverables and overall reporting are not changing
- Material Partner: Stratasys Certified ULTEM 9085
 - Polyetherimide high performance thermoplastic
 - Good smoke and toxicity rating
 - Ability to withstand high temperatures common use in aerospace and automotive duct work
- Controlled builds with fixed process
- Integrated test matrix





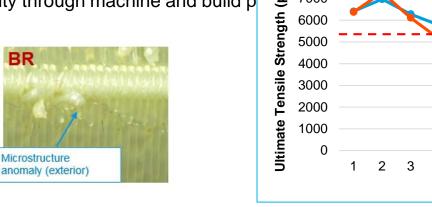


America Makes Program - High Performance Additive Manufactured Thermoplastics (HPAMT)

- <u>Objective</u>: Create dataset to expand and validate previous FDM data
- Enable industry members to use their own design allowable methodologies
- Led by RP+M (project management and build location)
 - Stratasys certified material supply, material and process specs, printing location
 - Zodiak printing location
- FDM Process Variability Analysis
 - Machine parameters

Burnt materia

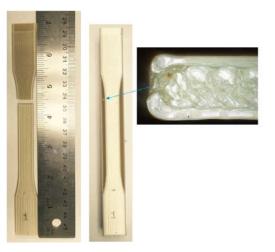
- Failure analysis/identify data spread
- Correlate data trends to machine and build paramet
- Control data variability through machine and build p

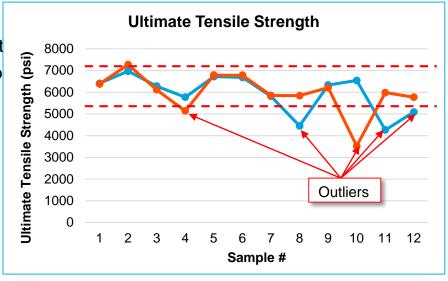










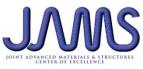


Current Steering Committee Activity

• Test Matrix

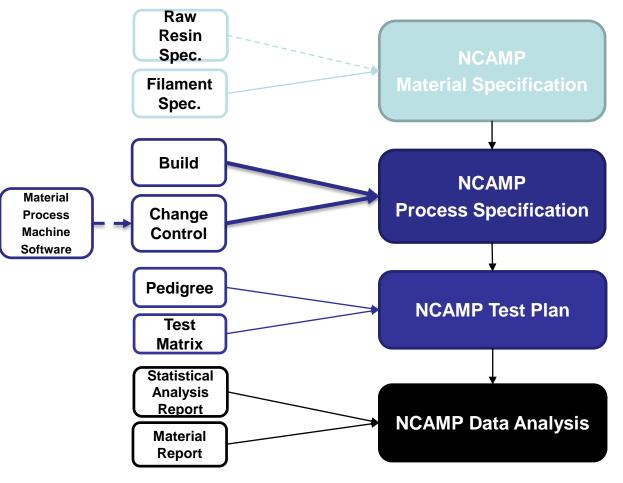
- Qualification matrix reviewed in February
- Test Plan: Material Property Data Acquisition and Qualification Test
 Plan
 - Initial draft posted in December
 - Several comments received
 - Updated version posted last week
- Other Upcoming Activity:
 - Specification Templates
 - Equivalency Test Plan
 - Coordination with SAE AMS AM Polymers







NCAMP DOCUMENTATION





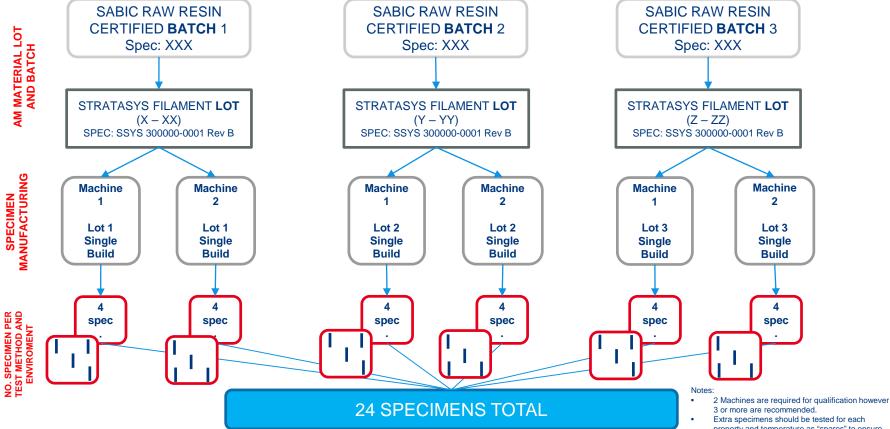


STATUS

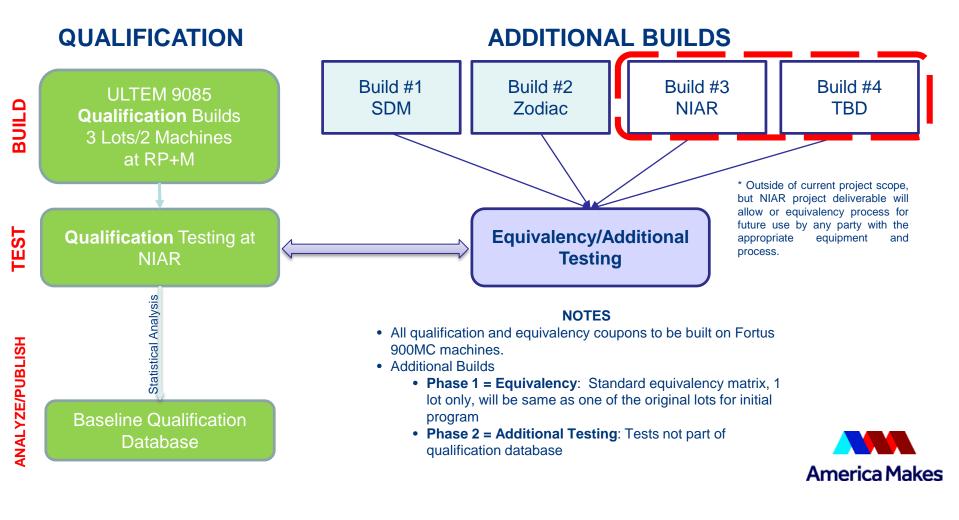
- Currently working with
 Stratasys to finalize Material and Process Specs (this week)
- Once content is stable, NCAMP templates to be developed
- Test Plan finalized, Equivalency plan being drafted
- Dimensional studies
 currently being conducted
- Site Inspections (Qualification) – week of March 27th
- Qualification builds to begin after inspections







property and temperature as "spares" to ensure desired quantity (min of 3 specimens).

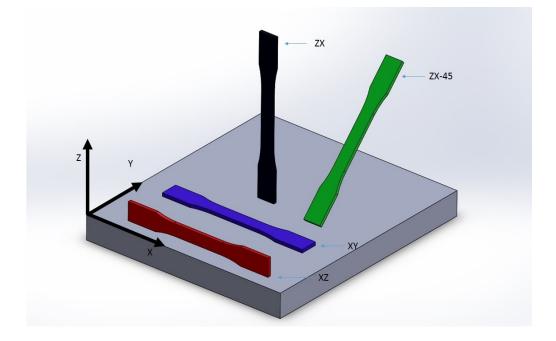








Build Orientation Investigation









ADHESIVE MATERIALS







Please contact Rachael if you are interested in more information:

rachael@niar.wichita.edu





A Center of Excellence Advanced Materials in Transport Aircraft Structures

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Questions?

Don't forget to fill out the feedback form in your packet or online at www.surveymonkey.com/r/jamsfeedback

Thank you.





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